

The Underline - Segment 6
BUILD Grant FY 2018
Appendix G

**Underline Road Impact Fee
Traffic Study**

Kimley»Horn

Memorandum

To: Ms. Darlene M. Fernandez, P.E.
Assistant Director, Traffic Services
Miami-Dade County Department of Transportation and Public Works (DTPW)

Ms. Maria Nardi
Chief of Planning and Design Excellence
Miami-Dade County Parks, Recreation and Open Spaces Department

Cc: Gaspar Miranda, P.E.
Leandro Oña, P.E.
Myra Patino
Mark A. Heinicke
Meg Daly, Friends of The Underline
Parker Thomson, Hogan Lovells
Hans Hertell, Hogan Lovells

From: Stewart E. Robertson, P.E.

Date: February 24, 2016

***Subject: The Underline
Miami-Dade Road Impact Fee Traffic Study***

We are pleased to submit the report of *The Underline Miami-Dade Road Impact Fee Traffic Study* for your review. The report represents the work of the study team to forecast the potential volume of Underline usage (pedestrians, bicyclists, and other non-motorized users) and to estimate the potential reduction in motor vehicle traffic that can be reasonably anticipated from the implementation of the project. The analysis followed the methodology established in *The Underline Miami-Dade Road Impact Fee Traffic Study Methodology*, November 4, 2015, with modifications as discussed in the project meeting on December 4, 2015, at the Traffic Engineering Division offices.

We look forward to discussing the results of the report with you once you have had a chance to review.

Respectfully submitted,

KIMLEY-HORN AND ASSOCIATES, INC.



Stewart E. Robertson, P.E.

The Underline – Miami-Dade Road Impact Fee Traffic Study

Purpose

The purpose of *The Underline Miami-Dade Road Impact Fee Traffic Study* is to measure the potential impact of The Underline on U.S. 1 traffic patterns and congestion. The Underline project does not expand roads to handle existing and future projected traffic, but rather makes the existing road system of U.S. 1 and its feeder roads into the city better able to handle existing traffic congestion by offloading a portion of that traffic into alternative transportation, including improved access to the transit system and non-motorized transportation alternatives. The potential for people to choose non-motorized transportation as a substitute for motor vehicle trips for certain trip types and trip patterns is just one of the many positive outcomes of The Underline.

Summary of Results

A summary of the results of *The Underline Miami-Dade Road Impact Fee Traffic Study* are presented below. Additional information and supporting documentation are provided in the remainder of this report and the Attachments.

- The Underline is anticipated to generate approximately 8,000 to 9,000 users per day.
- Based on an average trip length of 2 miles, The Underline will carry a volume of approximately 1,600 to 1,800 trips on average at a given point along the corridor.
- Measuring the mode shift between automobile traffic and non-motorized traffic caused by the implementation of urban trails can be estimated based on methodologies established within published literature.
- Vehicle substitution rates for The Underline were calculated based on a blend of two published methods.
 - Method 1 – Estimate the percentage of non-motorized transportation trips that are shifted from motor vehicle trips.
 - Method 2 – Estimate the percentage of motor vehicle trips that could be replaced by non-motorized transportation modes.
- The amount of motor vehicle traffic reduction on U.S. 1 as a direct result of The Underline is anticipated to range from 643 vehicles per day to 1,007 vehicles per day depending on the location along the corridor.
- The percentage reduction in traffic volumes on U.S. 1 as a direct result of The Underline is anticipated to range from -1.04% to -2.66%.
- Intersection capacity analyses were conducted for the weekday A.M. and P.M. peak periods at five intersections as determined during the methodology phase of this study. Intersection analyses were performed using Trafficware's *Synchro 8.0* traffic engineering analysis software.
- The Underline is anticipated to result in vehicle delay reductions at signalized intersections of up to -3.89% for total intersection delay in the A.M. peak period.
- Reductions in individual approach delays are anticipated to range up to -5.63% for through movements on U.S. 1.

Project Description

The Underline will transform the underutilized space below Miami-Dade's Metrorail from Dadeland South Station to the Miami River (near downtown) into a 10-mile world-class urban trail that connects communities; improves pedestrian and bicyclist safety; encourages a healthy lifestyle; and creates a mobility corridor that integrates transit, car, biking, and walking. The proposed project consists of a 10-foot bicycle path and an 8-foot walking path with connections to eight Metrorail stations and the surrounding neighborhoods along the corridor. The Underline Master Plan features straightened and lit pedestrian and bicycle trails, signature native landscaping, destination park spaces, and recommendations to improve crosswalk safety for the twenty-eight intersections along the corridor.

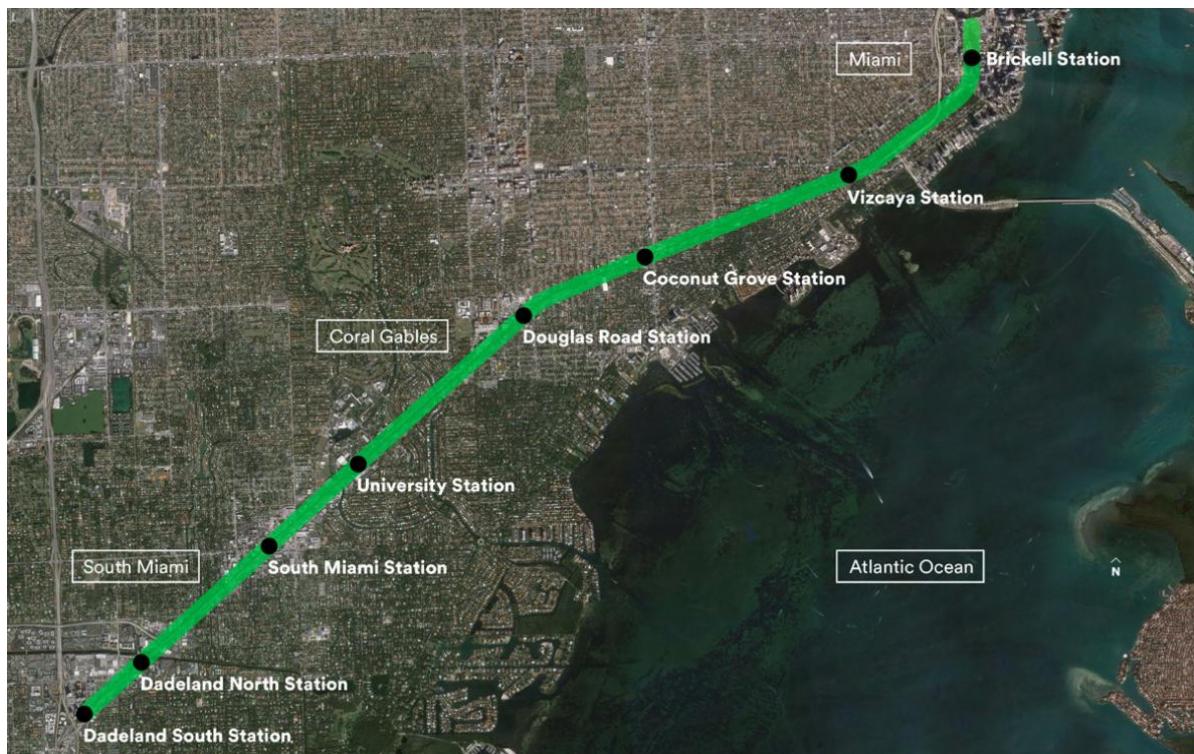


Figure 1. Project Corridor



Figure 2. The Underline

Connections

The map in Figure 3 illustrates the study corridor and shows connections to other Miami-Dade greenway trails. The Underline is the spine of a comprehensive non-motorized transportation system that will provide enhanced opportunities for people to divert from roadways.

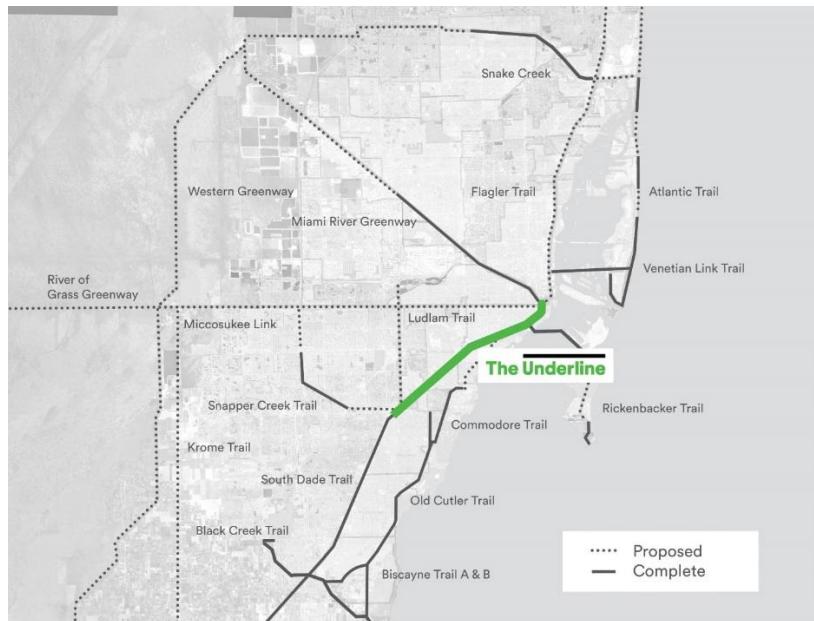


Figure 3. Study Area Map

Study Area Daily Traffic Counts

Daily traffic counts from FDOT's Florida Traffic Online Database form the baseline establishing existing traffic volumes along U.S. 1. Table 1 presents the daily traffic counts that were examined as part of the study area. The project team examined daily traffic counts to establish the annual average daily traffic (AADT) for various roadway segments along U.S. 1, which parallels The Underline and serves similar trip patterns (i.e. – commuting to Brickell, the University of Miami, and also shorter trips within the corridor). Existing published traffic count sites on U.S. 1 between Dadeland South and Brickell were studied to mirror trip patterns on the Underline, which also connects Dadeland South to Brickell. The AADT along U.S. 1 was used as the motor vehicle traffic baseline in the mode shift analysis. The most recent AADT data (2014) from FDOT's database were utilized in this analysis.

Table 1. Daily Traffic Counts Baseline

| Count Site Number | Roadway | Location Description | Annual Average Daily Traffic (AADT) |
|-------------------|---------|---|-------------------------------------|
| 870163 | U.S. 1 | 200' south of SR 878/Snapper Creek Expressway | 52,000 |
| 870164 | U.S. 1 | 200' south of SW 80th Street/Davis Road | 92,500 |
| 870127 | U.S. 1 | 400' east of SW 57th Avenue/Red Road | 79,500 |
| 870178 | U.S. 1 | south of Granada Boulevard | 77,900 |
| 870521 | U.S. 1 | 200' south of Grand Avenue | 72,500 |
| 875037 | U.S. 1 | 200' south of S Miami Avenue | 23,800 |
| 875039 | U.S. 1 | 200' north of Rickenbacker Causeway | 26,500 |
| 875041 | U.S. 1 | 200' south of SE 13 th Street | 23,500 |
| 875042 | U.S. 1 | 200' south of SE 8 th Street | 29,500 |
| 875200 | U.S. 1 | 200' south of SW 27th Avenue/Unity Blvd | 88,000 |
| 875201 | U.S. 1 | 200' north of SW 27th Avenue/Unity Blvd | 82,500 |

Source: FDOT's Florida Traffic Online Database (2014 data)

Background Growth Rate

A background growth rate was calculated based on historic trends at the traffic count stations listed in Table 1. The background growth rate was applied to traffic counts to "modify" the data from present day conditions to represent anticipated traffic conditions in the project's opening year. For this analysis, the project team assumed an opening year of 2019 for a completed Underline system from Dadeland South to Brickell. The opening year represents an estimated timeframe for a completed system in order to examine the impacts of the completed trail on motor vehicle traffic, rather than shorter demonstration projects that may not have a systemwide impact.

Historical traffic counts were examined from FDOT's Florida Traffic Online Database to calculate the background growth rate. Traffic counts from 2004 and 2009 were examined and compared to the 2014 data to calculate both a 10-year and a 5-year growth rate. Data show that traffic volumes have been generally decreasing in the U.S. 1 corridor over the last ten (10) years. Despite this general decline in traffic volumes, the project team assumed a 0.5 percent annual increase in traffic volumes to "grow" the 2014 data to 2019 projected traffic volumes, following a conservative analysis approach. Table 2 summarizes the measured change in traffic volumes over the past ten years and the assumed percentage annual increase in traffic between 2014 and 2019 utilized in this study. Attachment A presents an expanded version of Table 2 showing historical traffic counts.

Table 2. Traffic Growth Rates

| Count Site Number | Roadway | Location Description | 10-Year Historical Growth | 5-Year Historical Growth | Assumed Annual Growth | AADT Opening 2019 |
|-------------------|---------|---|---------------------------|--------------------------|-----------------------|-------------------|
| 870163 | U.S. 1 | 200' south of SR 878/Snapper Creek Expressway | -16.8% | -1.9% | 0.5% | 53,300 |
| 870164 | U.S. 1 | 200' south of SW 80th Street/Davis Road | -6.6% | 18.6% | 1.0% | 97,125 |
| 870127 | U.S. 1 | 400' east of SW 57th Avenue/Red Road | -14.1% | 1.9% | 0.5% | 81,488 |
| 870178 | U.S. 1 | south of Granada Boulevard | -9.7% | -6.7% | 0.5% | 79,848 |
| 870521 | U.S. 1 | 200' south of Grand Avenue | -22.5% | -7.6% | 0.5% | 74,313 |
| 875037 | U.S. 1 | 200' south of S Miami Avenue | 6.3% | -0.8% | 0.5% | 24,395 |
| 875039 | U.S. 1 | 200' north of Rickenbacker Causeway | -7.0% | -10.2% | 0.5% | 27,163 |
| 875041 | U.S. 1 | 200' south of SE 13 th Street | -19.0% | -16.1% | 0.5% | 24,088 |
| 875042 | U.S. 1 | 200' south of SE 8 th Street | -16.9% | -9.2% | 0.5% | 30,238 |
| 875200 | U.S. 1 | 200' south of SW 27th Avenue/Unity Blvd | -14.6% | -4.9% | 0.5% | 90,200 |
| 875201 | U.S. 1 | 200' north of SW 27th Avenue/Unity Blvd | -24.3% | -14.9% | 0.5% | 84,563 |

Source: FDOT's Florida Traffic Online Database (2014 data)

The data presented in Tables 1 and 2 indicate that U.S. 1 traffic is currently operating at level of service F (LOS F) between 200' south of SW 80th Street and 200' north of SW 27th Avenue.

Underline Usage Forecasting

The anticipated volume of users on The Underline was calculated using data from peer facilities. Bicyclist and pedestrian volumes from peer facilities were examined from readily available sources and compared to potential indicator data such as population, density, trail length, adjacent land use, and number of rail station connections.

Table 3. Peer Facility Data

| Peer Facility | Location | Description | Land Use Adjacent to the Trail | Length (miles) | Population Density (persons per sq. mi.) | Non-Motorized Commute Percentage | Daily Trail Users |
|-----------------------------|--------------------|---|---|----------------|--|----------------------------------|-------------------|
| Indianapolis Cultural Trail | Indianapolis, IN | Urban trail with separate paths for bicyclists and pedestrians that forms a loop through downtown, focusing on art and culture | Downtown commercial, restaurants, office, and parks; Trail is mostly in street right-of-way | 8 | 2273 | 2.5% | 3000 |
| Atlanta BeltLine | Atlanta, GA | Greenway trail in abandoned railroad corridor surrounding downtown; 5 miles (in 3 sections) of planned 33 miles have been built | Residential, parks, suburban retail and office; Trail is mostly in separated right-of-way | 5 | 3360 | 5.1% | 3000 |
| The 606 Trail | Chicago, IL | Elevated trail in abandoned railroad corridor that links four Chicago neighborhoods and includes parks, art, and event spaces | Multi-family residential; Trail is elevated with approx. four access points per mile | 3 | 12,750 | 6.9% | 2800 |
| Pinellas Trail | St. Petersburg, FL | Urban rails-to-trails linear park extending from St. Petersburg to Tarpon Springs with overpasses at ten key intersections | Ranges from suburban residential to nature preserves and open space | 38 | 3967 | 2.9% | 2500 |

Sources:<http://indyculturaltrail.org/>; <http://beltline.org/>; <http://www.the606.org/>; <http://www.pinellascounty.org/trailqd/default.htm>; http://www.census.gov/population/metro/data/pop_pro.html

Regression analyses were conducted to forecast Underline usage based on data from the peer facilities presented in Table 3. The R² value is a statistical measure of how close data are to a fitted regression line (as the R² becomes closer to 1.0 the equation represents a better fit for the data). The study team examined the R² value from regression analyses from a combination of variables to determine appropriateness of various equations to describe the data. During the course of running the analyses, two important factors were discovered – (1) using the metric “trail users per mile” performed better than using total trail users and (2) data for the Pinellas Trail were often found to be outliers, possibly because of the significantly longer length of the Pinellas Trail, which creates a small value for “trail users per mile.” Table 4 summarizes the predicted value for daily Underline users from regression analyses.

Table 4. Regression Analyses

| Variables | Predicted Value for Daily Underline Users | R ² Value |
|--|---|----------------------|
| Population Density and Daily Users Per Mile (excluding Pinellas Trail data) | 8678 | 0.9025 |

The analysis showed that population density correlates positively to the number of trail users per mile. The optimum R² value for the statistical analysis occurs when using the population density predictor to estimate daily users per mile, which for the Underline yields a value of 867.8 daily users per mile or 8,678 daily users (10 mile corridor length).

It is anticipated that not all Underline trips will utilize the entire corridor; most trips on the Underline will utilize only a portion of the corridor for each trip. The anticipated Underline usage can be distributed along the corridor by estimating the average trip length. According to data from the 2009 *National Household Travel Survey* (NHTS), the average bicycle trip is approximately 3 miles and the average walking trip is approximately 1 mile. For purposes of this analysis, the study team assumed a 50/50 split between bicycling and walking on the Underline; therefore, the average trip length can be estimated at 2 miles. Since the Underline project is 10 miles long when fully built, on average trips will only utilize 20 percent of the corridor length. Therefore, each point along the corridor can be estimated to carry 20 percent of the 8,678 daily users, or approximately 1,736 trips.

As a reasonableness check, the study team evaluated the anticipated daily volume of 1,736 within the capacity of an 18-foot shared use path, based on FHWA's *Shared Use Path Level of Service Calculator*, and found that The Underline would operate within acceptable levels (LOS B).

Existing M-Path Volume Data

Existing bicyclist and pedestrian counts along the M-Path were collected from the Miami-Dade MPO and examined to determine the baseline existing corridor usage. M-Path usage varies greatly depending on day of the week. In addition, M-Path usage is commonly higher during winter months than summer months. In general, existing counts show that M-Path usage ranges from 145 users per weekday at a temporary count location south of SW 17th Avenue to 263 users per day at a permanent count location north of the Vizcaya Station. Attachment B presents a summary of the existing M-Path

counts at the permanent count station during the period between September 2014 and January 2015, which roughly approximates the time period for which motor vehicle traffic volume data are available. The MPO also collects two-hour peak period counts at SW 57th Avenue (Red Road), although the corresponding daily volume at this location is unknown. Bicyclist volume ranges from 20-30 bicyclists per 2-hour period and pedestrian volume ranges from 30-50 pedestrians per 2-hour period at the SW 57th Avenue site.

Existing motor vehicle count locations on U.S. 1 are more frequent than M-Path usage count locations. In the absence of a consistent set of count data along the M-Path, the study team estimated 200 users per day to approximate an average M-Path count baseline (calculated based on the mathematical average between the SW 17th Avenue count site and the north of Vizcaya Station count site).

Mode Shift Analysis

Measuring the mode shift between automobile traffic and non-motorized traffic caused by the implementation of urban trails can be estimated based on methodologies developed within published literature. Vehicle travel substitution rates (the amount that motor vehicle travel declines due to non-motorized project implementation) involves complex issues including travel behavior, land use context, and social factors. Several studies, including Guo et. al. (2007) and Handy and Clifton (2001), have shown that mode shifts from automobile travel to non-motorized travel due to the implementation of a new facility do not occur at a 1:1 rate.

The Underline is directly adjacent to the U.S. 1/South Dixie Highway urban principal arterial; therefore, the Underline will have the potential to attract motorists from busy U.S. 1 traffic. It is likely that some of The Underline users will be new to the area (several committed developments are located in the corridor), some will be existing non-motorized users on the M-Path, and some will be existing non-motorized users who change travel patterns based on the comfort and convenience of The Underline. Furthermore, some users who choose to walk or bike The Underline may shift from cars at varying rates depending on trip type and trip frequency (i.e. – someone may choose to bike to work on Fridays).

The literature review reveals two primary methods for estimating vehicle travel substitution rates.

- Method 1 – Estimate the percentage of non-motorized transportation trips that are shifted from motor vehicle trips.
- Method 2 – Estimate the percentage of motor vehicle trips that could be replaced by non-motorized transportation modes.

Vehicle substitution rates for The Underline were calculated based on a blend of Methods 1 and 2.

- Method 1 – This method uses published data from the academic journal *Travel Behaviour and Society*. As described in “*Accounting for the Short Term Substitution Effects of Walking and Cycling in Sustainable Transportation*,” Piatkowski et. al. (2014) conducted intercept studies of five urban trail facilities in the U.S. to measure the rate at which utilitarian non-motorized trips substituted for automobile trips. There are many dimensions of the

substitution effect, including trip type, substituting mode, time horizon, and activity patterns. Logistic regression models found that the number of car trips per week and bicycle helmet usage correlated positively with automobile substitution trips. The analysis estimated that the rate at which utilitarian non-motorized trips substituted for automobile trips ranged from 25 percent to 86 percent, with presence of a parallel roadway facility being one of the factors identified as influencing a higher percentage.

Without any direct Miami-Dade substitution data to utilize, the percentage of non-motorized trips that substitute for automobile trips was assumed through indirect inference. Since The Underline will run directly parallel to U.S. 1, Kimley-Horn utilized a substitution rate of 60 percent, which is within the range proposed within the literature without being overly aggressive. An automobile substitution rate of 60 percent of Underline trips accounts for the remaining 40 percent of Underline trips coming from non-substitution events such as new residents, existing M-Path users, and non-motorized users who switch from other corridors. Therefore, 60 percent of The Underline usage forecast presented previously in this report will be assumed to be motor vehicle trip substitution.

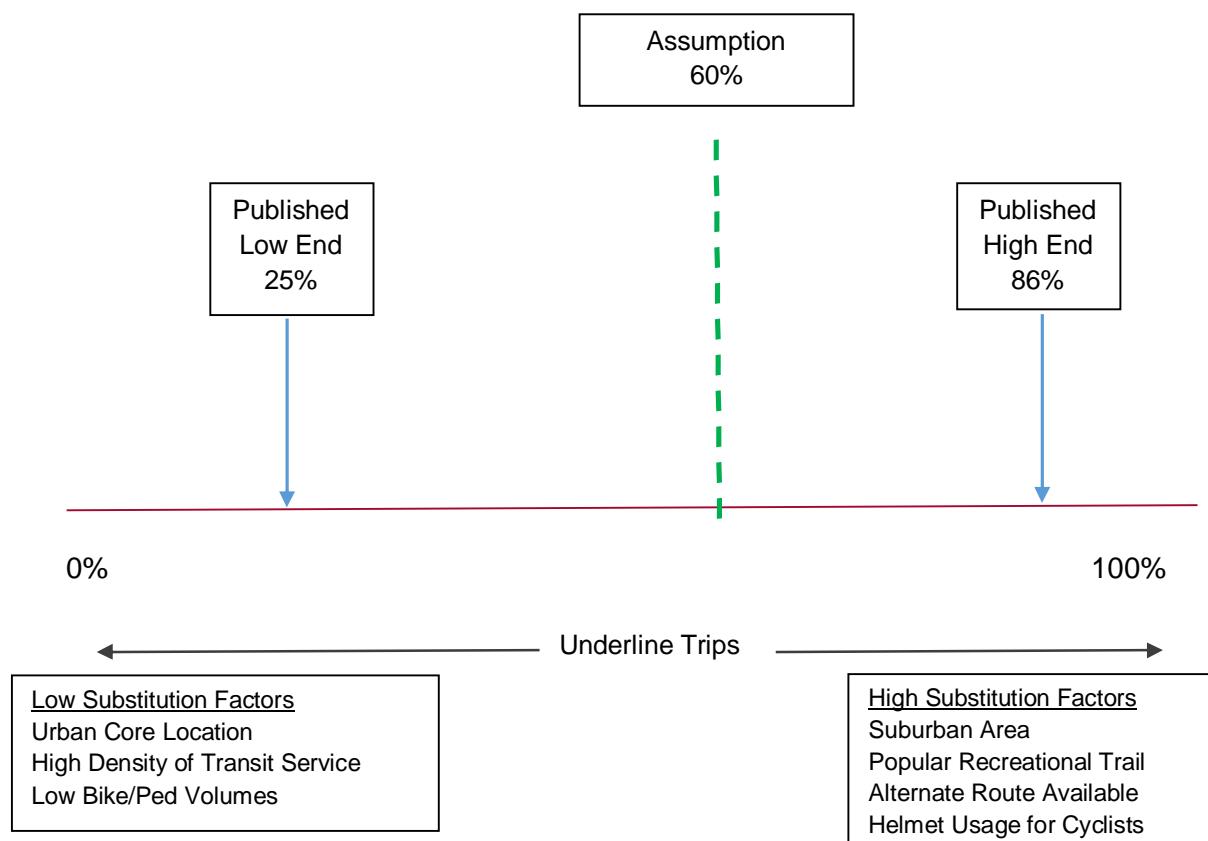


Figure 4. Substitution Percentage for The Underline Compared to Published Data

- Method 2 – Method 2 begins with a known number of driving trips on U.S. 1 (see the count data presented in Tables 1 and 2) and then estimates what fraction of those automobile trips could be replaced by non-motorized trips on The Underline utilizing published data from “*Nonmotorized Transportation Pilot Program Evaluation Study*,” Center for Transportation Studies, University of Minnesota, by Krizek et al. (2007). Recent reports and publications have estimated various benefits of walking and bicycling based on the share of vehicular travel that could be replaced. However, the literature review yielded a limited number of studies quantifying substitution rates, the majority of which indirectly infer the substitution due to problems associated with direct measurements (i.e. – direct questioning). Krizek (2007) found that the implementation of non-motorized travel facilities could reduce automobile travel by 1 percent to 4 percent and could reduce daily driving distance traveled by 0.25 miles per adult.

Krizek (2007) conducted a baseline survey to estimate non-motorized substitution for driving rates. Only utilitarian travel was considered in the estimates of non-motorized substitution for driving. Survey constraints limited the analysis to adult travel, thus chauffeuring of children was not addressed. Work commute and other utilitarian trip distances and daily walk and bike trips per adult were estimated from the five-area pilot survey. A low estimate was prepared on the basis of calculated reference trip distances and a high estimate was drawn from the daily walk and bike travel time totals reported. These steps were followed by survey-based estimation for degree of walk or bike substitution for auto travel. Commuter driving substitution was computed using the ratio of walk or bike commuters listing driving as their alternative travel mode to the total of walk or bike commuters reporting any alternative mode. Across the five communities studied, 32 percent of bicycle commute trips and 36 percent of walk work commute trips were estimated to be driving substitution. Non-commute utilitarian trip driving substitution was higher. Using the same methodology, 93 percent on non-work utilitarian bicycle trips and 95 percent of non-work utilitarian walk trips were estimated to be replacements for driving. The walk and bike modes of travel together were estimated to replace approximately $\frac{1}{4}$ to $\frac{3}{4}$ miles per day of driving per adult resident, depending on urban area characteristics. Present day use of non-motorized transportation modes, in the context of 15 to 25 miles per day of auto travel in the communities studied, thus appears to reduce driving by 1 to 4 percent. Krizek (2007) was republished in 2009 by the Federal Transit Administration (FTA) in *Transit Cooperative Research Program (TCRP) Report 95: Pedestrian and Bicycle Facilities – Traveler Response to Transportation System Changes*.

Guo and Gandavarapu (2010) found that sidewalks reduce automobile travel by 1.142 daily vehicle-miles; furthermore, there is a relationship of approximately 12 miles of reduced driving for each mile of increased non-motorized travel. This implies that non-motorized trips are much shorter than the automobile trips that they replace. Examples of travel behavior that could explain this phenomenon including replacing a longer entertainment trip in a car

with a closer entertainment trip on a bicycle and lifestyle changes that involve choosing to live and work in a corridor where bicycling to work is possible.

Based on the results of the literature review, Kimley-Horn utilized a 1 percent reduction in automobile traffic on U.S. 1 as an estimate for Method 2.

Attachment C presents the analysis for Method 1 applied to The Underline usage forecasts. Attachment D presents the analysis for Method 2 applied to the anticipated U.S. 1 traffic volumes in the assumed opening year of 2019.

The quantitative results of Methods 1 and 2 were compared in a critical analysis, which resulted in a blending or averaging of the two methods to forecast the traffic reduction on U.S. 1 for The Underline. Table 5 presents a summary of the mode shift analysis for The Underline. Attachment E presents an expanded analysis. The amount of motor vehicle traffic reduction on U.S. 1 as a direct result of The Underline is anticipated to range from 643 vehicles per day to 1,007 vehicles per day depending on the location.

Table 5. Motor Vehicle Traffic Volume Reduction as a Result of The Underline

| Count Site Number | Roadway | Location Description | AADT Opening 2019 | Motor Vehicle Reduction | AADT Adjusted 2019 | Percent Reduction in Traffic |
|-------------------|---------|---|-------------------|-------------------------|--------------------|------------------------------|
| 870163 | U.S. 1 | 200' south of SR 878/Snapper Creek Expressway | 53,300 | 788 | 52,513 | -1.48% |
| 870164 | U.S. 1 | 200' south of SW 80th Street/Davis Road | 97,125 | 1,007 | 96,118 | -1.04% |
| 870127 | U.S. 1 | 400' east of SW 57th Avenue/Red Road | 81,488 | 928 | 80,559 | -1.14% |
| 870178 | U.S. 1 | south of Granada Boulevard | 79,848 | 920 | 78,927 | -1.15% |
| 870521 | U.S. 1 | 200' south of Grand Avenue | 74,313 | 893 | 73,420 | -1.20% |
| 875037 | U.S. 1 | 200' south of S Miami Avenue | 24,395 | 643 | 23,752 | -2.64% |
| 875039 | U.S. 1 | 200' north of Rickenbacker Causeway | 27,163 | 657 | 26,506 | -2.42% |
| 875041 | U.S. 1 | 200' south of SE 13 th Street | 24,088 | 641 | 23,446 | -2.66% |
| 875042 | U.S. 1 | 200' south of SE 8 th Street | 30,238 | 672 | 29,565 | -2.22% |
| 875200 | U.S. 1 | 200' south of SW 27th Avenue/Unity Blvd | 90,200 | 972 | 89,228 | -1.08% |
| 875201 | U.S. 1 | 200' north of SW 27th Avenue/Unity Blvd | 84,563 | 944 | 83,619 | -1.12% |

Source: FDOT's Florida Traffic Online Database; Kimley-Horn and Associates, Inc.

Intersection Data Collection

A.M. (7:00-9:00 A.M.) and P.M. (4:00-6:00 P.M.) peak hour turning movement counts were collected at five (5) study intersections identified during the methodology phase. Turning movement counts were collected in 15-minute intervals during the peak periods. Attachment F includes the traffic count data collected at the five study intersections. The following intersections were examined as part of this study.

- US 1/South Dixie Highway and SW 88th Street/Kendall Drive
- US 1/South Dixie Highway and SW 72nd Street/Sunset Drive
- US 1/South Dixie Highway and SW 40th Street/Bird Road
- US 1/South Dixie Highway and SW 27th Avenue/Unity Boulevard
- US 1/Brickell Avenue and SE 26th Street

Intersection traffic counts were adjusted to peak season conditions using the appropriate Florida Department of Transportation (FDOT) peak season conversion factor (PSCF), which was identified to be 1.01 for the week of February 3. Signal timing information was obtained from Miami-Dade County Signals and Signs Division.

As discussed in the Background Growth Rate section of this report, the project team assumed a background growth rate of 0.5% per year, despite actual traffic volumes on U.S. 1 experiencing a general decline over the previous 5-year and 10-year periods according to FDOT traffic count data. The assumption of 0.5% per year provides for a conservative analysis. Attachment G presents the traffic volume development sheets at the study intersections.

Intersection Capacity Analysis

Intersection capacity analyses were conducted for the weekday A.M. and P.M. peak hours at the five study intersections. Intersection analyses were performed using Trafficware's *Synchro 8.0* traffic engineering analysis software, which applies Highway Capacity Manual (HCM) 2000 and 2010 methodologies.

Capacity analyses were conducted for three (3) scenarios: existing (2016); build-out year (2019) background without project; and build-out year (2019) total with project. The purpose of the intersection capacity analysis is to determine the reduction in automobile delay at each intersection based on the implementation of the project. The assumed background growth rate of 0.5% per year was used to convert the existing (2016) data to build-out year (2019). To account for the project, the percent traffic reduction for The Underline established in Table 5 was applied only to U.S. 1 through movements for purposes of the intersection capacity analysis in the build-out year (2019) with project. The percent reduction at the closest AADT count station was applied to each intersection. The percent reduction for the SW 27th Avenue intersection was averaged between the two equally adjacent AADT count stations 200 feet north and 200 feet south of the intersection. Attachment H presents the results of the *Synchro 8.0* traffic engineering analysis for intersection capacity.

Tables 6 through 8 present the percent reduction in delay for each intersection, as well as the northbound U.S. 1 and southbound U.S. 1 approach delay during the A.M. peak and P.M. peak periods. The results vary by intersection and by time of day within a range up to -3.89% reduction in

intersection delay. Approach delay varies up to a maximum reduction of -5.63% at the SW 72nd Street (Sunset Drive) intersection during the A.M. peak period. The results demonstrate that The Underline is anticipated to reduce intersection delay at the signalized intersections studied.

Table 6. Intersection Delay Comparison

A.M. Peak

| | 2019 w/o project | 2019 with project | Percent Change |
|----------------|----------------------------------|----------------------------------|----------------|
| | Overall Intersection Delay (sec) | Overall Intersection Delay (sec) | |
| SW 88th Street | 50.1 | 50.0 | -0.20% |
| SW 72nd Street | 56.6 | 54.4 | -3.89% |
| SW 40th Street | 52.1 | 51.9 | -0.38% |
| SW 27th Avenue | 48.5 | 48.6 | 0.21% |
| SW 26th Road | 35.5 | 35.2 | -0.85% |

P.M. Peak

| | 2019 w/o project | 2019 with project | Percent Change |
|----------------|----------------------------------|----------------------------------|----------------|
| | Overall Intersection Delay (sec) | Overall Intersection Delay (sec) | |
| SW 88th Street | 51.6 | 51.5 | -0.19% |
| SW 72nd Street | 40.4 | 39.9 | -1.24% |
| SW 40th Street | 37.3 | 37.3 | 0.00% |
| SW 27th Avenue | 38.4 | 38.1 | -0.78% |
| SW 26th Road | 34.6 | 34.5 | -0.29% |

Table 7. Northbound U.S. 1 Approach Delay Comparison

A.M. Peak

| | 2019 w/o project | 2019 with project | Percent Change |
|----------------|-------------------------------------|-------------------------------------|-----------------------|
| | Northbound U.S. 1 Delay (sec) | Northbound U.S. 1 Delay (sec) | |
| SW 88th Street | 56.1 | 56.2 | 0.18% |
| SW 72nd Street | 69.3 | 65.4 | -5.63% |
| SW 40th Street | 33.3 | 32.4 | -2.70% |
| SW 27th Avenue | 15.5 | 15.2 | -1.94% |
| SW 26th Road | 39.3 | 38.1 | -3.05% |

P.M. Peak

| | 2019 w/o project | 2019 with project | Percent Change |
|----------------|-------------------------------------|-------------------------------------|-----------------------|
| | Northbound U.S. 1 Delay (sec) | Northbound U.S. 1 Delay (sec) | |
| SW 88th Street | 58.6 | 58.4 | -0.34% |
| SW 72nd Street | 32.9 | 32.2 | -2.13% |
| SW 40th Street | 23.6 | 23.3 | -1.27% |
| SW 27th Avenue | 24.1 | 23.7 | -1.66% |
| SW 26th Road | 39.3 | 38.8 | -1.27% |

Table 8. Southbound U.S. 1 Approach Delay Comparison

A.M. Peak

| | 2019 w/o project | 2019 with project | Percent Change |
|----------------|-------------------------------------|-------------------------------------|-----------------------|
| | Southbound U.S. 1 Delay (sec) | Southbound U.S. 1 Delay (sec) | |
| SW 88th Street | 32.6 | 32.5 | -0.31% |
| SW 72nd Street | 21.3 | 21.1 | -0.94% |
| SW 40th Street | 22.7 | 22.3 | -1.76% |
| SW 27th Avenue | 21.6 | 21.1 | -2.31% |
| SW 26th Road | 27.7 | 27.8 | 0.36% |

P.M. Peak

| | 2019 w/o project | 2019 with project | Percent Change |
|----------------|-------------------------------------|-------------------------------------|-----------------------|
| | Southbound U.S. 1 Delay (sec) | Southbound U.S. 1 Delay (sec) | |
| SW 88th Street | 41.7 | 41.8 | 0.24% |
| SW 72nd Street | 29.7 | 28.9 | -2.69% |
| SW 40th Street | 21.4 | 21.3 | -0.47% |
| SW 27th Avenue | 26.7 | 26.2 | -1.87% |
| SW 26th Road | 33.9 | 33.8 | -0.29% |

Transit Ridership

It is likely that a component of the anticipated Underline usage will be non-motorized users who are connecting to one of the Metrorail Stations along the corridor. Peer facilities were examined for connections to rail transit; however, it was found that the peer facilities studied did not include direct connections to rail transit. The Underline corridor is unique in that rail transit still exists in the corridor where The Underline will be built. Many of the peer facilities (including the 606 Trail and the Atlanta BeltLine) exist in former railroad corridors that no longer carry train traffic.

Therefore, estimation of transit ridership increase is speculative. For example, if 25 percent of the anticipated 8,678 daily users connect to Metrorail, this would represent a Metrorail ridership increase of 2,170 passengers per day, which would be an increase of 2.8 percent above existing Metrorail ridership of approximately 77,000 passengers per weekday. Connections to Metrorail will likely be much higher on weekdays than weekends.

Summary

The Underline Miami-Dade Road Impact Fee Traffic Study measures the potential impact of The Underline on U.S. 1 traffic volumes. Most of U.S. 1 adjacent to The Underline currently operates at level of service F (LOS F). The usage forecasting analysis shows that approximately 8,600 trips per day are anticipated to be served on The Underline; an average of approximately 1,700 Underline users per day are anticipated at individual locations along the corridor.

The Underline improves traffic conditions on U.S. 1 by providing a highly attractive non-motorized transportation alternative to congested travel conditions on U.S. 1, along with direct connections to eight Miami-Dade Metrorail Stations, which ultimately will reduce traffic volumes on U.S. 1. The amount of motor vehicle traffic reduction on U.S. 1 as a direct result of The Underline is anticipated to range from 643 vehicles per day to 1,007 vehicles per day depending on the location along the corridor. The percentage reduction in traffic volumes on U.S. 1 as a direct result of The Underline is anticipated to range from -1.04% to -2.66%.

Intersection capacity analyses conducted at five intersections demonstrate that The Underline is anticipated to result in delay reductions at intersections of up to -3.89% for total intersection delay in the A.M. peak period at the SW 72nd Street intersection. Northbound and southbound traffic approaches on U.S. 1 are anticipated to receive direct delay reduction benefits since The Underline parallels these movements. Individual approach delays are anticipated to range up to -5.63%.

List of Attachments

- Attachment A – Annual average daily traffic (AADT) data and opening year AADT calculation
- Attachment B – M-Path trail counter report
- Attachment C – Method 1 motor vehicle substitution calculations
- Attachment D – Method 2 motor vehicle reduction calculations
- Attachment E – Blended average of traffic reduction methodologies
- Attachment F – Intersection traffic counts
- Attachment G – Volume development sheets
- Attachment H – Intersection capacity analysis

Attachment A

Attachment A. Annual Average Daily Traffic (AADT) Data and Opening Year Background AADT Calculation

| Count Site Number | Roadway | Location Description | AADT 2004 | AADT 2009 | AADT 2014 | 10-Year Historical Growth | 5-Year Historical Growth | Annual Growth Rate | AADT Opening 2019 |
|-------------------|---------|---|-----------|-----------|-----------|---------------------------|--------------------------|--------------------|-------------------|
| 870163 | U.S. 1 | 200' south of SR 878/Snapper Creek Expressway | 62,500 | 53,000 | 52,000 | -16.8% | -1.9% | 0.5% | 53,300 |
| 870164 | U.S. 1 | 200' south of SW 80th Street/Davis Road | 99,000 | 78,000 | 92,500 | -6.6% | 18.6% | 1.0% | 97,125 |
| 870127 | U.S. 1 | 400' east of SW 57th Avenue/Red Road | 92,500 | 78,000 | 79,500 | -14.1% | 1.9% | 0.5% | 81,488 |
| 870178 | U.S. 1 | south of Granada Boulevard | 86,300 | 83,500 | 77,900 | -9.7% | -6.7% | 0.5% | 79,848 |
| 870521 | U.S. 1 | 200' south of Grand Avenue | 93,500 | 78,500 | 72,500 | -22.5% | -7.6% | 0.5% | 74,313 |
| 875037 | U.S. 1 | 200' south of S Miami Avenue | 22,400 | 24,000 | 23,800 | 6.3% | -0.8% | 0.5% | 24,395 |
| 875039 | U.S. 1 | 200' north of Rickenbacker Causeway | 28,500 | 29,500 | 26,500 | -7.0% | -10.2% | 0.5% | 27,163 |
| 875041 | U.S. 1 | 200' south of SE 13 th Street | 29,000 | 28,000 | 23,500 | -19.0% | -16.1% | 0.5% | 24,088 |
| 875042 | U.S. 1 | 200' south of SE 8 th Street | 35,500 | 32,500 | 29,500 | -16.9% | -9.2% | 0.5% | 30,238 |
| 875200 | U.S. 1 | 200' south of SW 27th Avenue/Unity Blvd | 103,000 | 92,500 | 88,000 | -14.6% | -4.9% | 0.5% | 90,200 |
| 875201 | U.S. 1 | 200' north of SW 27th Avenue/Unity Blvd | 109,000 | 97,000 | 82,500 | -24.3% | -14.9% | 0.5% | 84,563 |

Source: FDOT's Florida Traffic Online Database

Attachment B

M-Path Trail Counter Data Report

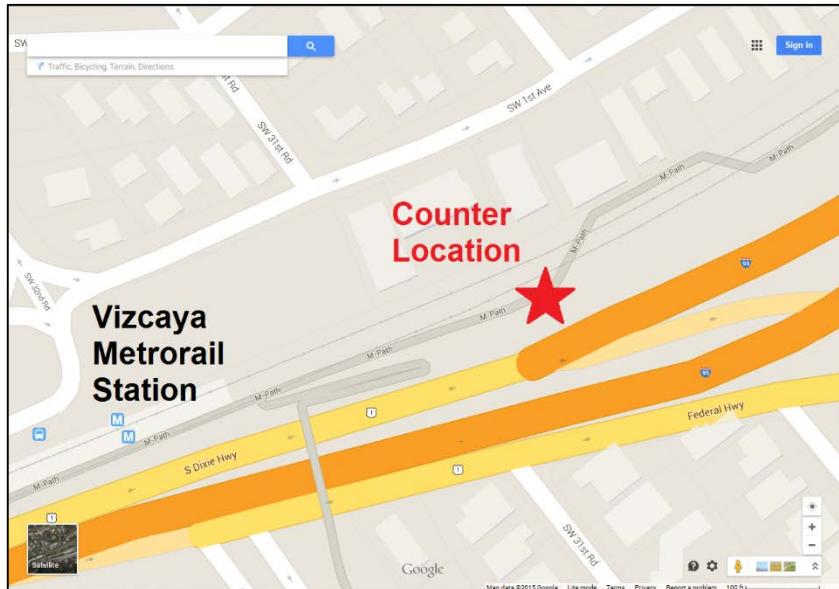
January, 2015

Background

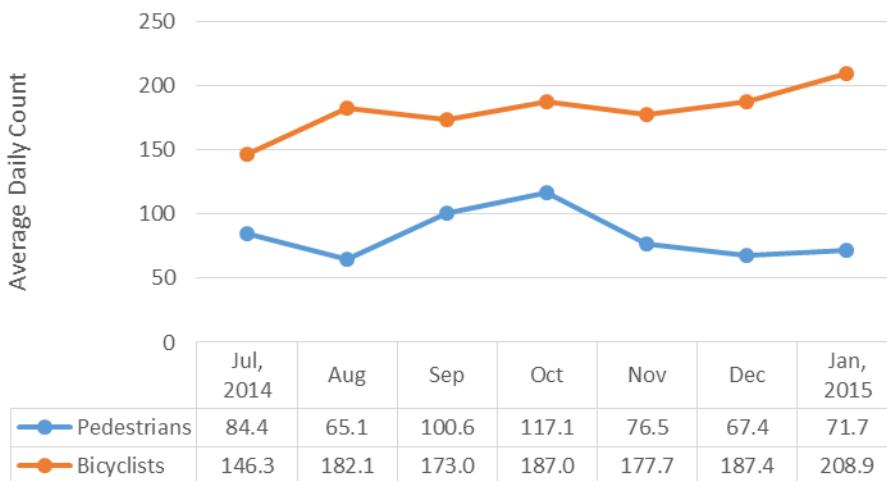
The Rails-to-Trails Conservancy (RTC) has installed a trail counter on the M-Path at the Vizcaya Metrorail Station June, 2014, to support their Trail Modeling and Assessment Program (T-MAP) project. The counter combines passive infrared and inductive loop technology to collect bicycle and pedestrian data directionally and by 15-minute period. Data is uploaded automatically each day to the Eco-visio data management platform.

Data

Data from the counter is available from July 1, 2014. The total counts to date are over 17,000 pedestrians and 36,000 bicyclists.



M-Path Average Daily Count



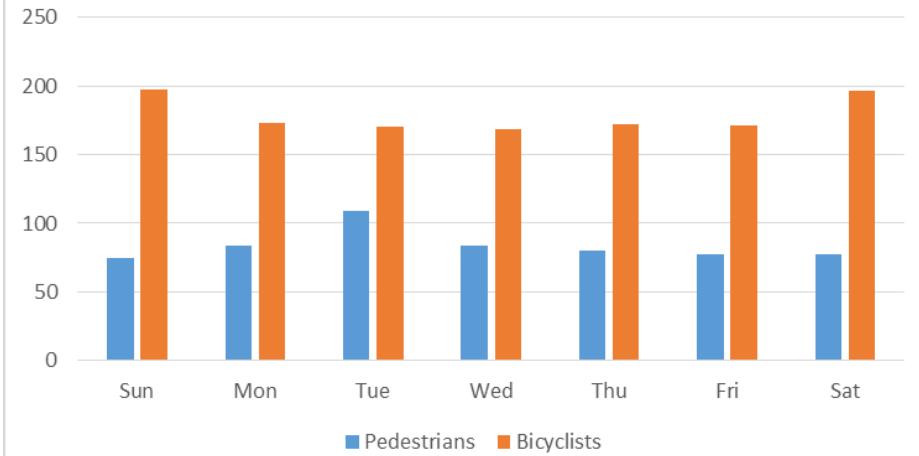
Monthly Volume

The M-Path is consistently used by more bicyclists than pedestrians. Average daily counts over this period are 179 bicyclists and 84 pedestrians. Bicycle counts have risen through the late summer and early winter. Pedestrian use in this period has been generally consistent with a peak in the early fall.

Weekday Volume

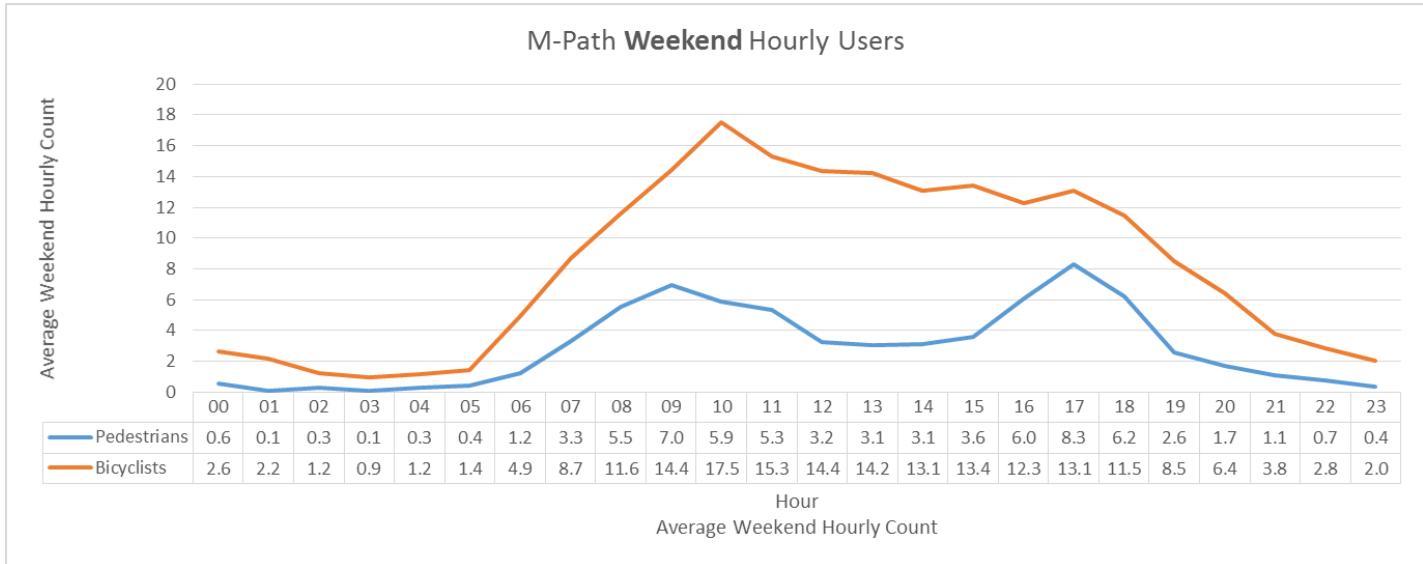
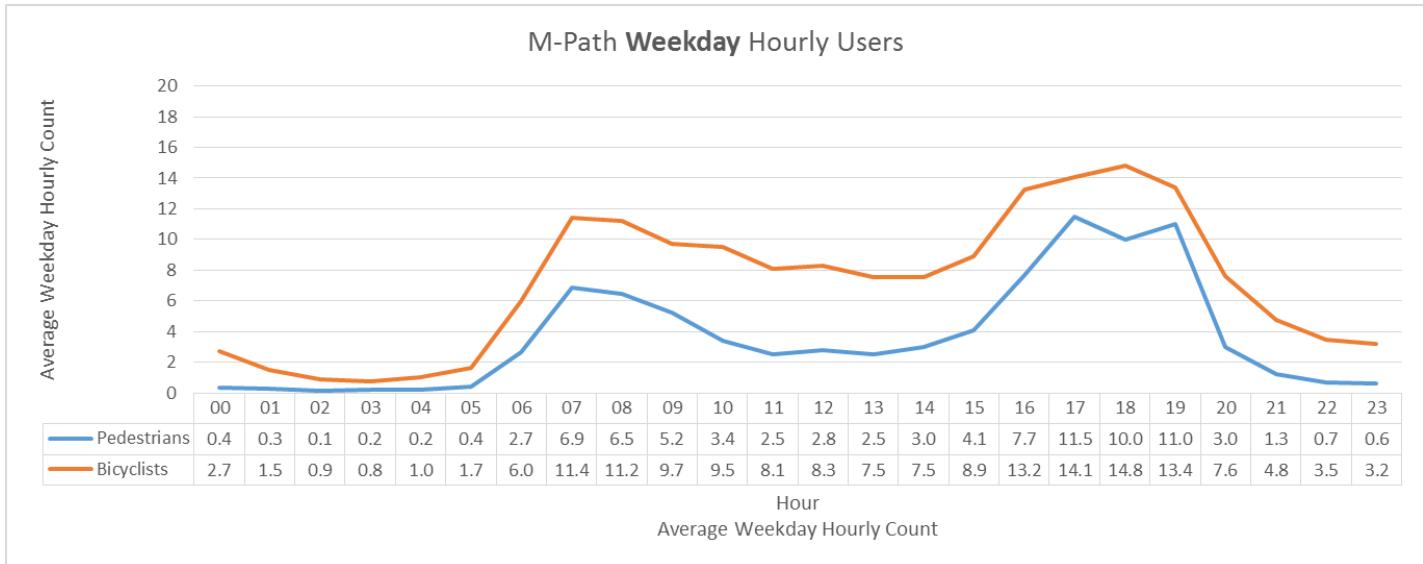
The average bicycle counts on the M-Path are higher on weekends and consistent during the weekdays. The pedestrian counts are generally consistent through the week with a peak on Tuesdays.

M-Path Average Weekday Count



Hourly Volume Profiles

The M-Path weekday average hourly count profile has clear morning and evening peaks for both bicyclists and pedestrians. On weekends, bicycle use peaks in late morning and tapers slowly throughout the daylight hours and more quickly in the evening. The weekend pedestrian count profile has moderate morning and evening peaks. On weekdays and weekends there is bicycle use late into the evening.



Attachment C

Attachment C. Method 1 Calculations

| Count Site Number | Roadway | Location Description | AADT 2014 | AADT Opening 2019 | Underline Volume | Vehicle Substitution | Motor Vehicle Reduction | AADT Adjusted 2019 |
|-------------------|---------|---|-----------|-------------------|------------------|----------------------|-------------------------|--------------------|
| 870163 | U.S. 1 | 200' south of SR 878/Snapper Creek Expressway | 52,000 | 53,300 | 1,736 | 60% | 1,042 | 52,258 |
| 870164 | U.S. 1 | 200' south of SW 80th Street/Davis Road | 92,500 | 97,125 | 1,736 | 60% | 1,042 | 96,083 |
| 870127 | U.S. 1 | 400' east of SW 57th Avenue/Red Road | 79,500 | 81,488 | 1,736 | 60% | 1,042 | 80,446 |
| 870178 | U.S. 1 | south of Granada Boulevard | 77,900 | 79,848 | 1,736 | 60% | 1,042 | 78,806 |
| 870521 | U.S. 1 | 200' south of Grand Avenue | 72,500 | 74,313 | 1,736 | 60% | 1,042 | 73,271 |
| 875037 | U.S. 1 | 200' south of S Miami Avenue | 23,800 | 24,395 | 1,736 | 60% | 1,042 | 23,353 |
| 875039 | U.S. 1 | 200' north of Rickenbacker Causeway | 26,500 | 27,163 | 1,736 | 60% | 1,042 | 26,121 |
| 875041 | U.S. 1 | 200' south of SE 13 th Street | 23,500 | 24,088 | 1,736 | 60% | 1,042 | 23,046 |
| 875042 | U.S. 1 | 200' south of SE 8 th Street | 29,500 | 30,238 | 1,736 | 60% | 1,042 | 29,196 |
| 875200 | U.S. 1 | 200' south of SW 27th Avenue/Unity Blvd | 88,000 | 90,200 | 1,736 | 60% | 1,042 | 89,158 |
| 875201 | U.S. 1 | 200' north of SW 27th Avenue/Unity Blvd | 82,500 | 84,563 | 1,736 | 60% | 1,042 | 83,521 |

Source: FDOT's Florida Traffic Online Database; Kimley-Horn and Associates, Inc.

Attachment D

Attachment D. Method 2 Calculations

| Count Site Number | Roadway | Location Description | AADT 2014 | AADT Opening 2019 | Vehicle Reduction | Motor Vehicle Reduction | AADT Adjusted 2019 |
|-------------------|---------|---|-----------|-------------------|-------------------|-------------------------|--------------------|
| 870163 | U.S. 1 | 200' south of SR 878/Snapper Creek Expressway | 52,000 | 53,300 | 1% | 533 | 52,767 |
| 870164 | U.S. 1 | 200' south of SW 80th Street/Davis Road | 92,500 | 97,125 | 1% | 971 | 96,154 |
| 870127 | U.S. 1 | 400' east of SW 57th Avenue/Red Road | 79,500 | 81,488 | 1% | 815 | 80,673 |
| 870178 | U.S. 1 | south of Granada Boulevard | 77,900 | 79,848 | 1% | 798 | 79,049 |
| 870521 | U.S. 1 | 200' south of Grand Avenue | 72,500 | 74,313 | 1% | 743 | 73,569 |
| 875037 | U.S. 1 | 200' south of S Miami Avenue | 23,800 | 24,395 | 1% | 244 | 24,151 |
| 875039 | U.S. 1 | 200' north of Rickenbacker Causeway | 26,500 | 27,163 | 1% | 272 | 26,891 |
| 875041 | U.S. 1 | 200' south of SE 13 th Street | 23,500 | 24,088 | 1% | 241 | 23,847 |
| 875042 | U.S. 1 | 200' south of SE 8 th Street | 29,500 | 30,238 | 1% | 302 | 29,935 |
| 875200 | U.S. 1 | 200' south of SW 27th Avenue/Unity Blvd | 88,000 | 90,200 | 1% | 902 | 89,298 |
| 875201 | U.S. 1 | 200' north of SW 27th Avenue/Unity Blvd | 82,500 | 84,563 | 1% | 846 | 83,717 |

Source: FDOT's Florida Traffic Online Database; Kimley-Horn and Associates, Inc.

Attachment E

Attachment E. Blended Average of Traffic Reduction Methodologies

| Count Site Number | Roadway | Location Description | AADT 2014 | AADT Opening 2019 | Method 1 Reduction | Method 2 Reduction | Blended Average Reduction | AADT Adjusted 2019 | Percent Reduction in Traffic due to The Underline |
|-------------------|---------|---|-----------|-------------------|--------------------|--------------------|---------------------------|--------------------|---|
| 870163 | U.S. 1 | 200' south of SR 878/Snapper Creek Expressway | 52,000 | 53,300 | 1,042 | 533 | 788 | 52,513 | -1.48% |
| 870164 | U.S. 1 | 200' south of SW 80th Street/Davis Road | 92,500 | 97,125 | 1,042 | 971 | 1,007 | 96,118 | -1.04% |
| 870127 | U.S. 1 | 400' east of SW 57th Avenue/Red Road | 79,500 | 81,488 | 1,042 | 815 | 928 | 80,559 | -1.14% |
| 870178 | U.S. 1 | south of Granada Boulevard | 77,900 | 79,848 | 1,042 | 798 | 920 | 78,927 | -1.15% |
| 870521 | U.S. 1 | 200' south of Grand Avenue | 72,500 | 74,313 | 1,042 | 743 | 893 | 73,420 | -1.20% |
| 875037 | U.S. 1 | 200' south of S Miami Avenue | 23,800 | 24,395 | 1,042 | 244 | 643 | 23,752 | -2.64% |
| 875039 | U.S. 1 | 200' north of Rickenbacker Causeway | 26,500 | 27,163 | 1,042 | 272 | 657 | 26,506 | -2.42% |
| 875041 | U.S. 1 | 200' south of SE 13 th Street | 23,500 | 24,088 | 1,042 | 241 | 641 | 23,446 | -2.66% |
| 875042 | U.S. 1 | 200' south of SE 8 th Street | 29,500 | 30,238 | 1,042 | 302 | 672 | 29,565 | -2.22% |
| 875200 | U.S. 1 | 200' south of SW 27th Avenue/Unity Blvd | 88,000 | 90,200 | 1,042 | 902 | 972 | 89,228 | -1.08% |
| 875201 | U.S. 1 | 200' north of SW 27th Avenue/Unity Blvd | 82,500 | 84,563 | 1,042 | 846 | 944 | 83,619 | -1.12% |

Source: FDOT's Florida Traffic Online Database; Kimley-Horn and Associates, Inc.

Attachment F

Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

SW 88TH STREET & US 1

Delray Beach, Florida 33483

Start Date: 02/03/16

KENDALL, FLORIDA

Phone (561) 272-3255

File I.D. : 88ST_US1

COUNTED BY: I. GONZALEZ & D. GONZALEZ

Page : 1

SIGNALIZED

ALL VEHICLES

| US 1 | | | | SW 88TH STREET | | | | US 1 | | | | SW 88TH STREET | | | | | | | | |
|-----------------------|------|------|-------|----------------|------|------|-------|------------|------|------|-------|----------------|------|------|-------|-------|------|------|-----|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total | | | | |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | | | | |
| 07:00 | 1 | 14 | 154 | 53 | | 0 | 14 | 59 | 8 | | 0 | 0 | 364 | 13 | | 0 | 101 | 131 | 1 | 913 |
| 07:15 | 0 | 25 | 208 | 82 | | 0 | 13 | 57 | 9 | | 0 | 0 | 278 | 29 | | 0 | 112 | 125 | 0 | 938 |
| 07:30 | 0 | 32 | 260 | 110 | | 0 | 13 | 76 | 8 | | 0 | 0 | 298 | 26 | | 0 | 94 | 80 | 7 | 1004 |
| 07:45 | 0 | 35 | 210 | 96 | | 0 | 23 | 94 | 13 | | 0 | 0 | 306 | 15 | | 0 | 131 | 55 | 5 | 983 |
| Hr Total | 1 | 106 | 832 | 341 | | 0 | 63 | 286 | 38 | | 0 | 0 | 1246 | 83 | | 0 | 438 | 391 | 13 | 3838 |
| 08:00 | 0 | 32 | 273 | 107 | | 0 | 19 | 56 | 9 | | 0 | 0 | 356 | 20 | | 0 | 129 | 106 | 11 | 1118 |
| 08:15 | 1 | 18 | 246 | 92 | | 0 | 19 | 63 | 10 | | 0 | 0 | 299 | 22 | | 0 | 123 | 102 | 11 | 1006 |
| 08:30 | 4 | 20 | 266 | 99 | | 0 | 24 | 91 | 13 | | 0 | 0 | 271 | 18 | | 0 | 129 | 101 | 9 | 1045 |
| 08:45 | 3 | 19 | 290 | 99 | | 1 | 22 | 73 | 15 | | 0 | 0 | 349 | 24 | | 0 | 90 | 84 | 6 | 1075 |
| Hr Total | 8 | 89 | 1075 | 397 | | 1 | 84 | 283 | 47 | | 0 | 0 | 1275 | 84 | | 0 | 471 | 393 | 37 | 4244 |
| ----- * BREAK * ----- | | | | | | | | | | | | | | | | | | | | |
| 16:00 | 5 | 13 | 427 | 158 | | 0 | 26 | 121 | 15 | | 0 | 0 | 313 | 28 | | 1 | 151 | 83 | 40 | 1381 |
| 16:15 | 2 | 13 | 489 | 171 | | 0 | 27 | 110 | 7 | | 0 | 0 | 283 | 32 | | 0 | 134 | 108 | 49 | 1425 |
| 16:30 | 3 | 20 | 440 | 153 | | 1 | 26 | 140 | 15 | | 0 | 0 | 273 | 41 | | 0 | 127 | 113 | 22 | 1374 |
| 16:45 | 0 | 18 | 401 | 153 | | 0 | 32 | 141 | 10 | | 0 | 0 | 272 | 25 | | 0 | 121 | 97 | 77 | 1347 |
| Hr Total | 10 | 64 | 1757 | 635 | | 1 | 111 | 512 | 47 | | 0 | 0 | 1141 | 126 | | 1 | 533 | 401 | 188 | 5527 |
| 17:00 | 4 | 22 | 486 | 138 | | 0 | 43 | 139 | 9 | | 0 | 0 | 357 | 33 | | 0 | 83 | 104 | 123 | 1541 |
| 17:15 | 5 | 25 | 459 | 166 | | 0 | 22 | 86 | 14 | | 0 | 0 | 300 | 28 | | 0 | 125 | 155 | 167 | 1552 |
| 17:30 | 7 | 25 | 424 | 168 | | 1 | 28 | 145 | 8 | | 0 | 0 | 300 | 27 | | 0 | 119 | 110 | 108 | 1470 |
| 17:45 | 4 | 19 | 452 | 167 | | 0 | 47 | 119 | 8 | | 0 | 0 | 380 | 36 | | 0 | 119 | 84 | 88 | 1523 |
| Hr Total | 20 | 91 | 1821 | 639 | | 1 | 140 | 489 | 39 | | 0 | 0 | 1337 | 124 | | 0 | 446 | 453 | 486 | 6086 |
| *TOTAL* | 39 | 350 | 5485 | 2012 | | 3 | 398 | 1570 | 171 | | 0 | 0 | 4999 | 417 | | 1 | 1888 | 1638 | 724 | 19695 |

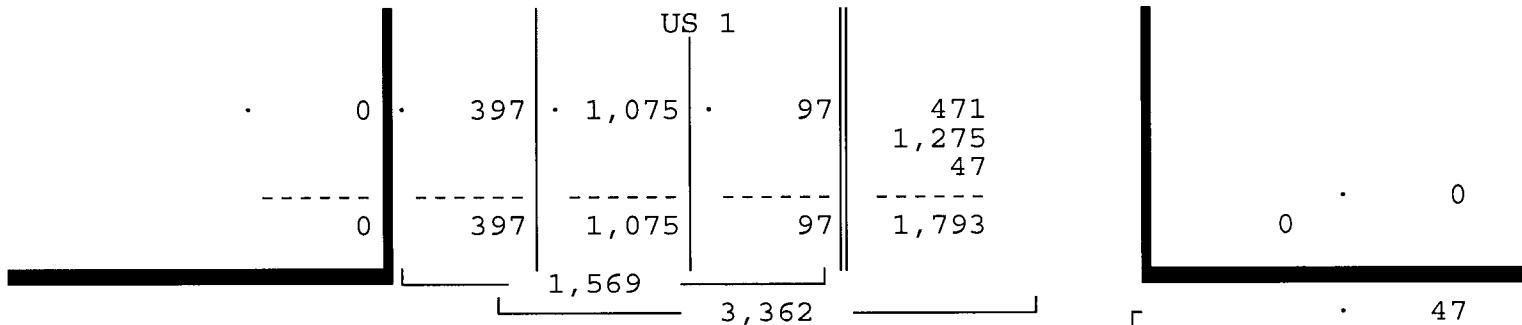
SW 88TH STREET & US 1
KENDALL, FLORIDA
COUNTED BY: I. GONZALEZ & D. GONZALEZ
SIGNALIZED

Traffic Survey Specialists, Inc.
85 SE 4th Avenue, Unit 109
Delray Beach, Florida 33483
Phone (561) 272-3255

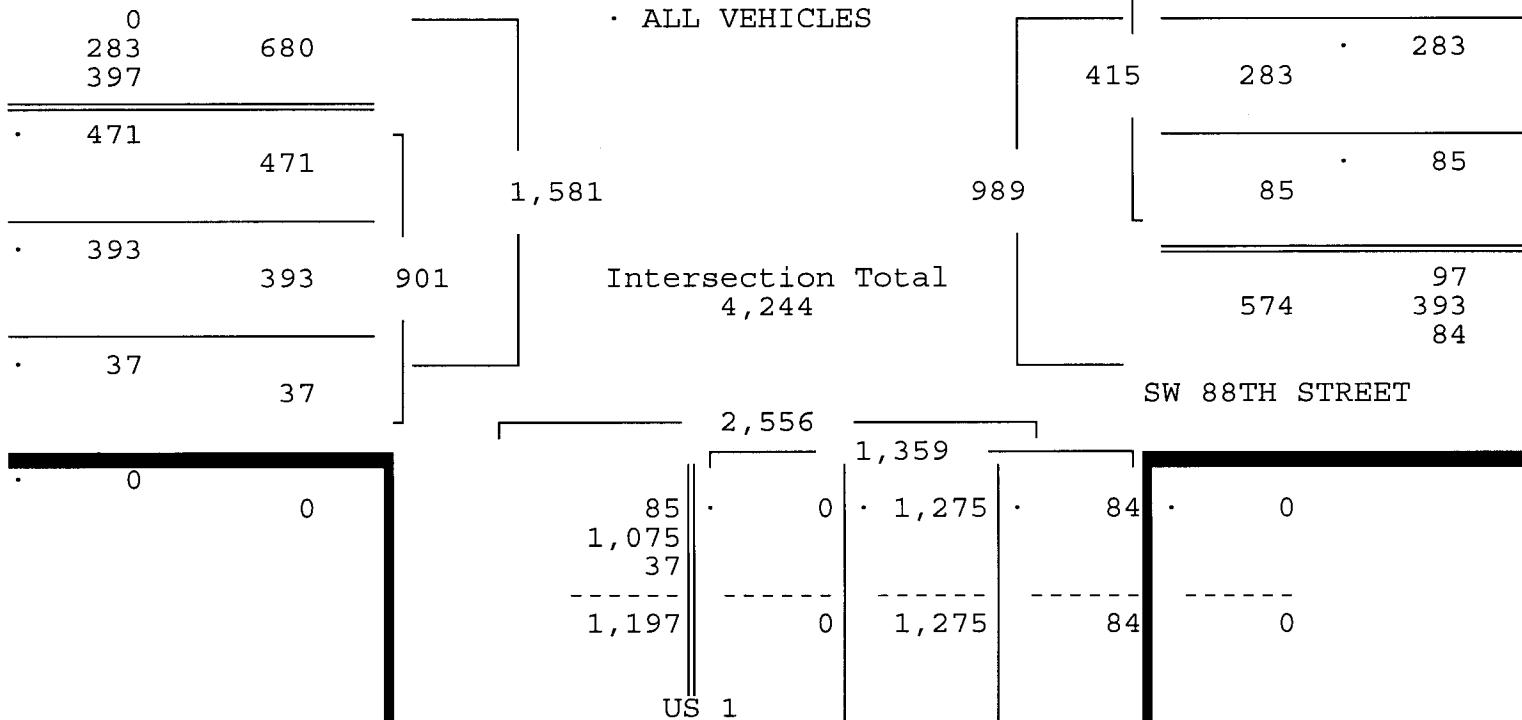
Site Code : 00160031
Start Date: 02/03/16
File I.D. : 88ST_US1
Page : 2

ALL VEHICLES

| US 1 | | | | SW 88TH STREET | | | | US 1 | | | | SW 88TH STREET | | | | |
|--|-------|------|-------|----------------|------|------|-------|------------|------|-------|-------|----------------|------|------|-------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 07:00 to 09:00 on 02/03/16 | | | | | | | | | | | | | | | | |
| Peak start 08:00 | | | | 08:00 | | | | 08:00 | | | | 08:00 | | | | |
| Volume | 8 | 89 | 1075 | 397 | 1 | 84 | 283 | 47 | 0 | 0 | 1275 | 84 | 0 | 471 | 393 | 37 |
| Percent | 1% | 6% | 69% | 25% | 0% | 20% | 68% | 11% | 0% | 0% | 94% | 6% | 0% | 52% | 44% | 4% |
| Pk total | 1569 | | | 415 | | | 1359 | | | 901 | | | | | | |
| Highest | 08:00 | | | 08:30 | | | 08:00 | | | 08:00 | | | | | | |
| Volume | 0 | 32 | 273 | 107 | 0 | 24 | 91 | 13 | 0 | 0 | 356 | 20 | 0 | 129 | 106 | 11 |
| Hi total | 412 | | | 128 | | | 376 | | | 246 | | | | | | |
| PHF | .95 | | | .81 | | | .90 | | | .92 | | | | | | |



SW 88TH STREET



Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

SW 88TH STREET & US 1

KENDALL, FLORIDA

Delray Beach, Florida 33483

Start Date: 02/03/16

COUNTED BY: I. GONZALEZ & D. GONZALEZ

Phone (561) 272-3255

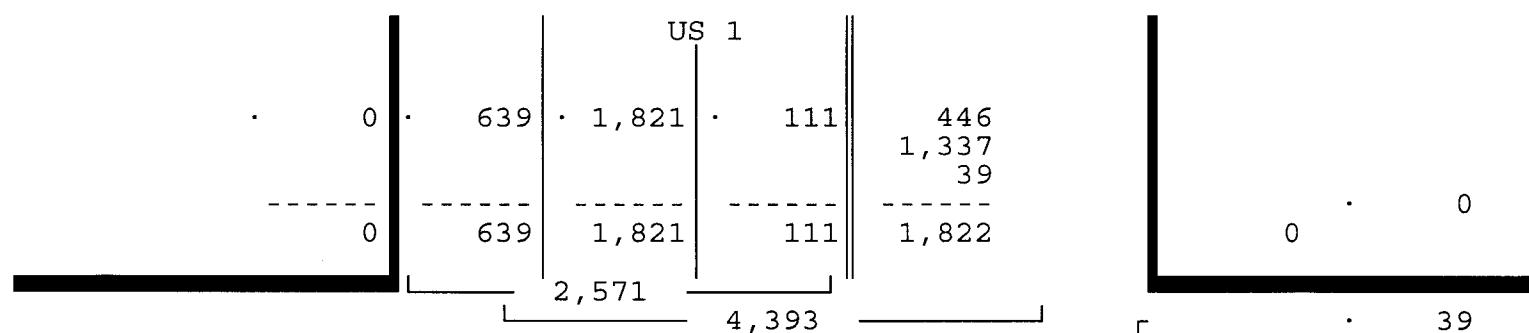
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SIGNALIZED

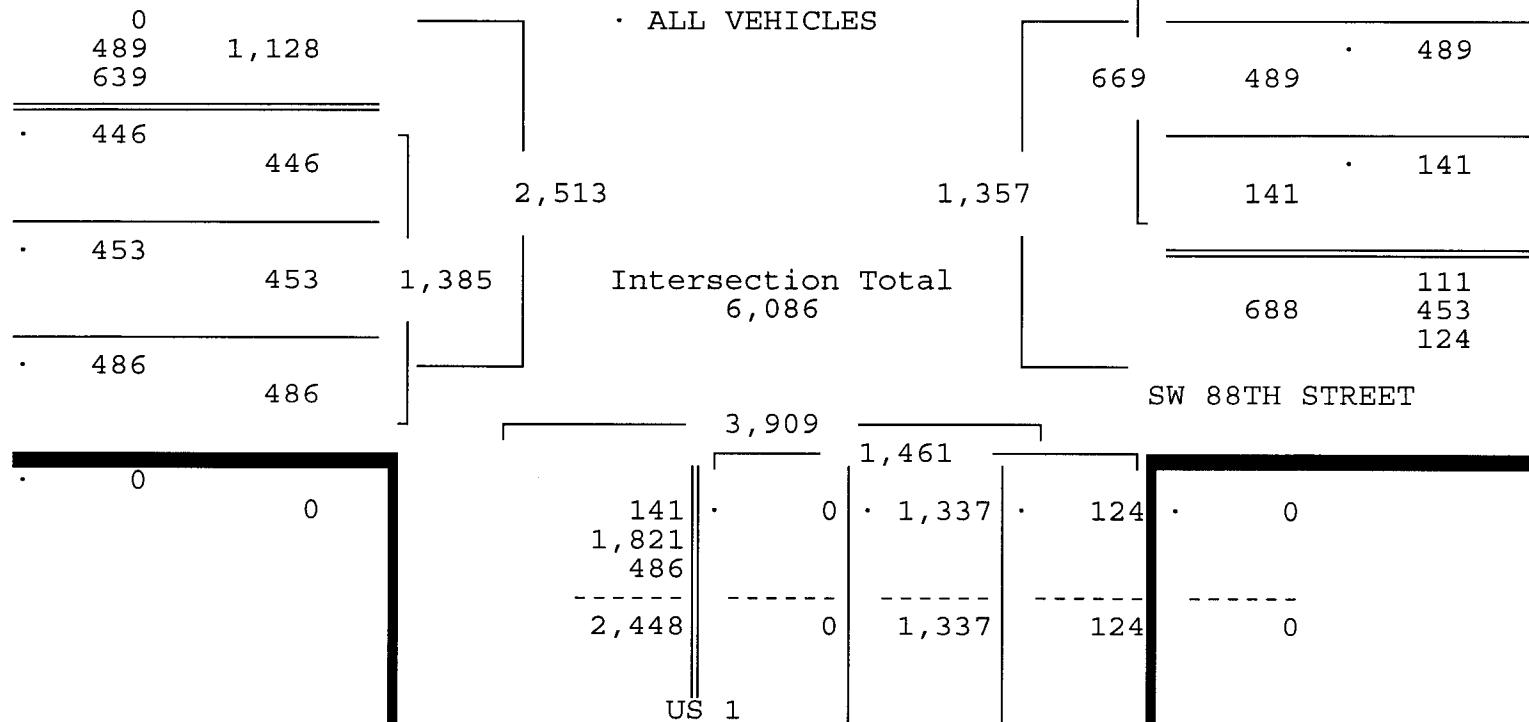
Page : 3

ALL VEHICLES

| US 1 | | | | SW 88TH STREET | | | | US 1 | | | | SW 88TH STREET | | | | |
|--|-------|------|-------|----------------|-------|------|-------|------------|-------|------|-------|----------------|-------|------|-------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 16:00 to 18:00 on 02/03/16 | | | | | | | | | | | | | | | | |
| Peak start 17:00 17:00 17:00 17:00 | | | | | | | | | | | | | | | | |
| Volume | 20 | 91 | 1821 | 639 | 1 | 140 | 489 | 39 | 0 | 0 | 1337 | 124 | 0 | 446 | 453 | 486 |
| Percent | 1% | 4% | 71% | 25% | 0% | 21% | 73% | 6% | 0% | 92% | 8% | 0% | 32% | 33% | 35% | |
| Pk total | 2571 | | | | 669 | | | | 1461 | | | | 1385 | | | |
| Highest | 17:15 | | | | 17:00 | | | | 17:45 | | | | 17:15 | | | |
| Volume | 5 | 25 | 459 | 166 | 0 | 43 | 139 | 9 | 0 | 0 | 380 | 36 | 0 | 125 | 155 | 167 |
| Hi total | 655 | | | | 191 | | | | 416 | | | | 447 | | | |
| PHF | .98 | | | | .88 | | | | .88 | | | | .77 | | | |



SW 88TH STREET



Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

Delray Beach, Florida 33483

Start Date: 02/03/16

Phone (561) 272-3255

File I.D. : 88ST_US1

SW 88TH STREET & US 1

Page : 1

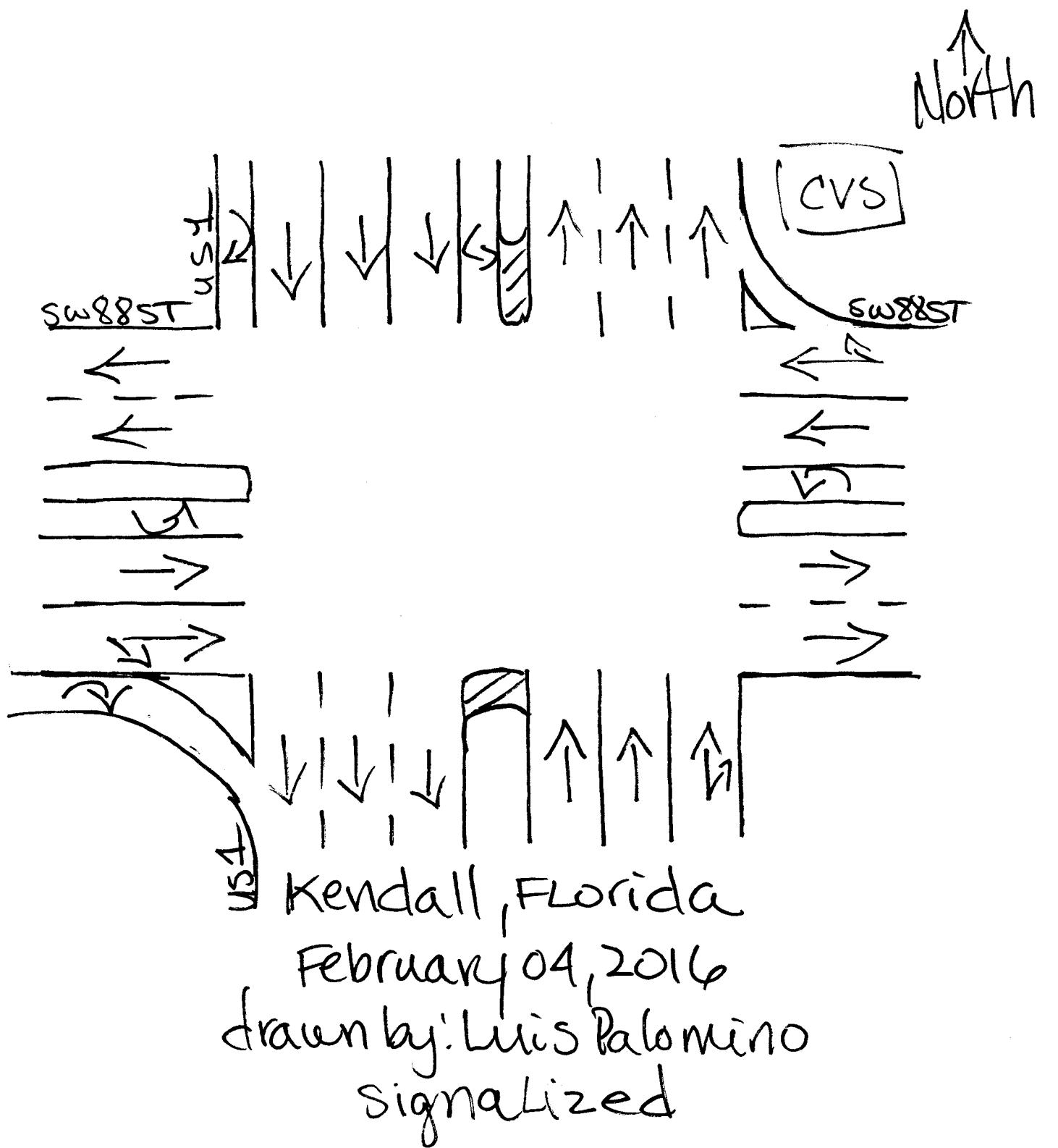
KENDALL, FLORIDA

COUNTED BY: I. GONZALEZ & D. GONZALEZ

SIGNALIZED

PEDESTRIANS & BIKES

| US 1 | | | | SW 88TH STREET | | | | US 1 | | | | SW 88TH STREET | | | | | | | | | |
|----------------------------|------|-------|-------|----------------|--|------|-------|------------|------|--|------|----------------|-------|------|--|------|-------|-------|------|-------|--|
| From North | | | | From East | | | | From South | | | | From West | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | | | | | |
| | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | Total | |
| 07:00 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| 07:15 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| 07:30 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 14 | 15 | |
| 07:45 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Hr Total | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 14 | 15 | |
| 08:00 | 0 | 0 | 0 | 2 | | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 3 | |
| 08:15 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | |
| 08:30 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 0 | 1 | |
| 08:45 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Hr Total | 0 | 0 | 0 | 2 | | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 1 | | 0 | 1 | 0 | 0 | 5 | |
| * BREAK * | | | | | | | | | | | | | | | | | | | | | |
| 16:00 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 1 | 2 | |
| 16:15 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 4 | 0 | 1 | 5 | |
| 16:30 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 2 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 2 | |
| 16:45 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 2 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 2 | |
| Hr Total | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 4 | | 0 | 0 | 0 | 0 | | 0 | 5 | 0 | 2 | 11 | |
| 17:00 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | | 0 | 1 | 0 | 0 | 2 | |
| 17:15 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| 17:30 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 1 | |
| 17:45 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 2 | | 0 | 3 | 0 | 1 | 7 | |
| Hr Total | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 2 | | 0 | 1 | 0 | 2 | | 0 | 4 | 0 | 1 | 10 | |
| *TOTAL* | 0 | 0 | 0 | 2 | | 0 | 0 | 0 | 7 | | 0 | 1 | 0 | 3 | | 0 | 11 | 0 | 17 | 41 | |



Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

SUNSET DRIVE & US 1

Delray Beach, Florida 33483

Start Date: 02/03/16

MIAMI, FLORIDA

Phone (561) 272-3255

File I.D. : SUNS_US1

COUNTED BY: S. SALVO & A. GUTIERREZ

Page : 1

SIGNALIZED

ALL VEHICLES

| US 1 | | | | SUNSET DRIVE | | | | US 1 | | | | SUNSET DRIVE | | | | | | | | | |
|-----------------------|------|------|-------|--------------|------|------|-------|------------|------|------|-------|--------------|------|------|-------|-------|------|------|-------|-------|------|
| From North | | | | From East | | | | From South | | | | From West | | | | | | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total | |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | | | | | |
| 07:00 | 0 | 4 | 333 | 33 | | 0 | 0 | 46 | 1 | | 1 | 18 | 758 | 21 | | 0 | 0 | 161 | 7 | | 1383 |
| 07:15 | 0 | 19 | 415 | 38 | | 0 | 0 | 56 | 0 | | 0 | 11 | 771 | 17 | | 0 | 0 | 142 | 9 | | 1478 |
| 07:30 | 0 | 6 | 512 | 41 | | 0 | 0 | 56 | 1 | | 1 | 15 | 817 | 18 | | 0 | 0 | 123 | 5 | | 1595 |
| 07:45 | 1 | 7 | 467 | 53 | | 0 | 0 | 52 | 2 | | 0 | 20 | 835 | 23 | | 0 | 0 | 161 | 5 | | 1626 |
| Hr Total | 1 | 36 | 1727 | 165 | | 0 | 0 | 210 | 4 | | 2 | 64 | 3181 | 79 | | 0 | 0 | 587 | 26 | | 6082 |
| 08:00 | 0 | 16 | 421 | 51 | | 0 | 0 | 63 | 1 | | 0 | 19 | 785 | 25 | | 0 | 0 | 151 | 3 | | 1535 |
| 08:15 | 0 | 16 | 461 | 44 | | 0 | 0 | 77 | 0 | | 1 | 24 | 866 | 15 | | 0 | 0 | 137 | 10 | | 1651 |
| 08:30 | 0 | 17 | 441 | 62 | | 1 | 0 | 69 | 0 | | 0 | 32 | 914 | 25 | | 0 | 0 | 116 | 6 | | 1683 |
| 08:45 | 1 | 17 | 440 | 51 | | 0 | 1 | 74 | 0 | | 1 | 35 | 729 | 29 | | 0 | 0 | 193 | 8 | | 1579 |
| Hr Total | 1 | 66 | 1763 | 208 | | 1 | 1 | 283 | 1 | | 2 | 110 | 3294 | 94 | | 0 | 0 | 597 | 27 | | 6448 |
| ----- * BREAK * ----- | | | | | | | | | | | | | | | | | | | | | |
| 16:00 | 0 | 11 | 687 | 60 | | 1 | 0 | 101 | 2 | | 1 | 30 | 504 | 21 | | 1 | 2 | 153 | 18 | | 1592 |
| 16:15 | 2 | 15 | 658 | 70 | | 0 | 0 | 109 | 2 | | 1 | 31 | 478 | 24 | | 0 | 0 | 95 | 20 | | 1505 |
| 16:30 | 1 | 13 | 628 | 44 | | 0 | 0 | 106 | 3 | | 0 | 33 | 487 | 23 | | 0 | 0 | 126 | 21 | | 1485 |
| 16:45 | 1 | 6 | 634 | 75 | | 0 | 0 | 146 | 2 | | 2 | 29 | 521 | 20 | | 0 | 0 | 136 | .24 | | 1596 |
| Hr Total | 4 | 45 | 2607 | 249 | | 1 | 0 | 462 | 9 | | 4 | 123 | 1990 | 88 | | 1 | 2 | 510 | 83 | | 6178 |
| 17:00 | 0 | 13 | 645 | 49 | | 0 | 0 | 109 | 5 | | 0 | 31 | 528 | 26 | | 0 | 0 | 94 | 15 | | 1515 |
| 17:15 | 1 | 10 | 571 | 55 | | 0 | 0 | 139 | 0 | | 3 | 31 | 506 | 26 | | 0 | 2 | 147 | 13 | | 1504 |
| 17:30 | 2 | 7 | 538 | 54 | | 0 | 0 | 126 | 3 | | 1 | 26 | 462 | 21 | | 0 | 0 | 142 | 9 | | 1391 |
| 17:45 | 1 | 14 | 619 | 65 | | 0 | 0 | 123 | 6 | | 2 | 27 | 529 | 20 | | 0 | 0 | 145 | 11 | | 1562 |
| Hr Total | 4 | 44 | 2373 | 223 | | 0 | 0 | 497 | 14 | | 6 | 115 | 2025 | 93 | | 0 | 2 | 528 | 48 | | 5972 |

TOTAL 10 191 8470 845 | 2 1 1452 28 | 14 412 10490 354 | 1 4 2222 184 | 24680

Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

SUNSET DRIVE & US 1

MIAMI, FLORIDA

Delray Beach, Florida 33483

Start Date: 02/03/16

COUNTED BY: S. SALVO & A. GUTIERREZ

Phone (561) 272-3255

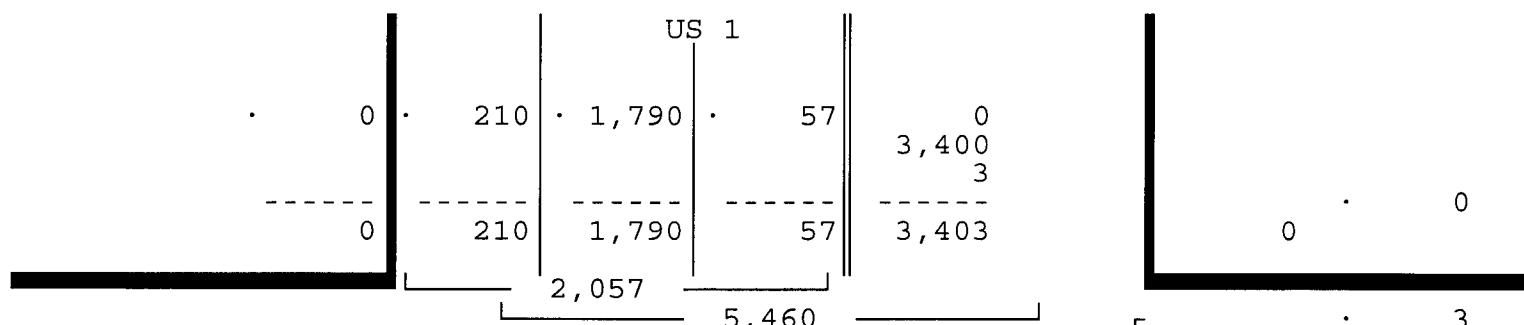
File I.D. : SUNS_US1

SIGNALIZED

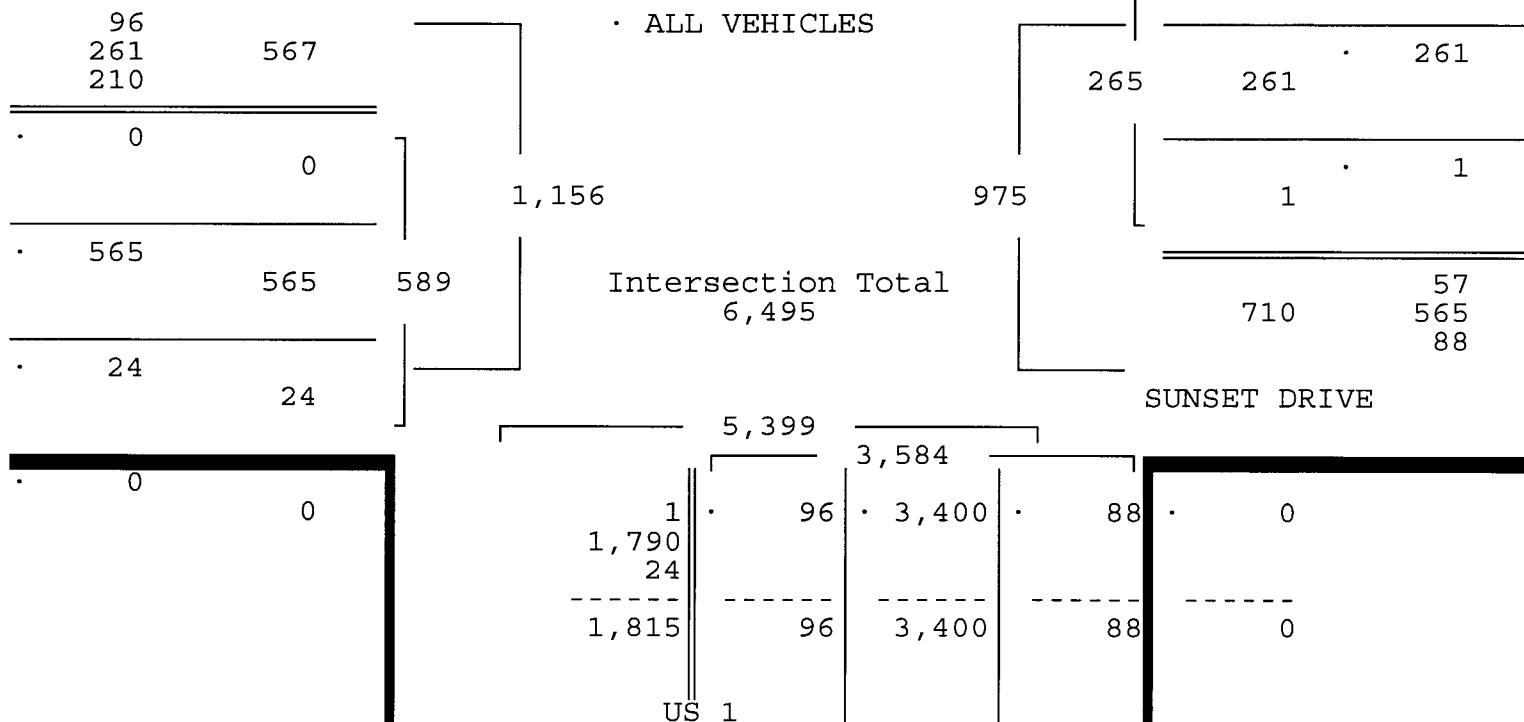
Page : 2

ALL VEHICLES

| US 1 | | | | SUNSET DRIVE | | | | US 1 | | | | SUNSET DRIVE | | | | SUNSET DRIVE | | | | |
|--|-------|------|-------|--------------|-------|------|-------|------------|-------|------|-------|--------------|-------|------|-------|--------------|-------|------|-------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 07:00 to 09:00 on 02/03/16 | | | | | | | | | | | | | | | | | | | | |
| Peak start | 07:45 | | | | 07:45 | | | | 07:45 | | | | 07:45 | | | | 07:45 | | | |
| Volume | 1 | 56 | 1790 | 210 | | 1 | 0 | 261 | 3 | 1 | 95 | 3400 | 88 | | 0 | 0 | 565 | 24 | | |
| Percent | 0% | 3% | 87% | 10% | | 0% | 0% | 98% | 1% | 0% | 3% | 95% | 2% | | 0% | 0% | 96% | 4% | | |
| Pk total | 2057 | | | | 265 | | | | 3584 | | | | 589 | | | | | | | |
| Highest | 07:45 | | | | 08:15 | | | | 08:30 | | | | 07:45 | | | | | | | |
| Volume | 1 | 7 | 467 | 53 | | 0 | 0 | 77 | 0 | 0 | 32 | 914 | 25 | | 0 | 0 | 161 | 5 | | |
| Hi total | 528 | | | | 77 | | | | 971 | | | | 166 | | | | | | | |
| PHF | .97 | | | | .86 | | | | .92 | | | | .89 | | | | | | | |



SUNSET DRIVE



Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

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Site Code : 00160031

Start Date: 02/03/16

File I.D. : SUNS_US1

Page : 3

SUNSET DRIVE & US 1

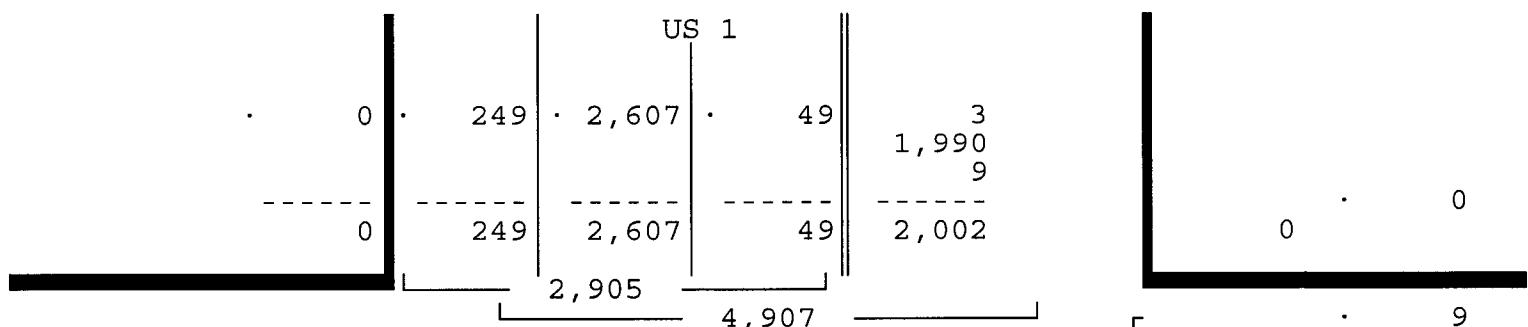
MIAMI, FLORIDA

COUNTED BY: S. SALVO & A. GUTIERREZ

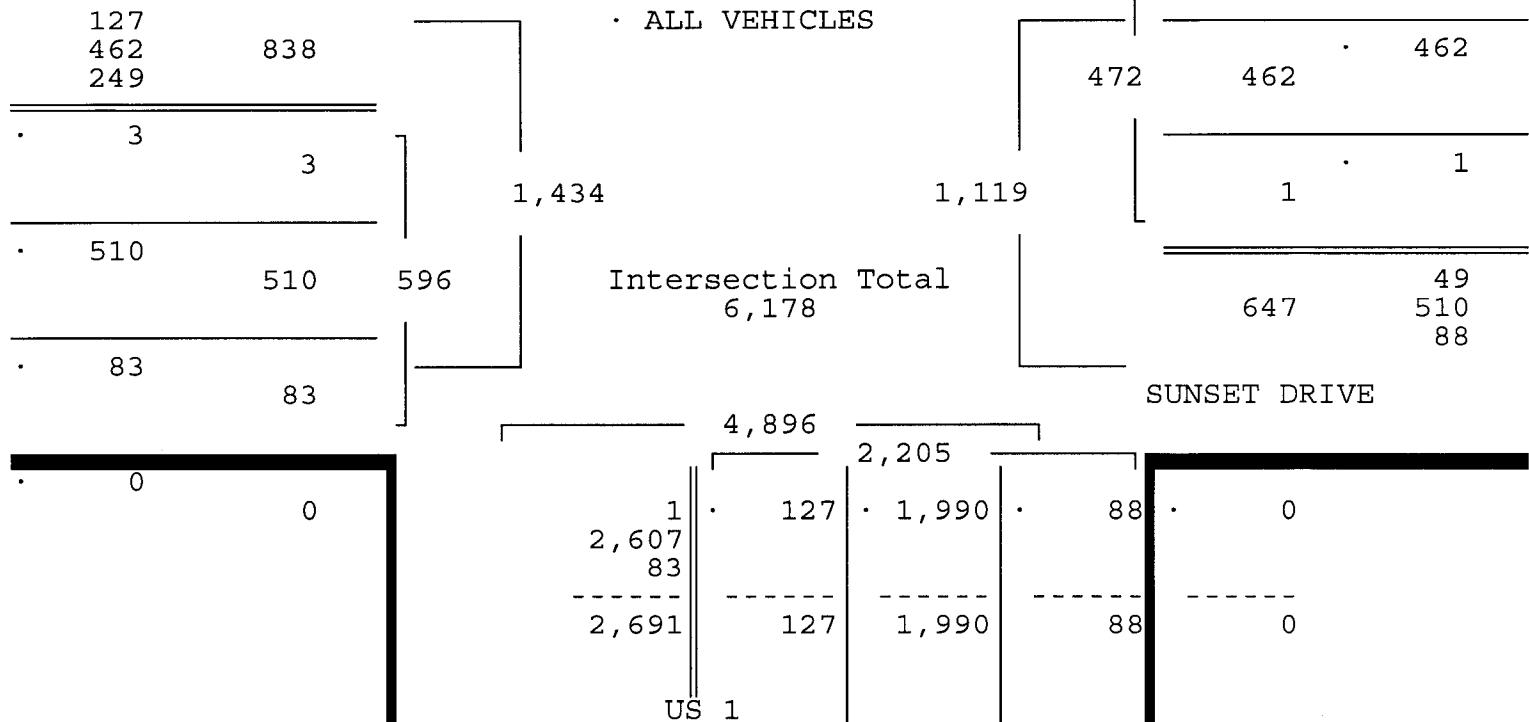
SIGNALIZED

ALL VEHICLES

| US 1 | | | | SUNSET DRIVE | | | | US 1 | | | | SUNSET DRIVE | | | | |
|--|-------|------|-------|--------------|-------|------|-------|------------|-------|------|-------|--------------|-------|------|-------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 16:00 to 18:00 on 02/03/16 | | | | | | | | | | | | | | | | |
| Peak start 16:00 | | | | 16:00 | | | | 16:00 | | | | 16:00 | | | | |
| Volume | 4 | 45 | 2607 | 249 | 1 | 0 | 462 | 9 | 4 | 123 | 1990 | 88 | 1 | 2 | 510 | 83 |
| Percent | 0% | 2% | 90% | 9% | 0% | 0% | 98% | 2% | 0% | 6% | 90% | 4% | 0% | 0% | 86% | 14% |
| PK total | 2905 | | | | 472 | | | | 2205 | | | | 596 | | | |
| Highest | 16:00 | | | | 16:45 | | | | 16:45 | | | | 16:00 | | | |
| Volume | 0 | 11 | 687 | 60 | 0 | 0 | 146 | 2 | 2 | 29 | 521 | 20 | 1 | 2 | 153 | 18 |
| Hi total | 758 | | | | 148 | | | | 572 | | | | 174 | | | |
| PHF | .96 | | | | .80 | | | | .96 | | | | .86 | | | |



SUNSET DRIVE



Traffic Survey Specialists, Inc.

SUNSET DRIVE & US 1

MIAMI, FLORIDA

COUNTED BY: S. SALVO & A. GUTIERREZ

SIGNALIZED

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Phone (561) 272-3255

Site Code : 00160031

Start Date: 02/03/16

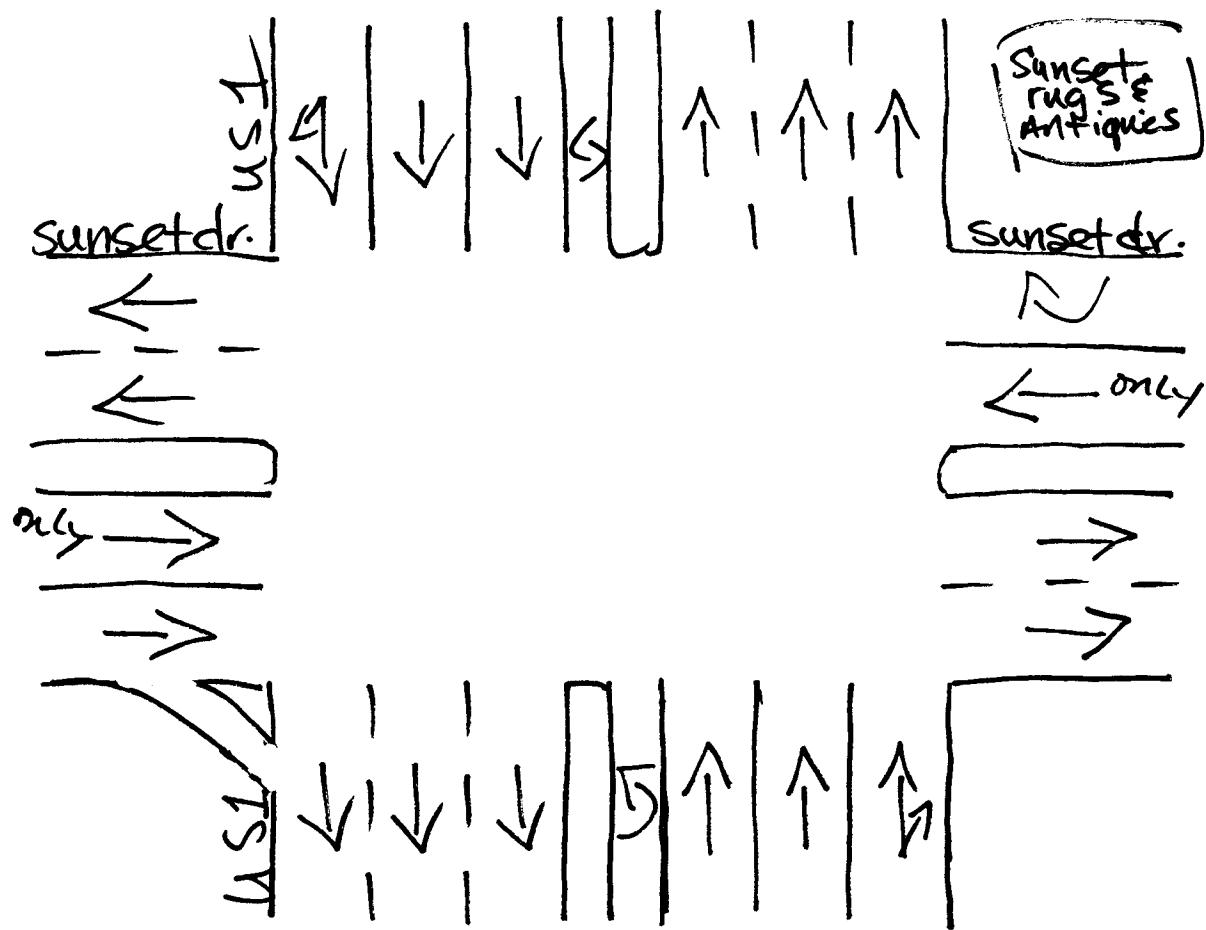
File I.D. : SUNS_US1

Page : 1

PEDESTRIANS & BIKES

| US 1 | | | | SUNSET DRIVE | | | | US 1 | | | | SUNSET DRIVE | | | | | | | | |
|----------------------------|------|-------|-------|--------------|--|------|-------|------------|------|--|------|--------------|-------|------|--|------|-------|-------|------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | | | | | |
| | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | | | | |
| 07:00 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 8 | | 0 | 2 | 0 | 2 | | 0 | 0 | 0 | 9 | 21 |
| 07:15 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 16 | | 0 | 0 | 0 | 0 | | 0 | 2 | 0 | 1 | 19 |
| 07:30 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 20 | | 0 | 0 | 0 | 0 | | 0 | 2 | 0 | 0 | 22 |
| 07:45 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 18 | | 0 | 0 | 0 | 4 | | 0 | 1 | 0 | 10 | 33 |
| Hr Total | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 62 | | 0 | 2 | 0 | 6 | | 0 | 5 | 0 | 20 | 95 |
| 08:00 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 8 | | 0 | 0 | 0 | 2 | | 0 | 0 | 0 | 2 | 12 |
| 08:15 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 20 | | 0 | 1 | 0 | 0 | | 0 | 0 | 0 | 5 | 26 |
| 08:30 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 8 | | 0 | 0 | 0 | 1 | | 0 | 3 | 0 | 2 | 14 |
| 08:45 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 6 | | 0 | 3 | 0 | 4 | | 0 | 1 | 0 | 1 | 15 |
| Hr Total | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 42 | | 0 | 4 | 0 | 7 | | 0 | 4 | 0 | 10 | 67 |
| * BREAK * | | | | | | | | | | | | | | | | | | | | |
| 16:00 | 0 | 0 | 0 | 9 | | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 2 | | 0 | 0 | 0 | 1 | 13 |
| 16:15 | 0 | 0 | 0 | 15 | | 0 | 0 | 0 | 5 | | 0 | 1 | 0 | 0 | | 0 | 1 | 0 | 0 | 22 |
| 16:30 | 0 | 0 | 0 | 12 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 4 | | 0 | 3 | 0 | 3 | 23 |
| 16:45 | 0 | 0 | 0 | 19 | | 0 | 0 | 0 | 1 | | 0 | 1 | 0 | 4 | | 0 | 1 | 0 | 1 | 27 |
| Hr Total | 0 | 0 | 0 | 55 | | 0 | 0 | 0 | 7 | | 0 | 3 | 0 | 10 | | 0 | 5 | 0 | 5 | 85 |
| 17:00 | 0 | 0 | 0 | 28 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 1 | | 0 | 1 | 0 | 1 | 32 |
| 17:15 | 0 | 0 | 0 | 35 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 2 | | 0 | 4 | 0 | 4 | 45 |
| 17:30 | 0 | 0 | 0 | 19 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 2 | | 0 | 3 | 0 | 6 | 30 |
| 17:45 | 0 | 0 | 0 | 20 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 1 | | 0 | 4 | 0 | 1 | 26 |
| Hr Total | 0 | 0 | 0 | 102 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 6 | | 0 | 12 | 0 | 12 | 133 |
| *TOTAL* | 0 | 0 | 0 | 157 | | 0 | 0 | 0 | 111 | | 0 | 10 | 0 | 29 | | 0 | 26 | 0 | 47 | 380 |

↑ North



Miami, Florida

February 04, 2016

drawn by: Lelis Palomino
signalized

Traffic Survey Specialists, Inc.

SW 40TH STREET & US 1

MIAMI, FLORIDA

COUNTED BY: A. PALOMINO & R. MARTINEZ

SIGNALIZED

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Phone (561) 272-3255

Site Code : 00160031

Start Date: 02/03/16

File I.D. : 40STRUS1

Page : 1

ALL VEHICLES

| US 1 | | | | SW 40TH STREET | | | | US 1 | | | | SW 40TH STREET | | | | | | | | |
|-----------------------|------|------|-------|----------------|------|------|-------|------------|------|------|-------|----------------|------|------|-------|-------|-----|----|--|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total | | | | |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | | | | |
| 07:00 | 0 | 0 | 522 | 120 | | 0 | 47 | 63 | 0 | 0 | 0 | 754 | 29 | | 0 | 100 | 38 | 0 | | 1673 |
| 07:15 | 0 | 0 | 559 | 133 | | 0 | 51 | 69 | 0 | 0 | 0 | 724 | 42 | | 0 | 135 | 57 | 1 | | 1771 |
| 07:30 | 0 | 9 | 470 | 110 | | 0 | 59 | 73 | 0 | 0 | 0 | 618 | 35 | | 0 | 135 | 50 | 3 | | 1562 |
| 07:45 | 0 | 0 | 594 | 121 | | 0 | 56 | 62 | 0 | 0 | 0 | 610 | 33 | | 0 | 104 | 46 | 0 | | 1626 |
| Hr Total | 0 | 9 | 2145 | 484 | | 0 | 213 | 267 | 0 | 0 | 0 | 2706 | 139 | | 0 | 474 | 191 | 4 | | 6632 |
| 08:00 | 0 | 0 | 561 | 147 | | 0 | 63 | 82 | 0 | 0 | 0 | 551 | 48 | | 0 | 108 | 57 | 2 | | 1619 |
| 08:15 | 0 | 0 | 490 | 151 | | 0 | 71 | 87 | 0 | 0 | 0 | 565 | 41 | | 0 | 121 | 49 | 3 | | 1578 |
| 08:30 | 0 | 0 | 454 | 114 | | 0 | 55 | 67 | 0 | 1 | 0 | 524 | 64 | | 0 | 112 | 70 | 2 | | 1463 |
| 08:45 | 0 | 0 | 597 | 192 | | 0 | 64 | 77 | 0 | 0 | 0 | 580 | 59 | | 0 | 93 | 51 | 4 | | 1717 |
| Hr Total | 0 | 0 | 2102 | 604 | | 0 | 253 | 313 | 0 | 1 | 0 | 2220 | 212 | | 0 | 434 | 227 | 11 | | 6377 |
| ----- * BREAK * ----- | | | | | | | | | | | | | | | | | | | | |
| 16:00 | 0 | 0 | 557 | 160 | | 0 | 42 | 69 | 1 | 1 | 0 | 609 | 60 | | 0 | 97 | 31 | 4 | | 1631 |
| 16:15 | 0 | 0 | 511 | 173 | | 0 | 45 | 90 | 1 | 0 | 0 | 635 | 44 | | 0 | 74 | 29 | 2 | | 1604 |
| 16:30 | 0 | 0 | 543 | 149 | | 0 | 46 | 78 | 1 | 0 | 0 | 523 | 42 | | 0 | 90 | 38 | 5 | | 1515 |
| 16:45 | 0 | 0 | 463 | 133 | | 0 | 37 | 74 | 0 | 0 | 0 | 519 | 52 | | 0 | 102 | 37 | 9 | | 1426 |
| Hr Total | 0 | 0 | 2074 | 615 | | 0 | 170 | 311 | 3 | 1 | 0 | 2286 | 198 | | 0 | 363 | 135 | 20 | | 6176 |
| 17:00 | 0 | 0 | 582 | 157 | | 0 | 31 | 69 | 0 | 0 | 0 | 589 | 55 | | 0 | 83 | 42 | 2 | | 1610 |
| 17:15 | 0 | 0 | 484 | 165 | | 0 | 45 | 90 | 0 | 1 | 0 | 599 | 59 | | 0 | 88 | 34 | 6 | | 1571 |
| 17:30 | 0 | 0 | 463 | 167 | | 0 | 38 | 84 | 0 | 0 | 0 | 538 | 54 | | 0 | 104 | 40 | 6 | | 1494 |
| 17:45 | 0 | 0 | 439 | 176 | | 0 | 46 | 77 | 0 | 0 | 0 | 506 | 59 | | 0 | 92 | 48 | 7 | | 1450 |
| Hr Total | 0 | 0 | 1968 | 665 | | 0 | 160 | 320 | 0 | 1 | 0 | 2232 | 227 | | 0 | 367 | 164 | 21 | | 6125 |
| *TOTAL* | 0 | 9 | 8289 | 2368 | | 0 | 796 | 1211 | 3 | 3 | 0 | 9444 | 776 | | 0 | 1638 | 717 | 56 | | 25310 |

Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Site Code : 00160031

SW 40TH STREET & US 1

MIAMI, FLORIDA

COUNTED BY: A. PALOMINO & R. MARTINEZ

SIGNALIZED

Phone (561) 272-3255

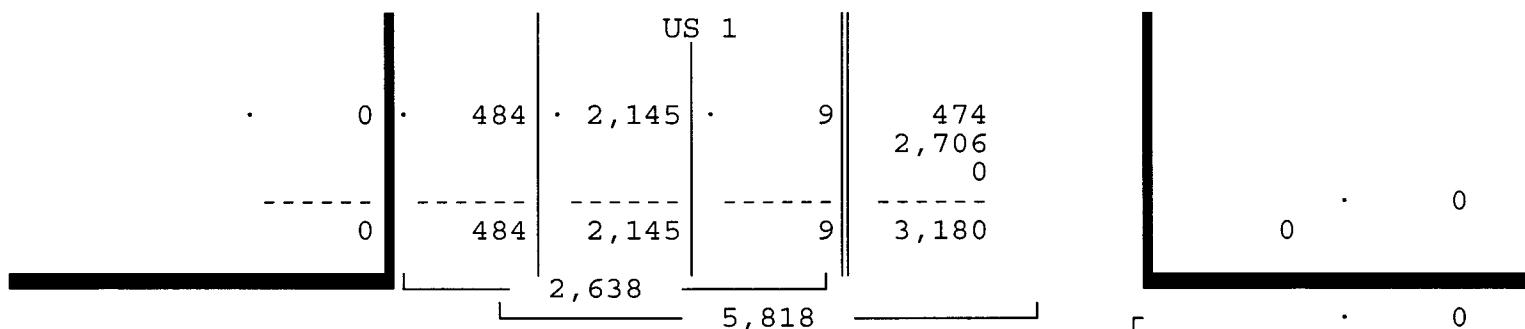
Start Date: 02/03/16

File I.D. : 40STRUS1

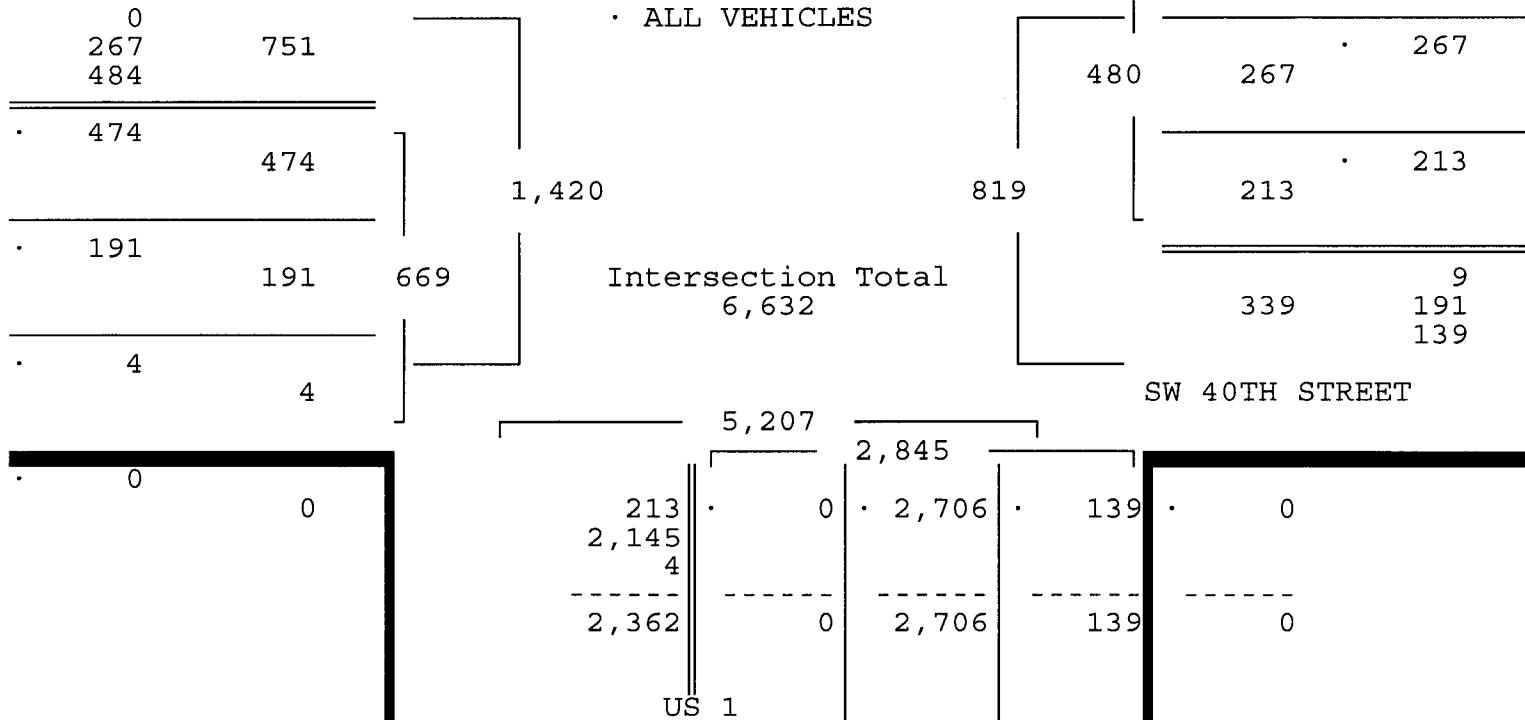
Page : 2

ALL VEHICLES

| US 1 | | SW 40TH STREET | | | | US 1 | | SW 40TH STREET | | | | SW 40TH STREET | | SW 40TH STREET | | | |
|---|-------|----------------|-------|-------|-------|------------|-------|----------------|-------|-----------|-------|----------------|------|----------------|-------|-------|----|
| From North | | From East | | | | From South | | | | From West | | | | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total | |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 07:00 to 09:00 on 02/03/16 | | | | | | | | | | | | | | | | | |
| Peak start 07:00 | | | | | | | | | | | | | | | | | |
| Volume | 0 | 9 | 2145 | 484 | 0 | 213 | 267 | 0 | 0 | 0 | 0 | 2706 | 139 | 0 | 474 | 191 | 4 |
| Percent | 0% | 0% | 81% | 18% | 0% | 44% | 56% | 0% | 0% | 0% | 0% | 95% | 5% | 0% | 71% | 29% | 1% |
| Pk total | 2638 | | | | 480 | | | | 2845 | | | | | 669 | | | |
| Highest | 07:45 | | | | 07:30 | | | | 07:00 | | | | | 07:15 | | | |
| Volume | 0 | 0 | 594 | 121 | 0 | 59 | 73 | 0 | 0 | 0 | 0 | 754 | 29 | 0 | 135 | 57 | 1 |
| Hi total | 715 | | | | 132 | | | | 783 | | | | | 193 | | | |
| PHF | .92 | | | | .91 | | | | .91 | | | | | .87 | | | |



SW 40TH STREET



Traffic Survey Specialists, Inc.

SW 40TH STREET & US 1

MIAMI, FLORIDA

COUNTED BY: A. PALOMINO & R. MARTINEZ

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Phone (561) 272-3255

Site Code : 00160031

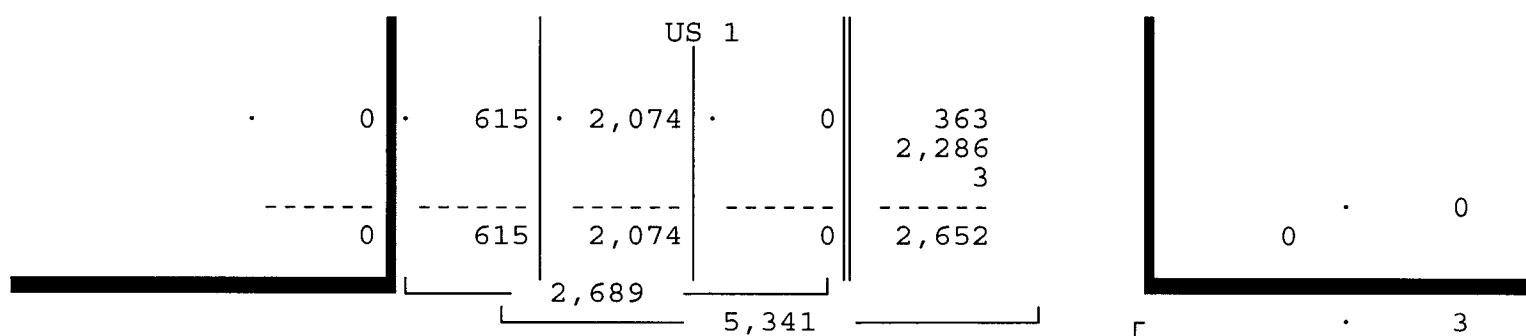
Start Date: 02/03/16

File I.D. : 40STRUS1

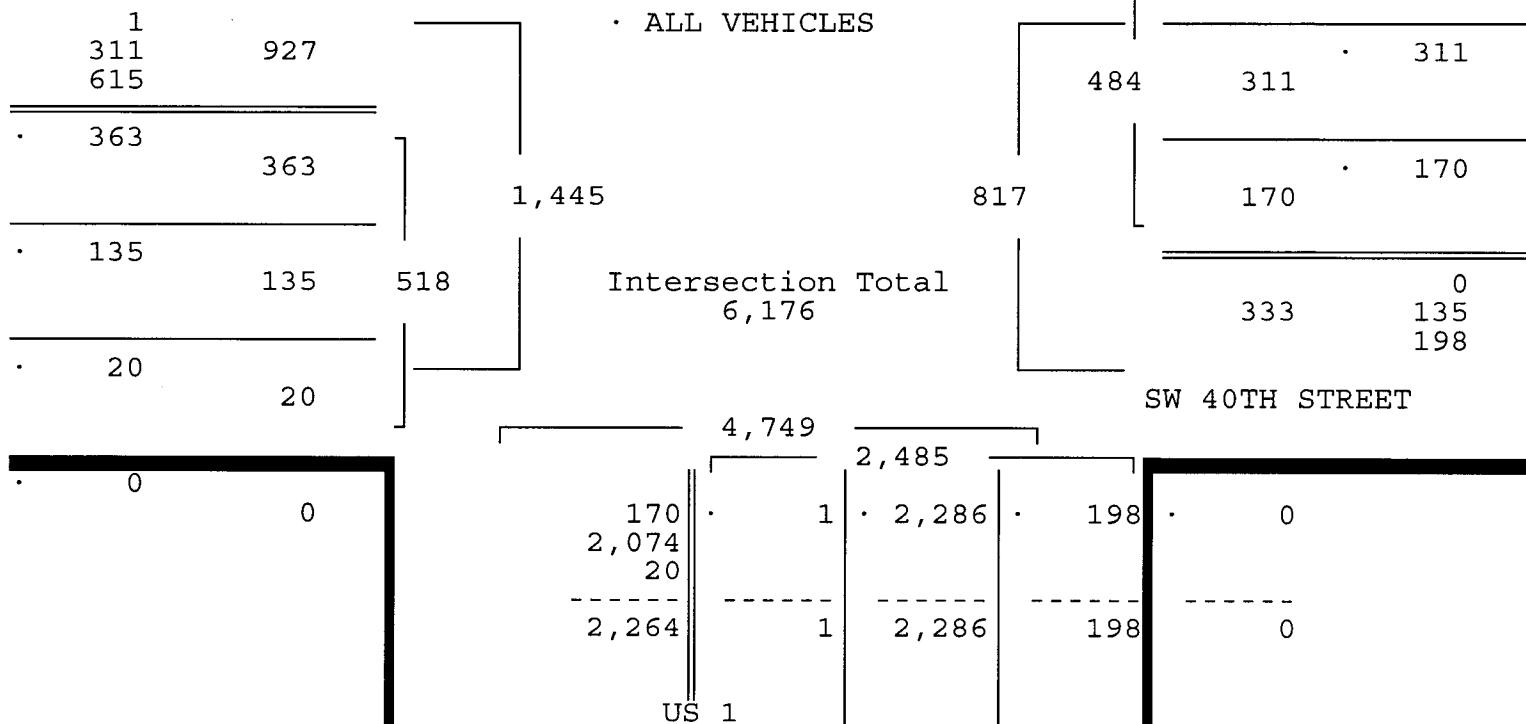
Page : 3

ALL VEHICLES

| US 1 | | | | SW 40TH STREET | | | | US 1 | | | | SW 40TH STREET | | | | |
|--|-------|------|-------|----------------|-------|------|-------|------------|-------|------|-------|----------------|-------|------|-------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 16:00 to 18:00 on 02/03/16 | | | | | | | | | | | | | | | | |
| Peak start 16:00 | | | | 16:00 | | | | 16:00 | | | | 16:00 | | | | |
| Volume | 0 | 0 | 2074 | 615 | 0 | 170 | 311 | 3 | 1 | 0 | 2286 | 198 | 0 | 363 | 135 | 20 |
| Percent | 0% | 0% | 77% | 23% | 0% | 35% | 64% | 1% | 0% | 0% | 92% | 8% | 0% | 70% | 26% | 4% |
| Pk total | 2689 | | | | 484 | | | | 2485 | | | | 518 | | | |
| Highest | 16:00 | | | | 16:15 | | | | 16:15 | | | | 16:45 | | | |
| Volume | 0 | 0 | 557 | 160 | 0 | 45 | 90 | 1 | 0 | 0 | 635 | 44 | 0 | 102 | 37 | 9 |
| Hi total | 717 | | | | 136 | | | | 679 | | | | 148 | | | |
| PHF | .94 | | | | .89 | | | | .91 | | | | .88 | | | |



SW 40TH STREET



Intersection Total

6,176

Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

Delray Beach, Florida 33483

Start Date: 02/03/16

Phone (561) 272-3255

File I.D. : 40STRUS1

SW 40TH STREET & US 1

Page : 1

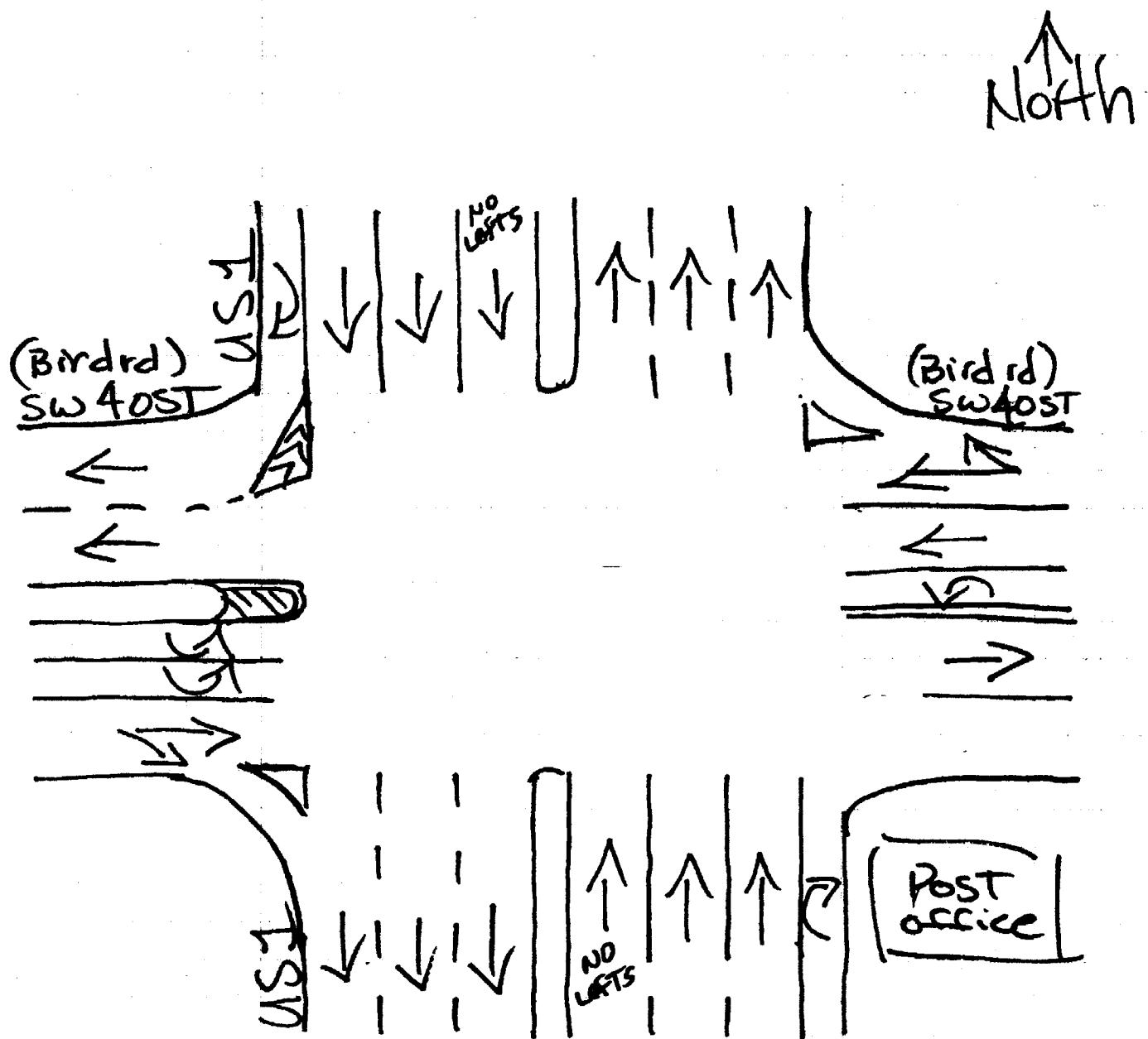
MIAMI, FLORIDA

COUNTED BY: A. PALOMINO & R. MARTINEZ

SIGNALIZED

PEDESTRIANS & BIKES

| US 1 | SW 40TH STREET | | | | US 1 | | | | SW 40TH STREET | | | | | | | | |
|----------------------------|----------------|-------|-----------|------|------------|-------|-----------|------|----------------|-------|-------|------|------|-------|-------|------|-------|
| | From North | | From East | | From South | | From West | | | | | | | | | | |
| | Left | BIKES | Right | Peds | Left | BIKES | Right | Peds | Left | BIKES | Right | Peds | Left | BIKES | Right | Peds | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | |
| 07:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 6 |
| 07:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Hr Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 3 | 0 | 0 | 0 | 0 | 7 |
| 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 0 | 0 | 0 | 5 |
| 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| 08:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 08:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| Hr Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 9 | 0 | 0 | 0 | 0 | 11 |
| * BREAK * | | | | | | | | | | | | | | | | | |
| 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 16:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 4 | 10 |
| 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 3 | 0 | 3 | 9 |
| Hr Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 5 | 0 | 6 | 0 | 7 | 20 |
| 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 1 | 0 | 6 | 10 |
| 17:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 3 |
| 17:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 17:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 4 |
| Hr Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 5 | 0 | 2 | 0 | 7 | 18 |
| *TOTAL* | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 22 | 0 | 8 | 0 | 14 | 56 |



Miami, Florida

December 03, 2014

drawn by: Luis Palomino
signalized ✓

Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

US 1 & SW 27TH AVENUE

Delray Beach, Florida 33483

Start Date: 02/03/16

MIAMI, FLORIDA

Phone (561) 272-3255

File I.D. : US1_27AV

COUNTED BY: L. PALOMINO & M. CRUZ

Page : 1

SIGNALIZED

ALL VEHICLES

| SW 27TH AVENUE | | | | US 1 | | | | SW 27TH AVENUE | | | | US 1 | | | | |
|-----------------------|------|------|-------|-----------|------|------|-------|----------------|------|------|-------|-----------|------|------|-------|-------------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | |
| 07:00 | 0 | 22 | 93 | 91 | 0 | 13 | 564 | 12 | 0 | 3 | 74 | 47 | 0 | 53 | 797 | 3 1772 |
| 07:15 | 0 | 22 | 124 | 98 | 0 | 16 | 682 | 17 | 0 | 11 | 74 | 39 | 0 | 35 | 739 | 7 1864 |
| 07:30 | 0 | 18 | 125 | 76 | 0 | 9 | 716 | 18 | 0 | 9 | 85 | 61 | 0 | 43 | 693 | 4 1857 |
| 07:45 | 0 | 16 | 132 | 89 | 0 | 5 | 681 | 12 | 0 | 8 | 94 | 58 | 0 | 35 | 630 | 4 1764 |
| Hr Total | 0 | 78 | 474 | 354 | 0 | 43 | 2643 | 59 | 0 | 31 | 327 | 205 | 0 | 166 | 2859 | 18 7257 |
| 08:00 | 0 | 13 | 131 | 60 | 0 | 14 | 681 | 14 | 0 | 2 | 78 | 55 | 0 | 26 | 691 | 1 1766 |
| 08:15 | 0 | 11 | 128 | 78 | 0 | 16 | 681 | 10 | 0 | 10 | 111 | 66 | 0 | 38 | 687 | 6 1842 |
| 08:30 | 0 | 8 | 109 | 72 | 0 | 5 | 642 | 12 | 0 | 8 | 96 | 68 | 0 | 36 | 654 | 5 1715 |
| 08:45 | 0 | 13 | 93 | 42 | 0 | 20 | 706 | 12 | 0 | 8 | 111 | 73 | 0 | 41 | 601 | 2 1722 |
| Hr Total | 0 | 45 | 461 | 252 | 0 | 55 | 2710 | 48 | 0 | 28 | 396 | 262 | 0 | 141 | 2633 | 14 7045 |
| ----- * BREAK * ----- | | | | | | | | | | | | | | | | |
| 16:00 | 0 | 15 | 105 | 70 | 0 | 20 | 713 | 25 | 0 | 13 | 112 | 35 | 0 | 30 | 569 | 3 1710 |
| 16:15 | 0 | 20 | 106 | 72 | 0 | 32 | 615 | 18 | 0 | 7 | 123 | 25 | 0 | 47 | 614 | 13 1692 |
| 16:30 | 0 | 10 | 96 | 54 | 0 | 31 | 687 | 21 | 0 | 4 | 132 | 27 | 0 | 30 | 611 | 10 1713 |
| 16:45 | 0 | 13 | 112 | 61 | 1 | 32 | 690 | 14 | 0 | 9 | 111 | 24 | 0 | 42 | 628 | 13 1750 |
| Hr Total | 0 | 58 | 419 | 257 | 1 | 115 | 2705 | 78 | 0 | 33 | 478 | 111 | 0 | 149 | 2422 | 39 6865 |
| 17:00 | 0 | 12 | 124 | 67 | 0 | 30 | 712 | 17 | 0 | 4 | 136 | 30 | 0 | 38 | 591 | 8 1769 |
| 17:15 | 0 | 9 | 128 | 59 | 0 | 25 | 681 | 24 | 0 | 6 | 133 | 34 | 0 | 51 | 628 | 8 1786 |
| 17:30 | 0 | 7 | 118 | 55 | 0 | 29 | 741 | 32 | 0 | 7 | 112 | 24 | 1 | 30 | 621 | 6 1783 |
| 17:45 | 0 | 11 | 126 | 43 | 0 | 42 | 715 | 23 | 0 | 9 | 123 | 40 | 0 | 34 | 610 | 11 1787 |
| Hr Total | 0 | 39 | 496 | 224 | 0 | 126 | 2849 | 96 | 0 | 26 | 504 | 128 | 1 | 153 | 2450 | 33 7125 |
| *TOTAL* | 0 | 220 | 1850 | 1087 | 1 | 339 | 10907 | 281 | 0 | 118 | 1705 | 706 | 1 | 609 | 10364 | 104 28292 |

Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

Delray Beach, Florida 33483

Start Date: 02/03/16

Phone (561) 272-3255

File I.D. : US1_27AV

US 1 & SW 27TH AVENUE

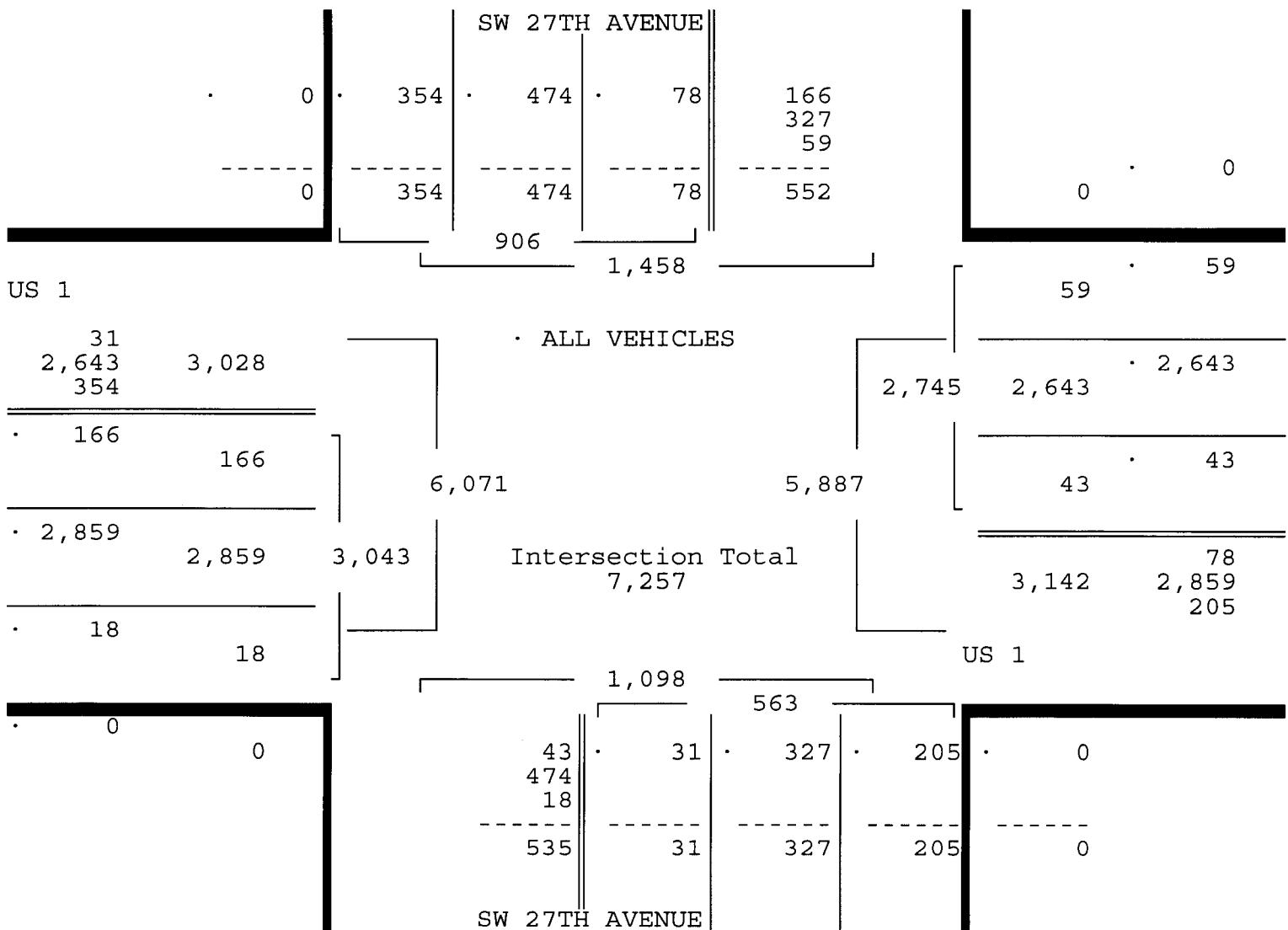
MIAMI, FLORIDA

COUNTED BY: L. PALOMINO & M. CRUZ

SIGNALIZED

ALL VEHICLES

| SW 27TH AVENUE | | | | US 1 | | | | SW 27TH AVENUE | | | | US 1 | | | | |
|--|-------|------|-------|-----------|-------|------|-------|----------------|-------|------|-------|-----------|-------|------|-------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 07:00 to 09:00 on 02/03/16 | | | | | | | | | | | | | | | | |
| Peak start 07:00 | | | | 07:00 | | | | 07:00 | | | | 07:00 | | | | |
| Volume | 0 | 78 | 474 | 354 | 0 | 43 | 2643 | 59 | 0 | 31 | 327 | 205 | 0 | 166 | 2859 | 18 |
| Percent | 0% | 9% | 52% | 39% | 0% | 2% | 96% | 2% | 0% | 6% | 58% | 36% | 0% | 5% | 94% | 1% |
| Pk total | 906 | | | | 2745 | | | | 563 | | | | 3043 | | | |
| Highest | 07:15 | | | | 07:30 | | | | 07:45 | | | | 07:00 | | | |
| Volume | 0 | 22 | 124 | 98 | 0 | 9 | 716 | 18 | 0 | 8 | 94 | 58 | 0 | 53 | 797 | 3 |
| Hi total | 244 | | | | 743 | | | | 160 | | | | 853 | | | |
| PHF | .93 | | | | .92 | | | | .88 | | | | .89 | | | |



Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Site Code : 00160031

US 1 & SW 27TH AVENUE

MIAMI, FLORIDA

COUNTED BY: L. PALOMINO & M. CRUZ

SIGNALIZED

Phone (561) 272-3255

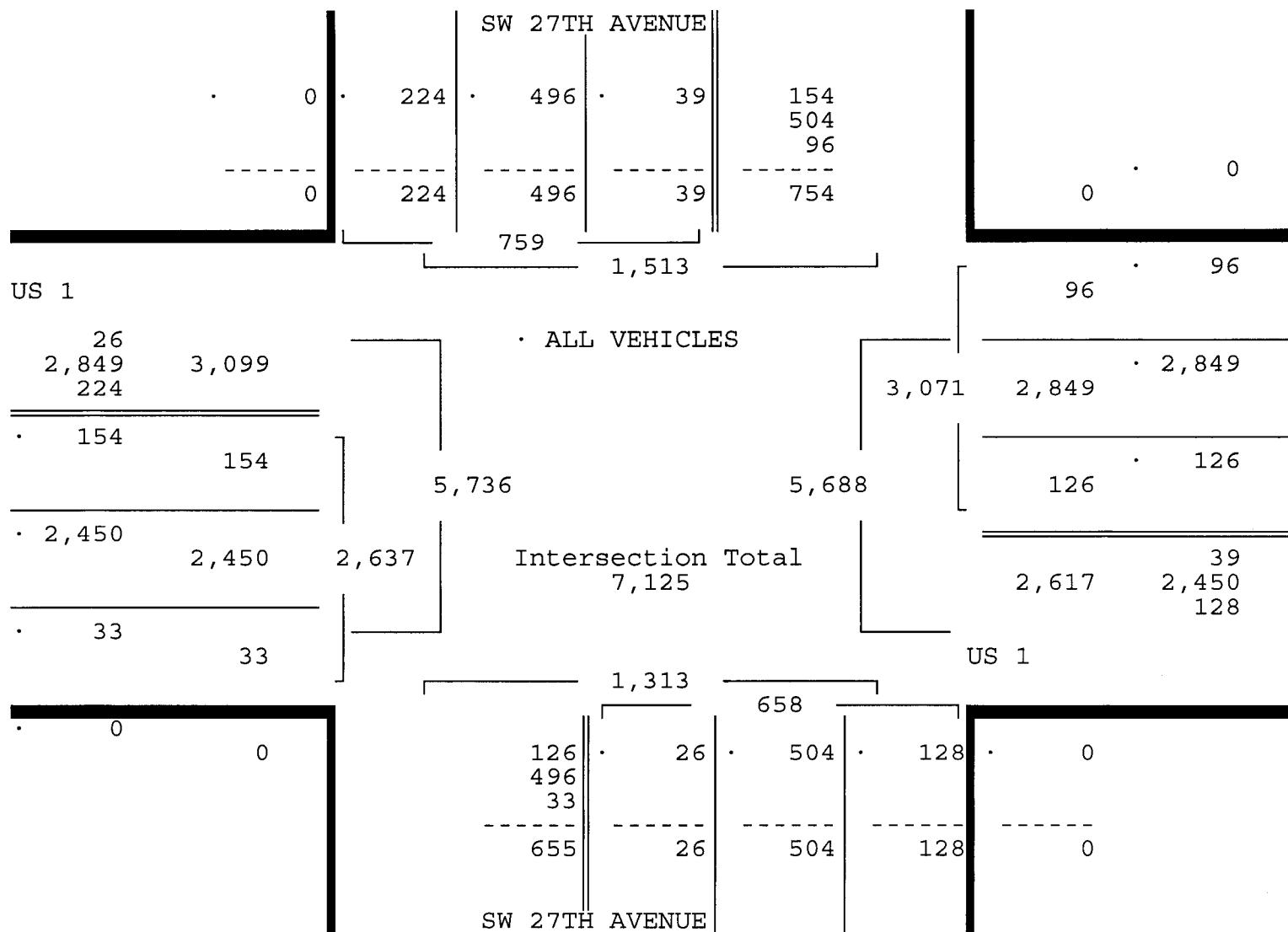
Start Date: 02/03/16

File I.D. : US1_27AV

Page : 3

ALL VEHICLES

| SW 27TH AVENUE | | | | US 1 | | | | SW 27TH AVENUE | | | | US 1 | | | | |
|---|-------|------|-------|-----------|------|-------|-------|----------------|------|------|-------|-----------|------|------|-------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 16:00 to 18:00 on 02/03/16 | | | | | | | | | | | | | | | | |
| Peak start 17:00 | | | | | | | | | | | | | | | | |
| Volume | 0 | 39 | 496 | 224 | | 0 | 126 | 2849 | 96 | | 0 | 26 | 504 | 128 | | |
| Percent | 0% | 5% | 65% | 30% | | 0% | 4% | 93% | 3% | | 0% | 4% | 77% | 19% | | |
| Pk total | 759 | | | | | 3071 | | | | | 658 | | | | | |
| Highest | 17:00 | | | | | 17:30 | | | | | 17:15 | | | | | |
| Volume | 0 | 12 | 124 | 67 | | 0 | 29 | 741 | 32 | | 0 | 6 | 133 | 34 | | |
| Hi total | 203 | | | | | 802 | | | | | 173 | | | | | |
| PHF | .93 | | | | | .96 | | | | | .95 | | | | | |



Traffic Survey Specialists, Inc.

85 SE 4th Avenue, Unit 109

Site Code : 00160031

Delray Beach, Florida 33483

Start Date: 02/03/16

Phone (561) 272-3255

File I.D. : US1_27AV

US 1 & SW 27TH AVENUE

MIAMI, FLORIDA

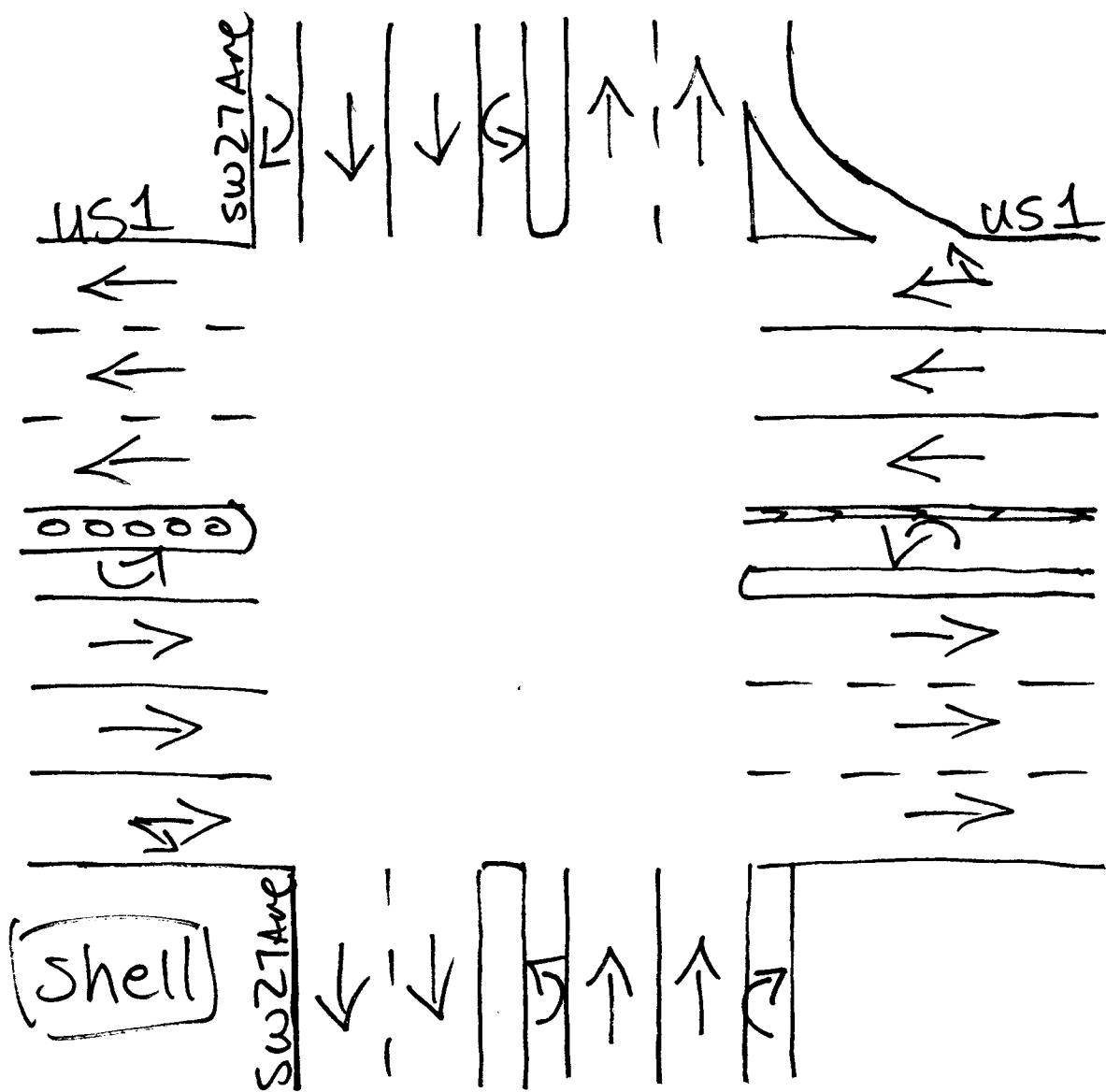
COUNTED BY: L. PALOMINO & M. CRUZ

SIGNALIZED

PEDESTRIANS & BIKES

| SW 27TH AVENUE | | | | US 1 | | | | SW 27TH AVENUE | | | | US 1 | | | | | | | | |
|-----------------------|------|-------|-------|-----------|--|------|-------|----------------|------|--|------|-----------|-------|------|--|------|-------|-------|------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | | | | | |
| | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | | Left | BIKES | Right | Peds | Total |
| Date 02/03/16 ----- | | | | | | | | | | | | | | | | | | | | |
| 07:00 | 0 | 1 | 0 | 2 | | 0 | 3 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 12 | 18 |
| 07:15 | 0 | 2 | 0 | 2 | | 0 | 1 | 0 | 4 | | 0 | 0 | 0 | 3 | | 0 | 4 | 0 | 19 | 35 |
| 07:30 | 0 | 6 | 0 | 6 | | 0 | 3 | 0 | 1 | | 0 | 0 | 0 | 2 | | 0 | 3 | 0 | 25 | 46 |
| 07:45 | 0 | 3 | 0 | 0 | | 0 | 1 | 0 | 0 | | 0 | 0 | 0 | 1 | | 0 | 2 | 0 | 3 | 10 |
| Hr Total | 0 | 12 | 0 | 10 | | 0 | 8 | 0 | 5 | | 0 | 0 | 0 | 6 | | 0 | 9 | 0 | 59 | 109 |
| 08:00 | 0 | 3 | 0 | 1 | | 0 | 0 | 0 | 3 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 18 | 25 |
| 08:15 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 2 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | 15 | 18 |
| 08:30 | 0 | 4 | 0 | 2 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 3 | | 0 | 5 | 0 | 29 | 43 |
| 08:45 | 0 | 3 | 0 | 5 | | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 2 | | 0 | 5 | 0 | 18 | 34 |
| Hr Total | 0 | 10 | 0 | 8 | | 0 | 0 | 0 | 6 | | 0 | 0 | 0 | 5 | | 0 | 11 | 0 | 80 | 120 |
| ----- * BREAK * ----- | | | | | | | | | | | | | | | | | | | | |
| 16:00 | 0 | 1 | 0 | 3 | | 0 | 0 | 0 | 6 | | 0 | 0 | 0 | 3 | | 0 | 0 | 0 | 14 | 27 |
| 16:15 | 0 | 3 | 0 | 1 | | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 6 | | 0 | 3 | 0 | 33 | 47 |
| 16:30 | 0 | 3 | 0 | 1 | | 0 | 2 | 0 | 4 | | 0 | 0 | 0 | 4 | | 0 | 4 | 0 | 36 | 54 |
| 16:45 | 0 | 7 | 0 | 1 | | 0 | 3 | 0 | 5 | | 0 | 0 | 0 | 4 | | 0 | 2 | 0 | 15 | 37 |
| Hr Total | 0 | 14 | 0 | 6 | | 0 | 5 | 0 | 16 | | 0 | 0 | 0 | 17 | | 0 | 9 | 0 | 98 | 165 |
| 17:00 | 0 | 1 | 0 | 4 | | 0 | 1 | 0 | 2 | | 0 | 0 | 0 | 4 | | 0 | 3 | 0 | 25 | 40 |
| 17:15 | 0 | 5 | 0 | 0 | | 0 | 3 | 0 | 1 | | 0 | 1 | 0 | 2 | | 0 | 4 | 0 | 38 | 54 |
| 17:30 | 0 | 6 | 0 | 2 | | 0 | 0 | 0 | 4 | | 0 | 0 | 0 | 4 | | 0 | 3 | 0 | 29 | 48 |
| 17:45 | 0 | 5 | 0 | 2 | | 0 | 0 | 0 | 1 | | 0 | 2 | 0 | 0 | | 0 | 3 | 0 | 22 | 35 |
| Hr Total | 0 | 17 | 0 | 8 | | 0 | 4 | 0 | 8 | | 0 | 3 | 0 | 10 | | 0 | 13 | 0 | 114 | 177 |
| *TOTAL* | 0 | 53 | 0 | 32 | | 0 | 17 | 0 | 35 | | 0 | 3 | 0 | 38 | | 0 | 42 | 0 | 351 | 571 |

North



Miami, Florida

February 04, 2016

drawn by: Luis Palomino
signalized

Traffic Survey Specialists, Inc.

SE 26TH ROAD & US 1/BRICKELL AVENUE

MIAMI, FLORIDA

COUNTED BY: S. SALVO, D. GONZALEZ, & I.

GONZALEZ, SIGNALIZED

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Phone (561) 272-3255

Site Code : 00160031

Start Date: 02/04/16

File I.D. : 26RDBRIC

Page : 1

ALL VEHICLES

| BRICKELL AVENUE | | | | SE 26TH ROAD | | | | US 1 | | | | SE 26TH ROAD | | | | |
|-----------------------|------|------|-------|--------------|------|------|-------|------------|------|------|-------|--------------|------|------|-------|------------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/04/16 ----- | | | | | | | | | | | | | | | | |
| 07:00 | 1 | 13 | 113 | 9 | 0 | 0 | 47 | 15 | 0 | 0 | 106 | 118 | 0 | 21 | 174 | 11 628 |
| 07:15 | 0 | 32 | 158 | 6 | 0 | 0 | 89 | 31 | 0 | 0 | 117 | 174 | 0 | 42 | 276 | 2 927 |
| 07:30 | 0 | 55 | 158 | 14 | 0 | 0 | 72 | 31 | 0 | 6 | 158 | 162 | 0 | 39 | 309 | 7 1011 |
| 07:45 | 0 | 46 | 136 | 22 | 0 | 0 | 66 | 56 | 0 | 0 | 169 | 163 | 0 | 44 | 349 | 5 1056 |
| Hr Total | 1 | 146 | 565 | 51 | 0 | 0 | 274 | 133 | 0 | 6 | 550 | 617 | 0 | 146 | 1108 | 25 3622 |
| 08:00 | 0 | 35 | 160 | 42 | 0 | 0 | 55 | 61 | 0 | 0 | 182 | 153 | 0 | 51 | 228 | 8 975 |
| 08:15 | 0 | 23 | 123 | 13 | 0 | 0 | 30 | 58 | 0 | 0 | 166 | 113 | 0 | 49 | 308 | 2 885 |
| 08:30 | 0 | 39 | 126 | 23 | 0 | 0 | 41 | 68 | 0 | 8 | 250 | 137 | 0 | 66 | 286 | 4 1048 |
| 08:45 | 0 | 37 | 145 | 23 | 0 | 0 | 80 | 79 | 0 | 0 | 307 | 139 | 0 | 66 | 412 | 4 1292 |
| Hr Total | 0 | 134 | 554 | 101 | 0 | 0 | 206 | 266 | 0 | 8 | 905 | 542 | 0 | 232 | 1234 | 18 4200 |
| ----- * BREAK * ----- | | | | | | | | | | | | | | | | |
| 16:00 | 1 | 44 | 158 | 14 | 0 | 0 | 105 | 46 | 0 | 0 | 119 | 132 | 1 | 44 | 155 | 4 823 |
| 16:15 | 1 | 51 | 147 | 17 | 0 | 0 | 103 | 48 | 0 | 0 | 146 | 124 | 0 | 70 | 155 | 6 868 |
| 16:30 | 1 | 30 | 180 | 7 | 0 | 0 | 118 | 42 | 0 | 0 | 116 | 138 | 0 | 47 | 229 | 5 913 |
| 16:45 | 1 | 41 | 155 | 17 | 0 | 0 | 102 | 39 | 0 | 0 | 131 | 111 | 0 | 64 | 195 | 8 864 |
| Hr Total | 4 | 166 | 640 | 55 | 0 | 0 | 428 | 175 | 0 | 0 | 512 | 505 | 1 | 225 | 734 | 23 3468 |
| 17:00 | 2 | 44 | 185 | 10 | 1 | 0 | 109 | 52 | 0 | 0 | 159 | 87 | 0 | 57 | 209 | 5 920 |
| 17:15 | 0 | 54 | 226 | 7 | 0 | 1 | 114 | 53 | 0 | 0 | 183 | 107 | 0 | 86 | 194 | 4 1029 |
| 17:30 | 0 | 70 | 204 | 10 | 0 | 1 | 104 | 50 | 0 | 0 | 149 | 132 | 0 | 79 | 163 | 4 966 |
| 17:45 | 0 | 52 | 192 | 11 | 1 | 0 | 93 | 48 | 0 | 0 | 215 | 126 | 0 | 84 | 200 | 1 1023 |
| Hr Total | 2 | 220 | 807 | 38 | 2 | 2 | 420 | 203 | 0 | 0 | 706 | 452 | 0 | 306 | 766 | 14 3938 |
| *TOTAL* | 7 | 666 | 2566 | 245 | 2 | 2 | 1328 | 777 | 0 | 14 | 2673 | 2116 | 1 | 909 | 3842 | 80 15228 |

Traffic Survey Specialists, Inc.

SE 26TH ROAD & US 1/BRICKELL AVENUE

MIAMI, FLORIDA

COUNTED BY: S. SALVO, D. GONZALEZ, & I.

GONZALEZ, SIGNALIZED

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Phone (561) 272-3255

Site Code : 00160031

Start Date: 02/04/16

File I.D. : 26RDBRIC

Page : 2

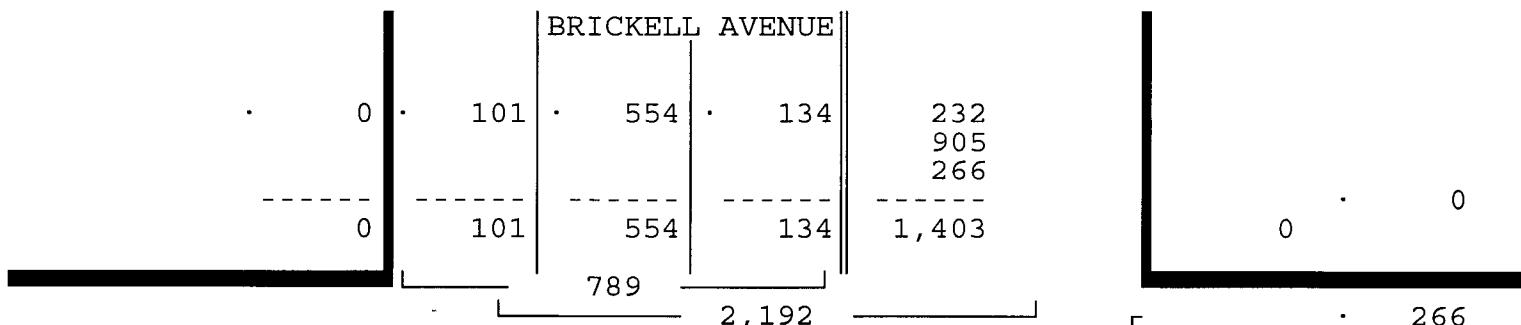
ALL VEHICLES

| BRICKELL AVENUE | | | | SE 26TH ROAD | | | | US 1 | | | | SE 26TH ROAD | | | |
|-----------------|------|------|-------|----------------|------|------|-------|------------|------|------|-------|----------------|------|------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | |
| Westbound | | | | Northwestbound | | | | Eastbound | | | | Southeastbound | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right |

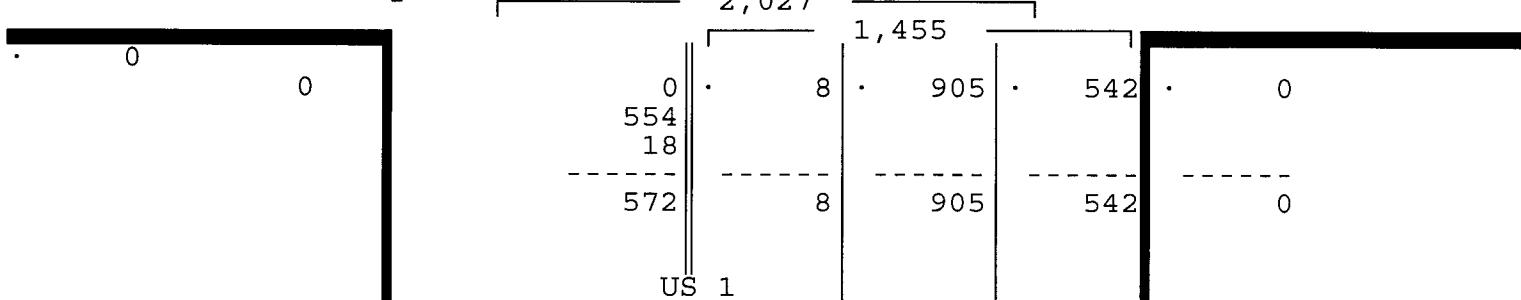
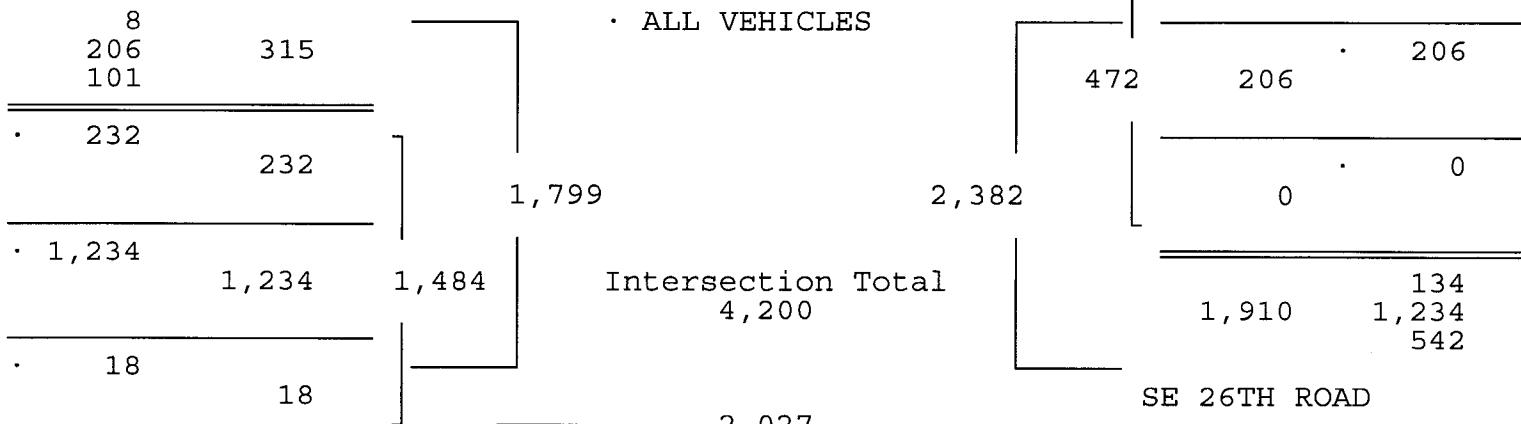
Date 02/04/16 -----

Peak Hour Analysis By Entire Intersection for the Period: 07:00 to 09:00 on 02/04/16

| Peak start | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | 08:00 | |
|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----|
| Volume | 0 | 134 | 554 | 101 | 0 | 0 | 206 | 266 | 0 | 8 | 905 | 542 | 0 | 232 | 1234 | 18 |
| Percent | 0% | 17% | 70% | 13% | 0% | 0% | 44% | 56% | 0% | 1% | 62% | 37% | 0% | 16% | 83% | 1% |
| Pk total | 789 | | | | 472 | | | | 1455 | | | | 1484 | | | |
| Highest | 08:00 | | | | 08:45 | | | | 08:45 | | | | 08:45 | | | |
| Volume | 0 | 35 | 160 | 42 | 0 | 0 | 80 | 79 | 0 | 0 | 307 | 139 | 0 | 66 | 412 | 4 |
| Hi total | 237 | | | | 159 | | | | 446 | | | | 482 | | | |
| PHF | .83 | | | | .74 | | | | .82 | | | | .77 | | | |



SE 26TH ROAD



Traffic Survey Specialists, Inc.

SE 26TH ROAD & US 1/BRICKELL AVENUE

MIAMI, FLORIDA

COUNTED BY: S. SALVO, D. GONZALEZ, & I.

GONZALEZ, SIGNALIZED

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Phone (561) 272-3255

Site Code : 00160031

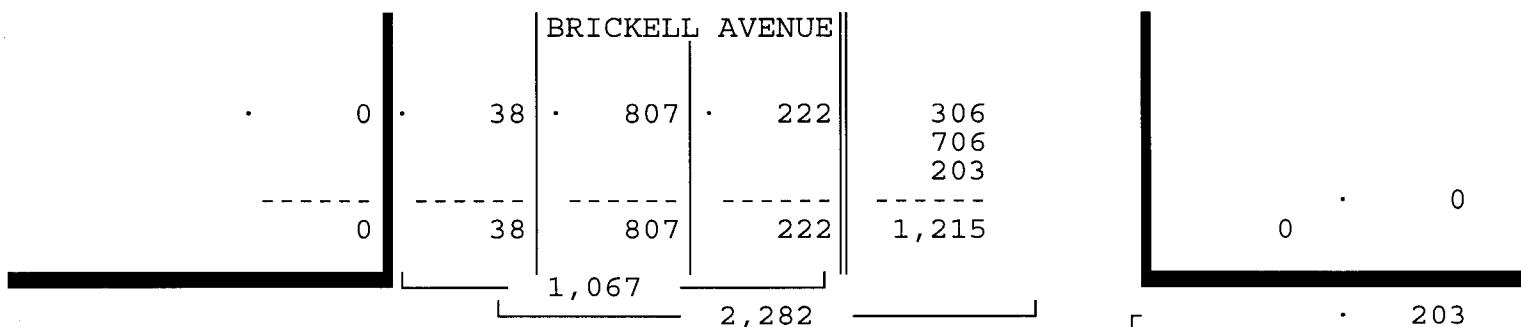
Start Date: 02/04/16

File I.D. : 26RDBRIC

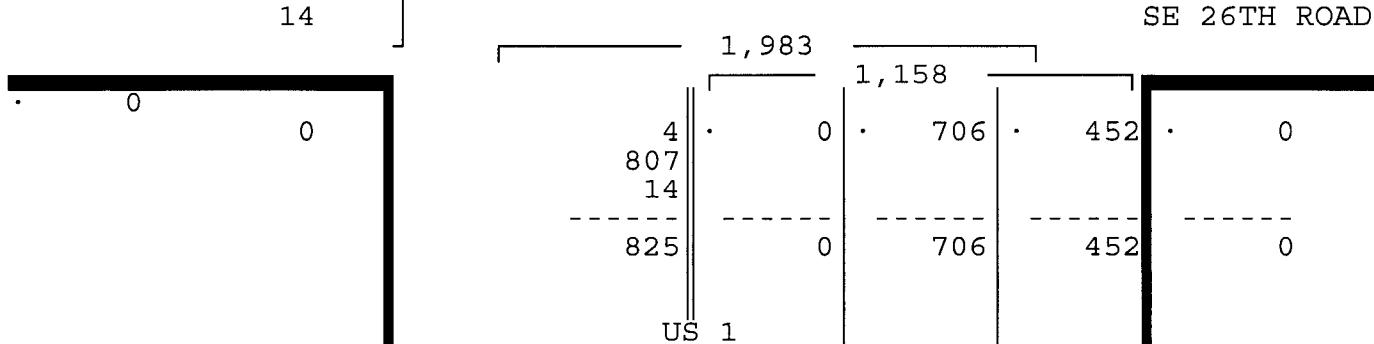
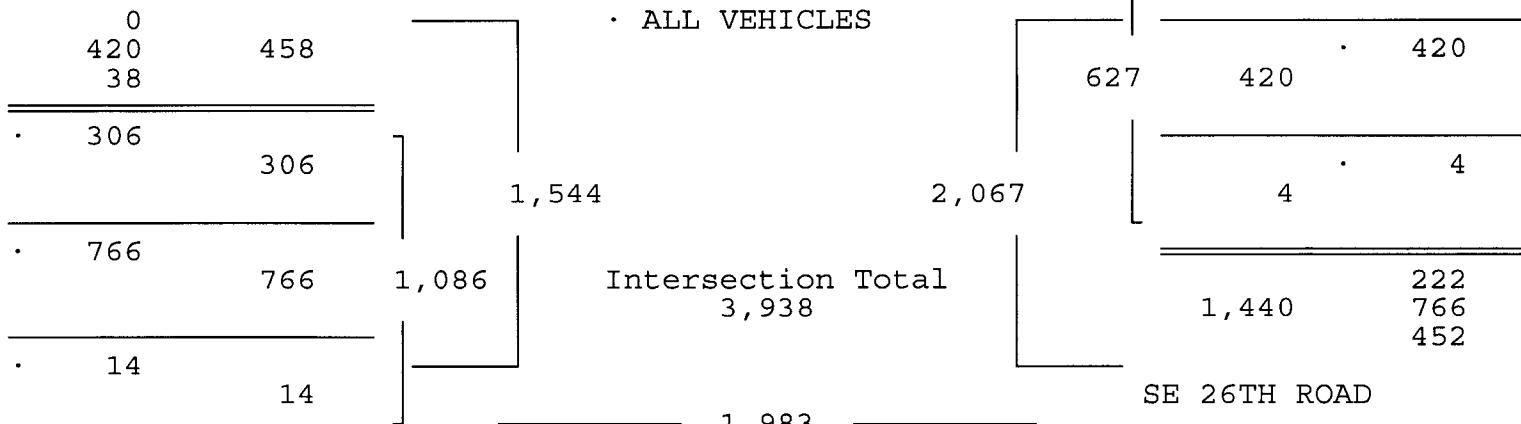
Page : 3

ALL VEHICLES

| BRICKELL AVENUE | | | | SE 26TH ROAD | | | | US 1 | | | | SE 26TH ROAD | | | | |
|--|-------|------|-------|--------------|-------|------|-------|------------|------|------|-------|--------------|-------|------|-------|-------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | UTurn | Left | Thru | Right | Total |
| Date 02/04/16 ----- | | | | | | | | | | | | | | | | |
| Peak Hour Analysis By Entire Intersection for the Period: 16:00 to 18:00 on 02/04/16 | | | | | | | | | | | | | | | | |
| Peak start 17:00 17:00 17:00 17:00 | | | | | | | | | | | | | | | | |
| Volume | 2 | 220 | 807 | 38 | 2 | 2 | 420 | 203 | 0 | 0 | 706 | 452 | 0 | 306 | 766 | 14 |
| Percent | 0% | 21% | 76% | 4% | 0% | 0% | 67% | 32% | 0% | 0% | 61% | 39% | 0% | 28% | 71% | 1% |
| Pk total | 1067 | | | | 627 | | | 1158 | | | | | 1086 | | | |
| Highest | 17:15 | | | | 17:15 | | | 17:45 | | | | | 17:45 | | | |
| Volume | 0 | 54 | 226 | 7 | 0 | 1 | 114 | 53 | 0 | 0 | 215 | 126 | 0 | 84 | 200 | 1 |
| Hi total | 287 | | | | 168 | | | 341 | | | | | 285 | | | |
| PHF | .93 | | | | .93 | | | .85 | | | | | .95 | | | |



SE 26TH ROAD



Traffic Survey Specialists, Inc.

SE 26TH ROAD & US 1/BRICKELL AVENUE

MIAMI, FLORIDA

COUNTED BY: S. SALVO, D. GONZALEZ, & I.

GONZALEZ, SIGNALIZED

85 SE 4th Avenue, Unit 109

Delray Beach, Florida 33483

Phone (561) 272-3255

Site Code : 00160031

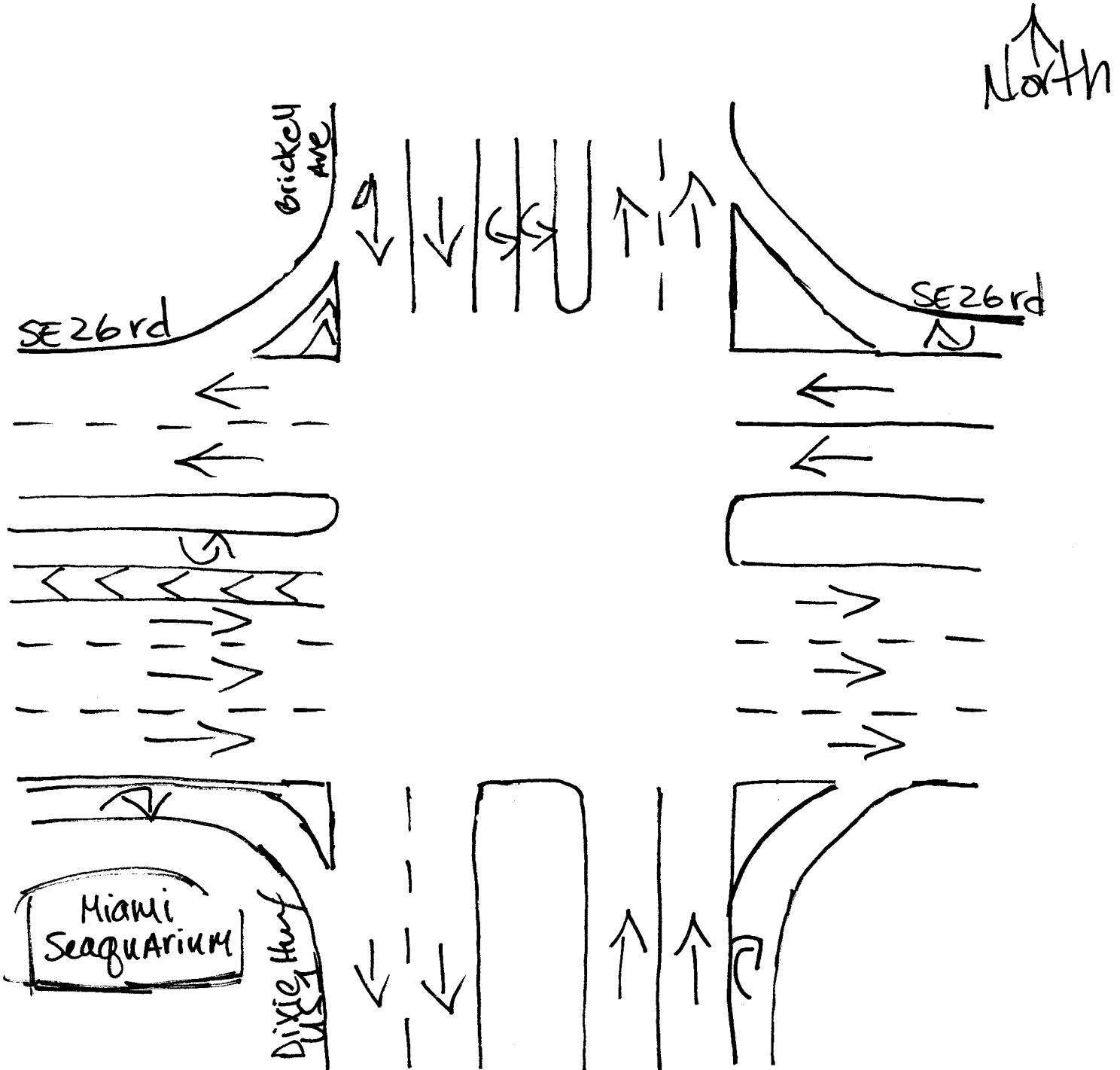
Start Date: 02/04/16

File I.D. : 26RDBRIC

Page : 1

PEDESTRIANS & BIKES

| BRICKELL AVENUE | | | | SE 26TH ROAD | | | | US 1 | | | | SE 26TH ROAD | | | | |
|-----------------------|-------|-------|------|----------------|-------|-------|------|------------|-------|-------|------|----------------|-------|-------|------|----------|
| From North | | | | From East | | | | From South | | | | From West | | | | |
| Westbound | | | | Northwestbound | | | | Eastbound | | | | Southeastbound | | | | |
| Left | BIKES | Right | Peds | Left | BIKES | Right | Peds | Left | BIKES | Right | Peds | Left | BIKES | Right | Peds | Total |
| Date 02/04/16 ----- | | | | | | | | | | | | | | | | |
| 07:00 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 6 | 0 | 2 | 0 | 9 | 0 | 11 38 |
| 07:15 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 11 | 0 | 4 | 0 | 2 | 0 | 3 | 0 | 0 22 |
| 07:30 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 10 | 0 | 7 | 0 | 7 | 0 | 1 | 0 | 2 35 |
| 07:45 | 0 | 7 | 0 | 0 | 0 | 5 | 0 | 8 | 0 | 6 | 0 | 3 | 0 | 0 | 1 | 0 30 |
| Hr Total | 0 | 7 | 0 | 0 | 0 | 20 | 0 | 34 | 0 | 23 | 0 | 14 | 0 | 13 | 0 | 14 125 |
| 08:00 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 5 | 0 | 4 | 0 | 0 | 0 | 5 | 0 | 1 20 |
| 08:15 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 12 | 0 | 8 | 0 | 1 | 0 | 5 | 0 | 1 31 |
| 08:30 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 12 | 0 | 3 | 0 | 3 | 0 | 1 | 0 | 0 21 |
| 08:45 | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 13 |
| Hr Total | 0 | 8 | 0 | 0 | 0 | 10 | 0 | 33 | 0 | 16 | 0 | 5 | 0 | 11 | 0 | 2 85 |
| ----- * BREAK * ----- | | | | | | | | | | | | | | | | |
| 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 6 |
| 16:15 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | 12 | 0 | 17 | 0 | 2 | 0 | 0 | 0 | 1 37 |
| 16:30 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 6 | 0 | 2 | 0 | 2 | 0 | 0 | 5 | 0 20 |
| 16:45 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 12 | 0 | 5 | 0 | 2 | 0 | 0 | 0 | 0 24 |
| Hr Total | 0 | 0 | 0 | 7 | 0 | 8 | 0 | 35 | 0 | 24 | 0 | 7 | 0 | 0 | 0 | 6 87 |
| 17:00 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 5 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 0 11 |
| 17:15 | 0 | 2 | 0 | 1 | 0 | 6 | 0 | 7 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 20 |
| 17:30 | 0 | 3 | 0 | 3 | 0 | 10 | 0 | 9 | 0 | 5 | 0 | 3 | 0 | 0 | 0 | 2 35 |
| 17:45 | 0 | 1 | 0 | 4 | 0 | 3 | 0 | 15 | 0 | 5 | 0 | 3 | 0 | 0 | 0 | 0 31 |
| Hr Total | 0 | 6 | 0 | 8 | 0 | 20 | 0 | 36 | 0 | 15 | 0 | 10 | 0 | 0 | 0 | 2 97 |
| *TOTAL* | 0 | 21 | 0 | 15 | 0 | 58 | 0 | 138 | 0 | 78 | 0 | 36 | 0 | 24 | 0 | 24 394 |



Miami, Florida

February 04, 2016

drawn by: Luis Palomino
signaled

Attachment G

2014 PEAK SEASON FACTOR CATEGORY REPORT - REPORT TYPE: ALL
 CATEGORY: 8701 MIAMI-DADE SOUTH

MOCF: 0.99
 PSCF

| WEEK | DATES | SF | |
|------|-------------------------|------|------|
| 1 | 01/01/2014 - 01/04/2014 | 0.98 | 0.99 |
| 2 | 01/05/2014 - 01/11/2014 | 1.01 | 1.02 |
| 3 | 01/12/2014 - 01/18/2014 | 1.03 | 1.04 |
| 4 | 01/19/2014 - 01/25/2014 | 1.02 | 1.03 |
| 5 | 01/26/2014 - 02/01/2014 | 1.01 | 1.02 |
| 6 | 02/02/2014 - 02/08/2014 | 1.00 | 1.01 |
| 7 | 02/09/2014 - 02/15/2014 | 1.00 | 1.01 |
| 8 | 02/16/2014 - 02/22/2014 | 0.99 | 1.00 |
| * 9 | 02/23/2014 - 03/01/2014 | 0.99 | 1.00 |
| *10 | 03/02/2014 - 03/08/2014 | 0.99 | 1.00 |
| *11 | 03/09/2014 - 03/15/2014 | 0.99 | 1.00 |
| *12 | 03/16/2014 - 03/22/2014 | 0.99 | 1.00 |
| *13 | 03/23/2014 - 03/29/2014 | 0.99 | 1.00 |
| *14 | 03/30/2014 - 04/05/2014 | 0.99 | 1.00 |
| *15 | 04/06/2014 - 04/12/2014 | 0.99 | 1.00 |
| *16 | 04/13/2014 - 04/19/2014 | 0.99 | 1.00 |
| *17 | 04/20/2014 - 04/26/2014 | 0.99 | 1.00 |
| *18 | 04/27/2014 - 05/03/2014 | 0.99 | 1.00 |
| *19 | 05/04/2014 - 05/10/2014 | 0.99 | 1.00 |
| *20 | 05/11/2014 - 05/17/2014 | 0.99 | 1.00 |
| *21 | 05/18/2014 - 05/24/2014 | 0.99 | 1.00 |
| 22 | 05/25/2014 - 05/31/2014 | 1.00 | 1.01 |
| 23 | 06/01/2014 - 06/07/2014 | 1.01 | 1.02 |
| 24 | 06/08/2014 - 06/14/2014 | 1.01 | 1.02 |
| 25 | 06/15/2014 - 06/21/2014 | 1.02 | 1.03 |
| 26 | 06/22/2014 - 06/28/2014 | 1.02 | 1.03 |
| 27 | 06/29/2014 - 07/05/2014 | 1.03 | 1.04 |
| 28 | 07/06/2014 - 07/12/2014 | 1.03 | 1.04 |
| 29 | 07/13/2014 - 07/19/2014 | 1.04 | 1.05 |
| 30 | 07/20/2014 - 07/26/2014 | 1.03 | 1.04 |
| 31 | 07/27/2014 - 08/02/2014 | 1.02 | 1.03 |
| 32 | 08/03/2014 - 08/09/2014 | 1.02 | 1.03 |
| 33 | 08/10/2014 - 08/16/2014 | 1.01 | 1.02 |
| 34 | 08/17/2014 - 08/23/2014 | 1.00 | 1.01 |
| 35 | 08/24/2014 - 08/30/2014 | 1.01 | 1.02 |
| 36 | 08/31/2014 - 09/06/2014 | 1.01 | 1.02 |
| 37 | 09/07/2014 - 09/13/2014 | 1.01 | 1.02 |
| 38 | 09/14/2014 - 09/20/2014 | 1.01 | 1.02 |
| 39 | 09/21/2014 - 09/27/2014 | 1.01 | 1.02 |
| 40 | 09/28/2014 - 10/04/2014 | 1.00 | 1.01 |
| 41 | 10/05/2014 - 10/11/2014 | 1.00 | 1.01 |
| 42 | 10/12/2014 - 10/18/2014 | 0.99 | 1.00 |
| 43 | 10/19/2014 - 10/25/2014 | 0.99 | 1.00 |
| 44 | 10/26/2014 - 11/01/2014 | 1.00 | 1.01 |
| 45 | 11/02/2014 - 11/08/2014 | 1.00 | 1.01 |
| 46 | 11/09/2014 - 11/15/2014 | 1.00 | 1.01 |
| 47 | 11/16/2014 - 11/22/2014 | 1.00 | 1.01 |
| 48 | 11/23/2014 - 11/29/2014 | 1.00 | 1.01 |
| 49 | 11/30/2014 - 12/06/2014 | 0.99 | 1.00 |
| 50 | 12/07/2014 - 12/13/2014 | 0.99 | 1.00 |
| 51 | 12/14/2014 - 12/20/2014 | 0.98 | 0.99 |
| 52 | 12/21/2014 - 12/27/2014 | 1.01 | 1.02 |
| 53 | 12/28/2014 - 12/31/2014 | 1.03 | 1.04 |

* PEAK SEASON

09-MAR-2015 16:07:55

830UPD

6_8701_PKSEASON.TXT

TRAFFIC VOLUMES AT STUDY INTERSECTIONS

INTERSECTION: US 1 at SW 88 Street
 COUNT DATE: February 3, 2016
 AM PEAK HOUR FACTOR: 0.95
 PM PEAK HOUR FACTOR: 0.98

| | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR | | |
|-------------------------------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----|-----|
| AM Raw Turning Movements | | 471 | 393 | 37 | | 85 | 283 | 47 | | | 1,275 | 84 | | 97 | 1,075 | 397 | | |
| Peak Season Correction Factor | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | | |
| AM EXISTING CONDITIONS | | 476 | 397 | 37 | | 86 | 286 | 47 | | | 1,288 | 85 | | 98 | 1,086 | 401 | | |
| "PM EXISTING TRAFFIC" | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR | | |
| PM Raw Turning Movements | | 446 | 453 | 486 | | 141 | 489 | 39 | | | 1,337 | 124 | | 111 | 1,821 | 639 | | |
| Peak Season Correction Factor | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | | |
| PM EXISTING CONDITIONS | | 450 | 458 | 491 | | 142 | 494 | 39 | | | 1,350 | 125 | | 112 | 1,839 | 645 | | |
| "AM BACKGROUND TRAFFIC" | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR | | |
| TOTAL "VESTED" TRAFFIC | | 0 | 0 | 0 | | 0 | 0 | 0 | | | 0 | 0 | | 0 | 0 | 0 | | |
| Years To Buildout | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | |
| Yearly Growth Rate | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | | |
| AM BACKGROUND TRAFFIC GROWTH | | 7 | 6 | 1 | | 1 | 4 | 1 | | | 19 | 1 | | 1 | 16 | 6 | | |
| AM NON-PROJECT TRAFFIC | | 483 | 403 | 38 | | 87 | 290 | 48 | | | 1,307 | 86 | | 99 | 1,102 | 407 | | |
| AM PROJECT TRAFFIC | | 483 | 403 | 38 | | 87 | 290 | 48 | | | 1,288 | 86 | | 99 | 1,086 | 407 | | |
| "PM BACKGROUND TRAFFIC" | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR | | |
| TOTAL "VESTED" TRAFFIC | | 0 | 0 | 0 | | 0 | 0 | 0 | | | 0 | 0 | | 0 | 0 | 0 | | |
| Years To Buildout | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | |
| Yearly Growth Rate | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | | |
| PM BACKGROUND TRAFFIC GROWTH | | 7 | 7 | 7 | | 2 | 7 | 1 | | | 20 | 2 | | 2 | 28 | 10 | | |
| PM NON-PROJECT TRAFFIC | | 457 | 465 | 498 | | 144 | 501 | 40 | | | 1,370 | 127 | | 114 | 1,867 | 655 | | |
| PM PROJECT TRAFFIC | | 457 | 465 | 498 | | 144 | 501 | 40 | | | 1,350 | 127 | | 114 | 1,839 | 655 | | |
| "PROJECT DISTRIBUTION" | LAND USE | TYPE | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Pass-By Distribution | Entering | | | | | | | | | | | | | | | | | |
| | Exiting | | | | | | | | | | | | | | | | | |
| Net New Distribution | Entering | | | | | | | | | | | | | | | | | |
| | Exiting | | | | | | | | | | | | | | | | | |
| "AM PROJECT TRAFFIC" | LAND USE | TYPE | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Project Trips | Pass - By | | | | | | | | | | | | | | | | | |
| | Net New | | | | | | | | | | | | | | | | | |
| AM TOTAL PROJECT TRAFFIC | | 0 | 0 | 0 | | 0 | 0 | 0 | | | 0 | 0 | | 0 | 0 | 0 | 0 | |
| AM TOTAL TRAFFIC | | 483 | 403 | 38 | | 87 | 290 | 48 | | | 1,307 | 86 | | 99 | 1,102 | 407 | | |
| "PM PROJECT TRAFFIC" | LAND USE | TYPE | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Project Trips | Pass - By | | | | | | | | | | | | | | | | | |
| | Net New | | | | | | | | | | | | | | | | | |
| PM TOTAL PROJECT TRAFFIC | | 457 | 465 | 498 | | 144 | 501 | 40 | | | 1,370 | 127 | | 114 | 1,867 | 655 | | |
| PM TOTAL TRAFFIC | | 457 | 465 | 498 | | 144 | 501 | 40 | | | 1,350 | 127 | | 114 | 1,839 | 655 | | |

TRAFFIC VOLUMES AT STUDY INTERSECTIONS

INTERSECTION: US 1 at SW 72 Street/Sunset Drive
COUNT DATE: February 3, 2016
AM PEAK HOUR FACTOR: 0.96
PM PEAK HOUR FACTOR: 0.97

TRAFFIC VOLUMES AT STUDY INTERSECTIONS

INTERSECTION: US 1 at SW 40 Street
COUNT DATE: February 3, 2016
AM PEAK HOUR FACTOR: 0.94
PM PEAK HOUR FACTOR: 0.95

| "AM EXISTING TRAFFIC" | | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR | | |
|-------------------------------|-----------|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----|-----|
| AM Raw Turning Movements | | | 474 | 191 | 4 | | 213 | 267 | | | | 2,706 | 139 | | 9 | 2,145 | 484 | | |
| Peak Season Correction Factor | | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | | |
| AM EXISTING CONDITIONS | | | 479 | 193 | 4 | | 215 | 270 | | | | 2,733 | 140 | | 9 | 2,166 | 489 | | |
| "PM EXISTING TRAFFIC" | | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR | | |
| PM Raw Turning Movements | | | 363 | 135 | 20 | | 170 | 311 | 3 | | 1 | 2,286 | 198 | | 2,074 | 615 | | | |
| Peak Season Correction Factor | | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | 1.010 | | |
| PM EXISTING CONDITIONS | | | 367 | 136 | 20 | | 172 | 314 | 3 | | 1 | 2,309 | 200 | | | 2,095 | 621 | | |
| "AM BACKGROUND TRAFFIC" | | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| TOTAL "VESTED" TRAFFIC | | 0 | 0 | 0 | | 0 | 0 | | | | | 0 | 0 | | 0 | 0 | 0 | | |
| Years To Buildout | | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | |
| Yearly Growth Rate | | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | | |
| AM BACKGROUND TRAFFIC GROWTH | | 7 | 3 | 0 | | 3 | 4 | | | | | 41 | 2 | | 0 | 33 | 7 | | |
| AM NON-PROJECT TRAFFIC | | 486 | 196 | 4 | | 218 | 274 | | | | | 2,774 | 142 | | 9 | 2,199 | 496 | | |
| AM PROJECT TRAFFIC | | 486 | 196 | 4 | | 218 | 274 | | | | | 2,741 | 142 | | 9 | 2,173 | 496 | | |
| "PM BACKGROUND TRAFFIC" | | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| TOTAL "VESTED" TRAFFIC | | 0 | 0 | 0 | | 0 | 0 | | | | | 0 | 0 | | 0 | 0 | 0 | | |
| Years To Buildout | | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | |
| Yearly Growth Rate | | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | | |
| PM BACKGROUND TRAFFIC GROWTH | | 6 | 2 | 0 | | 3 | 5 | 0 | | | | 0 | 35 | 3 | | 32 | 9 | | |
| PM NON-PROJECT TRAFFIC | | 373 | 138 | 20 | | 175 | 319 | 3 | | | 1 | 2,344 | 203 | | 0 | 2,127 | 630 | | |
| PM PROJECT TRAFFIC | | 373 | 138 | 20 | | 175 | 319 | 3 | | | 1 | 2,316 | 203 | | 0 | 2,101 | 630 | | |
| "PROJECT DISTRIBUTION" | | LAND USE | TYPE | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Pass-By Distribution | Entering | | | | | | | | | | | | | | | | | | |
| | Exiting | | | | | | | | | | | | | | | | | | |
| Net New Distribution | Entering | | | | | | | | | | | | | | | | | | |
| | Exiting | | | | | | | | | | | | | | | | | | |
| "AM PROJECT TRAFFIC" | | LAND USE | TYPE | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Project Trips | Pass - By | | | | | | | | | | | | | | | | | | |
| | Net New | | | | | | | | | | | | | | | | | | |
| AM TOTAL PROJECT TRAFFIC | | 0 | 0 | 0 | | 0 | 0 | | | | | 0 | 0 | | 0 | 0 | 0 | | |
| AM TOTAL TRAFFIC | | 486 | 196 | 4 | | 218 | 274 | | | | | 2,774 | 142 | | 9 | 2,199 | 496 | | |
| "PM PROJECT TRAFFIC" | | LAND USE | TYPE | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Project Trips | Pass - By | | | | | | | | | | | | | | | | | | |
| | Net New | | | | | | | | | | | | | | | | | | |
| PM TOTAL PROJECT TRAFFIC | | 0 | 0 | 0 | | 0 | 0 | | | | | 0 | 0 | | 0 | 0 | 0 | | |

TRAFFIC VOLUMES AT STUDY INTERSECTIONS

INTERSECTION: US 1 at SW 27 Avenue
COUNT DATE: February 3, 2016
AM PEAK HOUR FACTOR: 0.97
PM PEAK HOUR FACTOR: 1

TRAFFIC VOLUMES AT STUDY INTERSECTIONS

INTERSECTION: Brickell Avenue at SE 26 Road
COUNT DATE: February 4, 2016
AM PEAK HOUR FACTOR: 0.81
PM PEAK HOUR FACTOR: 0.96

Attachment H

Timings

1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2016 Existing Conditions

A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | SWL | SWT | SWR |
|----------------------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 476 | 397 | 37 | 86 | 286 | 47 | 1288 | 98 | 1086 | 401 |
| Future Volume (vph) | 476 | 397 | 37 | 86 | 286 | 47 | 1288 | 98 | 1086 | 401 |
| Turn Type | Split | NA | Free | Split | NA | Perm | NA | pm+pt | NA | pm+ov |
| Protected Phases | 8 | 8 | | 7 | 7 | | 6 | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | 7 | | 2 | | 2 |
| Detector Phase | 8 | 8 | | 7 | 7 | 7 | 6 | 5 | 2 | 8 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 39.0 | 39.0 | | 15.9 | 15.9 | 15.9 | 40.7 | 11.8 | 40.7 | 39.0 |
| Total Split (s) | 39.0 | 39.0 | | 39.0 | 39.0 | 39.0 | 98.0 | 14.0 | 112.0 | 39.0 |
| Total Split (%) | 20.5% | 20.5% | | 20.5% | 20.5% | 20.5% | 51.6% | 7.4% | 58.9% | 20.5% |
| Yellow Time (s) | 4.8 | 4.8 | | 4.0 | 4.0 | 4.0 | 4.8 | 4.8 | 4.8 | 4.8 |
| All-Red Time (s) | 2.9 | 2.9 | | 4.1 | 4.1 | 4.1 | 2.9 | 2.0 | 2.9 | 2.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | 7.7 | 6.8 | 7.7 | 7.7 |
| Lead/Lag | Lag | Lag | | Lead | Lead | Lead | Lag | Lead | | Lag |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | | Yes |
| Recall Mode | None | None | | None | None | None | C-Min | None | C-Min | None |

Intersection Summary

Cycle Length: 190

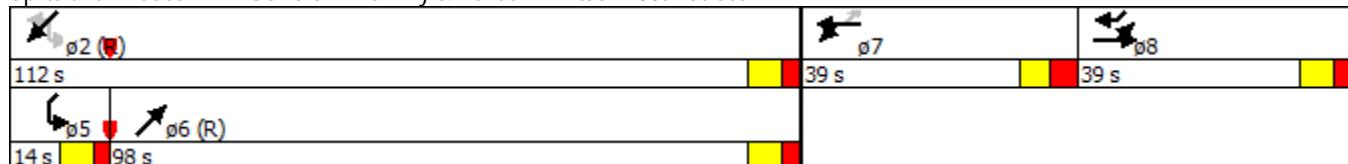
Actuated Cycle Length: 190

Offset: 61 (32%), Referenced to phase 2:SWTL and 6:NET, Start of Green

Natural Cycle: 110

Control Type: Actuated-Coordinated

Splits and Phases: 1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street



HCM Signalized Intersection Capacity Analysis
1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2016 Existing Conditions

A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|------------------------|-------|------|-------|-------|-------|------|------|------|-------|------|-------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 476 | 397 | 37 | 86 | 286 | 47 | 0 | 1288 | 85 | 98 | 1086 | 401 |
| Future Volume (vph) | 476 | 397 | 37 | 86 | 286 | 47 | 0 | 1288 | 85 | 98 | 1086 | 401 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.7 | 7.7 | 4.0 | 8.1 | 8.1 | 8.1 | | 7.7 | | 6.8 | 7.7 | 7.7 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | | 1.00 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1610 | 3336 | 1564 | 1770 | 3539 | 1557 | | 5034 | | 1770 | 5085 | 1572 |
| Flt Permitted | 0.95 | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.06 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1610 | 3336 | 1564 | 1770 | 3539 | 1557 | | 5034 | | 120 | 5085 | 1572 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 501 | 418 | 39 | 91 | 301 | 49 | 0 | 1356 | 89 | 103 | 1143 | 422 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 43 | 0 | 4 | 0 | 0 | 0 | 22 |
| Lane Group Flow (vph) | 301 | 618 | 39 | 91 | 301 | 6 | 0 | 1441 | 0 | 103 | 1143 | 400 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | | | 1 | 1 | | 1 |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Turn Type | Split | NA | Free | Split | NA | Perm | | NA | pm+pt | NA | pm+ov | |
| Protected Phases | 8 | 8 | | 7 | 7 | | | 6 | | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | 7 | | | | 2 | | 2 |
| Actuated Green, G (s) | 57.2 | 57.2 | 190.0 | 23.0 | 23.0 | 23.0 | | 71.0 | 86.3 | 86.3 | 143.5 | |
| Effective Green, g (s) | 57.2 | 57.2 | 190.0 | 23.0 | 23.0 | 23.0 | | 71.0 | 86.3 | 86.3 | 143.5 | |
| Actuated g/C Ratio | 0.30 | 0.30 | 1.00 | 0.12 | 0.12 | 0.12 | | 0.37 | 0.45 | 0.45 | 0.76 | |
| Clearance Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | | 7.7 | 6.8 | 7.7 | 7.7 | |
| Vehicle Extension (s) | 3.5 | 3.5 | | 4.0 | 4.0 | 4.0 | | 1.0 | 2.0 | 1.0 | 3.5 | |
| Lane Grp Cap (vph) | 484 | 1004 | 1564 | 214 | 428 | 188 | | 1881 | | 128 | 2309 | 1250 |
| v/s Ratio Prot | c0.19 | 0.19 | | 0.05 | c0.09 | | | 0.29 | c0.04 | 0.22 | 0.10 | |
| v/s Ratio Perm | | | 0.02 | | | 0.00 | | | c0.33 | | 0.16 | |
| v/c Ratio | 0.62 | 0.62 | 0.02 | 0.43 | 0.70 | 0.03 | | 0.77 | 0.80 | 0.50 | 0.32 | |
| Uniform Delay, d1 | 57.1 | 57.0 | 0.0 | 77.4 | 80.2 | 73.7 | | 52.2 | 39.2 | 36.5 | 7.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.6 | 1.2 | 0.0 | 1.9 | 5.6 | 0.1 | | 3.0 | 28.1 | 0.8 | 0.2 | |
| Delay (s) | 59.7 | 58.2 | 0.0 | 79.2 | 85.8 | 73.8 | | 55.2 | 67.3 | 37.3 | 7.7 | |
| Level of Service | E | E | A | E | F | E | | E | E | D | A | |
| Approach Delay (s) | | 56.3 | | | 83.1 | | | 55.2 | | | 31.6 | |
| Approach LOS | | E | | | F | | | E | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 49.5 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.74 | | |
| Actuated Cycle Length (s) | 190.0 | Sum of lost time (s) | 30.3 |
| Intersection Capacity Utilization | 82.9% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

Timings

2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2016 Existing Conditions

A.M. Peak Hour

| Lane Group | EBT | EBR | WBT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↑ | ↑↓ | ↑ | ↑↑↓ | ↑ | ↑↑↓ |
| Traffic Volume (vph) | 571 | 24 | 265 | 97 | 3434 | 58 | 1808 |
| Future Volume (vph) | 571 | 24 | 265 | 97 | 3434 | 58 | 1808 |
| Turn Type | NA | Perm | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 8 | | 4 | 1 | 6 | 5 | 2 |
| Permitted Phases | | | | 6 | | 2 | |
| Detector Phase | 8 | 8 | 4 | 1 | 6 | 5 | 2 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 12.0 | 12.0 | 12.0 | 5.0 | 7.0 | 5.0 | 7.0 |
| Minimum Split (s) | 34.9 | 34.9 | 34.9 | 11.4 | 37.0 | 11.0 | 37.0 |
| Total Split (s) | 44.0 | 44.0 | 44.0 | 18.0 | 135.0 | 11.0 | 128.0 |
| Total Split (%) | 23.2% | 23.2% | 23.2% | 9.5% | 71.1% | 5.8% | 67.4% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.4 | 4.0 | 4.4 |
| All-Red Time (s) | 4.9 | 4.9 | 4.9 | 2.0 | 3.6 | 2.0 | 3.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.9 | 8.9 | 8.9 | 6.0 | 8.0 | 6.0 | 8.0 |
| Lead/Lag | | | | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | C-Min | None | C-Min |

Intersection Summary

Cycle Length: 190

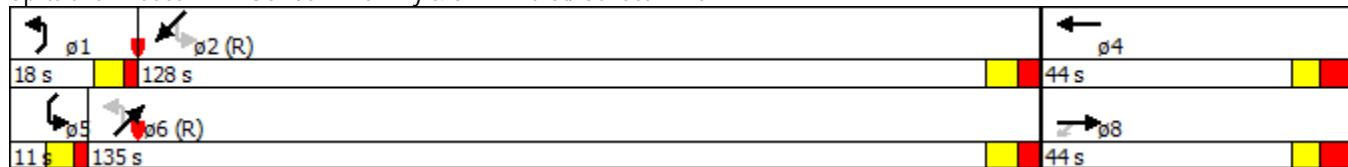
Actuated Cycle Length: 190

Offset: 160 (84%), Referenced to phase 2:SWTL and 6:NETL, Start of Green

Natural Cycle: 145

Control Type: Actuated-Coordinated

Splits and Phases: 2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive



HCM 2010 Signalized Intersection Summary
2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2016 Existing Conditions
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|---------------------------------------|------|-------|------|-------|------|-------|------|-------|-------|------|------|------|
| Lane Configurations | | ↑↑ | ↑ | | ↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | |
| Traffic Volume (veh/h) | 0 | 571 | 24 | 0 | 265 | 3 | 97 | 3434 | 89 | 58 | 1808 | 212 |
| Future Volume (veh/h) | 0 | 571 | 24 | 0 | 265 | 3 | 97 | 3434 | 89 | 58 | 1808 | 212 |
| Number | 3 | 8 | 18 | 7 | 4 | 14 | 1 | 6 | 16 | 5 | 2 | 12 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.98 | 1.00 | | 0.96 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1863 | 1863 | 0 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 0 | 595 | 0 | 0 | 276 | 3 | 101 | 3577 | 93 | 60 | 1883 | 221 |
| Adj No. of Lanes | 0 | 2 | 1 | 0 | 2 | 0 | 1 | 3 | 0 | 1 | 3 | 0 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, % | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 0 | 640 | 286 | 0 | 649 | 7 | 174 | 3431 | 88 | 83 | 3080 | 358 |
| Arrive On Green | 0.00 | 0.18 | 0.00 | 0.00 | 0.18 | 0.18 | 0.03 | 0.67 | 0.67 | 0.03 | 0.67 | 0.67 |
| Sat Flow, veh/h | 0 | 3632 | 1583 | 0 | 3680 | 39 | 1774 | 5095 | 131 | 1774 | 4600 | 535 |
| Grp Volume(v), veh/h | 0 | 595 | 0 | 0 | 136 | 143 | 101 | 2369 | 1301 | 60 | 1383 | 721 |
| Grp Sat Flow(s),veh/h/ln | 0 | 1770 | 1583 | 0 | 1770 | 1856 | 1774 | 1695 | 1836 | 1774 | 1695 | 1744 |
| Q Serve(g_s), s | 0.0 | 31.5 | 0.0 | 0.0 | 13.0 | 13.0 | 3.5 | 127.9 | 127.9 | 2.3 | 43.3 | 44.2 |
| Cycle Q Clear(g_c), s | 0.0 | 31.5 | 0.0 | 0.0 | 13.0 | 13.0 | 3.5 | 127.9 | 127.9 | 2.3 | 43.3 | 44.2 |
| Prop In Lane | 0.00 | | 1.00 | 0.00 | | 0.02 | 1.00 | | 0.07 | 1.00 | | 0.31 |
| Lane Grp Cap(c), veh/h | 0 | 640 | 286 | 0 | 320 | 336 | 174 | 2283 | 1236 | 83 | 2271 | 1168 |
| V/C Ratio(X) | 0.00 | 0.93 | 0.00 | 0.00 | 0.43 | 0.43 | 0.58 | 1.04 | 1.05 | 0.73 | 0.61 | 0.62 |
| Avail Cap(c_a), veh/h | 0 | 654 | 292 | 0 | 327 | 343 | 235 | 2283 | 1236 | 85 | 2271 | 1168 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 76.6 | 0.0 | 0.0 | 69.1 | 69.1 | 19.9 | 31.0 | 31.0 | 54.1 | 17.5 | 17.7 |
| Incr Delay (d2), s/veh | 0.0 | 19.7 | 0.0 | 0.0 | 0.9 | 0.9 | 1.1 | 29.4 | 40.7 | 22.7 | 1.2 | 2.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.0 | 17.1 | 0.0 | 0.0 | 6.4 | 6.8 | 2.6 | 68.9 | 78.5 | 3.6 | 20.6 | 22.0 |
| LnGrp Delay(d),s/veh | 0.0 | 96.3 | 0.0 | 0.0 | 69.9 | 69.9 | 21.0 | 60.4 | 71.7 | 76.8 | 18.7 | 20.1 |
| LnGrp LOS | F | | | | E | E | C | F | F | E | B | C |
| Approach Vol, veh/h | | 595 | | | 279 | | | 3771 | | | 2164 | |
| Approach Delay, s/veh | | 96.3 | | | 69.9 | | | 63.3 | | | 20.8 | |
| Approach LOS | | F | | | E | | | E | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 11.5 | 135.3 | | 43.3 | 10.8 | 135.9 | | 43.3 | | | | |
| Change Period (Y+R _c), s | 6.0 | 8.0 | | * 8.9 | 6.0 | 8.0 | | * 8.9 | | | | |
| Max Green Setting (Gmax), s | 12.0 | 120.0 | | * 35 | 5.0 | 127.0 | | * 35 | | | | |
| Max Q Clear Time (g_c+l1), s | 5.5 | 46.2 | | 15.0 | 4.3 | 129.9 | | 33.5 | | | | |
| Green Ext Time (p_c), s | 0.1 | 60.4 | | 5.7 | 0.0 | 0.0 | | 0.9 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 52.9 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings

3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2016 Existing Conditions

A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | NET | NER | SWT | SWR | ø1 | ø2 |
|----------------------|-------|-------|-------|-------|-------|-------|-------|------|--------|------|-------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ | | |
| Traffic Volume (vph) | 479 | 193 | 4 | 215 | 270 | 2733 | 140 | 2175 | 489 | | |
| Future Volume (vph) | 479 | 193 | 4 | 215 | 270 | 2733 | 140 | 2175 | 489 | | |
| Turn Type | Split | NA | Perm | Split | NA | NA | Prot | NA | custom | | |
| Protected Phases | 3 | 3 | | 4 | 4 | 6 | 6 | 12 | 23 | 1 | 2 |
| Permitted Phases | | | | 3 | | | | | | | |
| Detector Phase | 3 | 3 | 3 | 4 | 4 | 6 | 6 | 12 | 23 | | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 15.0 | 15.0 | | | 1.0 | 15.0 |
| Minimum Split (s) | 26.1 | 26.1 | 26.1 | 26.1 | 26.1 | 25.5 | 25.5 | | | 25.0 | 32.5 |
| Total Split (s) | 33.0 | 33.0 | 33.0 | 28.0 | 28.0 | 129.0 | 129.0 | | | 25.0 | 104.0 |
| Total Split (%) | 17.4% | 17.4% | 17.4% | 14.7% | 14.7% | 67.9% | 67.9% | | | 13% | 55% |
| Yellow Time (s) | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.8 | 4.8 | | | 2.0 | 4.8 |
| All-Red Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 2.7 | 2.7 | | | 0.0 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | 7.5 | 7.5 | | | | |
| Lead/Lag | Lead | Lead | Lead | Lag | Lag | | | | | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | | | | Yes | Yes |
| Recall Mode | None | None | None | None | None | C-Min | C-Min | | | Max | C-Min |

Intersection Summary

Cycle Length: 190

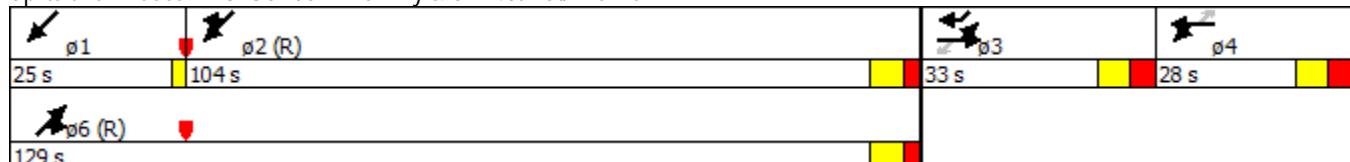
Actuated Cycle Length: 190

Offset: 99 (52%), Referenced to phase 2:SWT and 6:NET, Start of Green

Natural Cycle: 150

Control Type: Actuated-Coordinated

Splits and Phases: 3: US 1/S Dixie Hwy & SW 40th St/Bird Rd



HCM Signalized Intersection Capacity Analysis
3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2016 Existing Conditions

A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|-----------------------------------|-------|-------|-------|-------|-------|------|---------------------------|-------|-------|------|-------|--------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | ↑ | | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 479 | 193 | 4 | 215 | 270 | 0 | 0 | 2733 | 140 | 0 | 2175 | 489 |
| Future Volume (vph) | 479 | 193 | 4 | 215 | 270 | 0 | 0 | 2733 | 140 | 0 | 2175 | 489 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | | | 7.5 | 7.5 | | 2.0 | 7.5 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | | | 0.91 | 1.00 | | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (prot) | 3221 | 1678 | 1532 | 1770 | 3539 | | | 5085 | 1583 | | 5085 | 1583 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (perm) | 3221 | 1678 | 1532 | 1770 | 3539 | | | 5085 | 1583 | | 5085 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 510 | 205 | 4 | 229 | 287 | 0 | 0 | 2907 | 149 | 0 | 2314 | 520 |
| RTOR Reduction (vph) | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 459 | 256 | 1 | 229 | 287 | 0 | 0 | 2907 | 149 | 0 | 2314 | 520 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | | | | | | |
| Confl. Bikes (#/hr) | | | | 4 | | | | | | | | |
| Turn Type | Split | NA | Perm | Split | NA | Perm | | NA | Prot | | NA | custom |
| Protected Phases | 3 | 3 | | 4 | 4 | | | 6 | 6 | | 12 | 23 |
| Permitted Phases | | | 3 | | | 4 | | | | | | |
| Actuated Green, G (s) | 24.9 | 24.9 | 24.9 | 19.9 | 19.9 | | | 121.5 | 121.5 | | 121.5 | 128.9 |
| Effective Green, g (s) | 24.9 | 24.9 | 24.9 | 19.9 | 19.9 | | | 121.5 | 121.5 | | 121.5 | 128.9 |
| Actuated g/C Ratio | 0.13 | 0.13 | 0.13 | 0.10 | 0.10 | | | 0.64 | 0.64 | | 0.64 | 0.68 |
| Clearance Time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | | | 7.5 | 7.5 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | | | 1.0 | 1.0 | | | |
| Lane Grp Cap (vph) | 422 | 219 | 200 | 185 | 370 | | | 3251 | 1012 | | 3251 | 1073 |
| v/s Ratio Prot | 0.14 | c0.15 | | c0.13 | 0.08 | | | c0.57 | 0.09 | | 0.46 | 0.33 |
| v/s Ratio Perm | | | 0.00 | | | | | | | | | |
| v/c Ratio | 1.09 | 1.17 | 0.00 | 1.24 | 0.78 | | | 0.89 | 0.15 | | 0.71 | 0.48 |
| Uniform Delay, d1 | 82.5 | 82.5 | 71.8 | 85.0 | 82.9 | | | 28.8 | 13.6 | | 22.7 | 14.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 69.5 | 114.0 | 0.0 | 144.5 | 9.4 | | | 4.3 | 0.3 | | 1.4 | 0.3 |
| Delay (s) | 152.0 | 196.5 | 71.8 | 229.6 | 92.3 | | | 33.1 | 13.9 | | 24.0 | 15.0 |
| Level of Service | F | F | E | F | F | | | C | B | | C | B |
| Approach Delay (s) | | 167.4 | | | 153.2 | | | 32.2 | | | 22.4 | |
| Approach LOS | | F | | | F | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 50.7 | | | | HCM 2000 Level of Service | | D | | | |
| HCM 2000 Volume to Capacity ratio | | | 0.99 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 190.0 | | | | Sum of lost time (s) | | | | | |
| Intersection Capacity Utilization | | | 96.7% | | | | ICU Level of Service | | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Timings

4: SW 27th Ave & US 1/S Dixie Hwy

2016 Existing Conditions

A.M. Peak Hour

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↓ | ↑ | ↑↑↓ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 168 | 2888 | 43 | 2669 | 31 | 330 | 207 | 79 | 479 | 358 |
| Future Volume (vph) | 168 | 2888 | 43 | 2669 | 31 | 330 | 207 | 79 | 479 | 358 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Perm | Perm | NA | pm+ov |
| Protected Phases | 1 | 6 | | 2 | | 4 | | 4 | 8 | 1 |
| Permitted Phases | 6 | | 2 | | 4 | | 4 | 8 | | 8 |
| Detector Phase | 1 | 6 | 2 | 2 | 4 | 4 | 4 | 8 | 8 | 1 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 |
| Minimum Split (s) | 9.5 | 39.9 | 39.9 | 39.9 | 29.6 | 29.6 | 29.6 | 29.6 | 29.6 | 9.5 |
| Total Split (s) | 31.0 | 158.0 | 127.0 | 127.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 | 31.0 |
| Total Split (%) | 16.3% | 83.2% | 66.8% | 66.8% | 16.8% | 16.8% | 16.8% | 16.8% | 16.8% | 16.3% |
| Yellow Time (s) | 3.5 | 4.8 | 4.8 | 4.8 | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 3.5 |
| All-Red Time (s) | 1.0 | 2.1 | 2.0 | 2.0 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 6.9 | 6.8 | 6.8 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 | 4.5 |
| Lead/Lag | Lead | | Lag | Lag | | | | | | Lead |
| Lead-Lag Optimize? | Yes | | Yes | Yes | | | | | | Yes |
| Recall Mode | None | C-Min | C-Min | C-Min | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 190

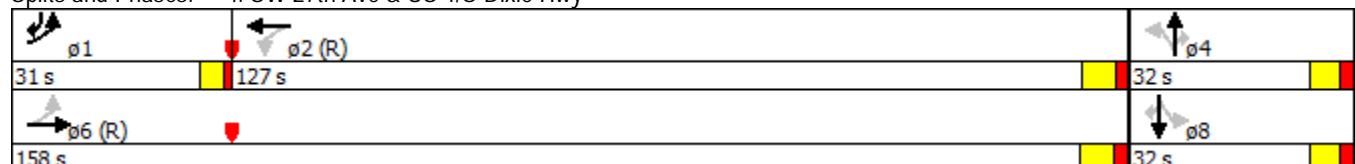
Actuated Cycle Length: 190

Offset: 39 (21%), Referenced to phase 2:WBTL and 6:EBTL, Start of Green

Natural Cycle: 110

Control Type: Actuated-Coordinated

Splits and Phases: 4: SW 27th Ave & US 1/S Dixie Hwy



HCM 2010 Signalized Intersection Summary
4: SW 27th Ave & US 1/S Dixie Hwy

2016 Existing Conditions
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--|------|---------|------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 168 | 2888 | 18 | 43 | 2669 | 60 | 31 | 330 | 207 | 79 | 479 | 358 |
| Future Volume (veh/h) | 168 | 2888 | 18 | 43 | 2669 | 60 | 31 | 330 | 207 | 79 | 479 | 358 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pb} T) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.85 | 0.97 | | 0.85 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 173 | 2977 | 19 | 44 | 2752 | 0 | 32 | 340 | 213 | 81 | 494 | 369 |
| Adj No. of Lanes | 1 | 3 | 0 | 1 | 3 | 0 | 1 | 2 | 1 | 1 | 2 | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 193 | 4146 | 26 | 79 | 3583 | 0 | 38 | 473 | 179 | 72 | 473 | 285 |
| Arrive On Green | 0.07 | 0.80 | 0.80 | 0.70 | 0.70 | 0.00 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| Sat Flow, veh/h | 1774 | 5214 | 33 | 79 | 5253 | 0 | 638 | 3539 | 1342 | 827 | 3539 | 1340 |
| Grp Volume(v), veh/h | 173 | 1934 | 1062 | 44 | 2752 | 0 | 32 | 340 | 213 | 81 | 494 | 369 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1857 | 79 | 1695 | 0 | 638 | 1770 | 1342 | 827 | 1770 | 1340 |
| Q Serve(g_s), s | 10.4 | 51.6 | 52.0 | 99.1 | 66.2 | 0.0 | 0.0 | 17.5 | 25.4 | 7.9 | 25.4 | 25.4 |
| Cycle Q Clear(g_c), s | 10.4 | 51.6 | 52.0 | 133.9 | 66.2 | 0.0 | 25.4 | 17.5 | 25.4 | 25.4 | 25.4 | 25.4 |
| Prop In Lane | 1.00 | | 0.02 | 1.00 | | 0.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 193 | 2696 | 1477 | 79 | 3583 | 0 | 38 | 473 | 179 | 72 | 473 | 285 |
| V/C Ratio(X) | 0.90 | 0.72 | 0.72 | 0.56 | 0.77 | 0.00 | 0.84 | 0.72 | 1.19 | 1.12 | 1.04 | 1.29 |
| Avail Cap(c_a), veh/h | 321 | 2696 | 1477 | 79 | 3583 | 0 | 38 | 473 | 179 | 72 | 473 | 285 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 60.5 | 9.3 | 9.3 | 48.4 | 18.1 | 0.0 | 95.0 | 78.9 | 82.3 | 93.1 | 82.3 | 76.7 |
| Incr Delay (d2), s/veh | 16.4 | 1.7 | 3.1 | 25.2 | 1.6 | 0.0 | 88.0 | 5.4 | 126.4 | 142.3 | 53.3 | 155.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 9.9 | 24.5 | 27.5 | 2.9 | 31.4 | 0.0 | 2.6 | 8.9 | 15.7 | 6.7 | 15.9 | 27.3 |
| LnGrp Delay(d),s/veh | 77.0 | 10.9 | 12.4 | 73.6 | 19.7 | 0.0 | 183.0 | 84.3 | 208.7 | 235.6 | 135.6 | 232.1 |
| LnGrp LOS | E | B | B | E | B | | F | F | F | F | F | F |
| Approach Vol, veh/h | | 3169 | | | 2796 | | | 585 | | | 944 | |
| Approach Delay, s/veh | | 15.0 | | | 20.6 | | | 135.0 | | | 181.9 | |
| Approach LOS | | B | | | C | | | F | | | F | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 17.2 | 140.8 | | 32.0 | | 158.0 | | 32.0 | | | | |
| Change Period (Y+R _c), s | 4.5 | * 6.9 | | * 6.6 | | 6.9 | | * 6.6 | | | | |
| Max Green Setting (Gmax), s | 26.5 | * 1.2E2 | | * 25 | | 151.1 | | * 25 | | | | |
| Max Q Clear Time (g _c +l1), s | 12.4 | 135.9 | | 27.4 | | 54.0 | | 27.4 | | | | |
| Green Ext Time (p _c), s | 0.4 | 0.0 | | 0.0 | | 81.0 | | 0.0 | | | | |

Intersection Summary

| | |
|---------------------|------|
| HCM 2010 Ctrl Delay | 47.5 |
| HCM 2010 LOS | D |

Notes

Timings
5: SE 26th Rd & US 1/Brickell Ave

2016 Existing Conditions

A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBT | WBR | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 234 | 1246 | 18 | 208 | 269 | 922 | 547 | 135 | 560 | 102 |
| Future Volume (vph) | 234 | 1246 | 18 | 208 | 269 | 922 | 547 | 135 | 560 | 102 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Free | Prot | NA | Perm |
| Protected Phases | 7 | 4 | | 8 | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | Free | | | 6 |
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 11.0 | 27.8 | 27.8 | 27.8 | 27.8 | 33.6 | | 11.0 | 33.6 | 33.6 |
| Total Split (s) | 23.0 | 53.0 | 53.0 | 30.0 | 30.0 | 52.0 | | 15.0 | 67.0 | 67.0 |
| Total Split (%) | 19.2% | 44.2% | 44.2% | 25.0% | 25.0% | 43.3% | | 12.5% | 55.8% | 55.8% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.8 | 2.8 | 2.8 | 2.8 | 2.6 | | 2.0 | 2.6 | 2.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.8 | 6.8 | 6.8 | 6.8 | 6.6 | | 6.0 | 6.6 | 6.6 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | | Yes | | |
| Recall Mode | None | Max | Max | None | None | C-Min | | None | C-Min | C-Min |

Intersection Summary

Cycle Length: 120

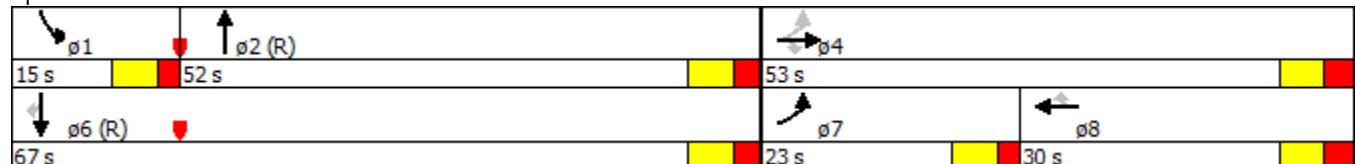
Actuated Cycle Length: 120

Offset: 74 (62%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Natural Cycle: 85

Control Type: Actuated-Coordinated

Splits and Phases: 5: SE 26th Rd & US 1/Brickell Ave



HCM 2010 Signalized Intersection Summary
5: SE 26th Rd & US 1/Brickell Ave

2016 Existing Conditions
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|-------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | | ↑↑ | ↑ | | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 234 | 1246 | 18 | 0 | 208 | 269 | 0 | 922 | 547 | 135 | 560 | 102 |
| Future Volume (veh/h) | 234 | 1246 | 18 | 0 | 208 | 269 | 0 | 922 | 547 | 135 | 560 | 102 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 0 | 1863 | 1863 | 0 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 289 | 1538 | 0 | 0 | 257 | 0 | 0 | 1138 | 0 | 167 | 691 | 0 |
| Adj No. of Lanes | 1 | 3 | 1 | 0 | 2 | 1 | 0 | 2 | 1 | 2 | 2 | 1 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 457 | 1958 | 610 | 0 | 684 | 306 | 0 | 1376 | 616 | 222 | 1781 | 797 |
| Arrive On Green | 0.14 | 0.38 | 0.00 | 0.00 | 0.19 | 0.00 | 0.00 | 0.39 | 0.00 | 0.06 | 0.50 | 0.00 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 0 | 3632 | 1583 | 0 | 3632 | 1583 | 3442 | 3539 | 1583 |
| Grp Volume(v), veh/h | 289 | 1538 | 0 | 0 | 257 | 0 | 0 | 1138 | 0 | 167 | 691 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 0 | 1770 | 1583 | 0 | 1770 | 1583 | 1721 | 1770 | 1583 |
| Q Serve(g_s), s | 15.1 | 32.0 | 0.0 | 0.0 | 7.6 | 0.0 | 0.0 | 34.8 | 0.0 | 5.7 | 14.5 | 0.0 |
| Cycle Q Clear(g_c), s | 15.1 | 32.0 | 0.0 | 0.0 | 7.6 | 0.0 | 0.0 | 34.8 | 0.0 | 5.7 | 14.5 | 0.0 |
| Prop In Lane | 1.00 | | | 1.00 | 0.00 | | 1.00 | 0.00 | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 457 | 1958 | 610 | 0 | 684 | 306 | 0 | 1376 | 616 | 222 | 1781 | 797 |
| V/C Ratio(X) | 0.63 | 0.79 | 0.00 | 0.00 | 0.38 | 0.00 | 0.00 | 0.83 | 0.00 | 0.75 | 0.39 | 0.00 |
| Avail Cap(c_a), veh/h | 457 | 1958 | 610 | 0 | 684 | 306 | 0 | 1376 | 616 | 258 | 1781 | 797 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 30.6 | 32.5 | 0.0 | 0.0 | 42.1 | 0.0 | 0.0 | 33.0 | 0.0 | 55.2 | 18.4 | 0.0 |
| Incr Delay (d2), s/veh | 2.2 | 3.3 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 5.8 | 0.0 | 8.1 | 0.6 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 7.6 | 15.5 | 0.0 | 0.0 | 3.7 | 0.0 | 0.0 | 18.0 | 0.0 | 3.0 | 7.2 | 0.0 |
| LnGrp Delay(d),s/veh | 32.8 | 35.8 | 0.0 | 0.0 | 42.4 | 0.0 | 0.0 | 38.8 | 0.0 | 63.3 | 19.0 | 0.0 |
| LnGrp LOS | C | D | | | D | | | D | | E | B | |
| Approach Vol, veh/h | | 1827 | | | 257 | | | 1138 | | | 858 | |
| Approach Delay, s/veh | | 35.3 | | | 42.4 | | | 38.8 | | | 27.6 | |
| Approach LOS | | D | | | D | | | D | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 13.7 | 53.3 | | 53.0 | | 67.0 | 23.0 | 30.0 | | | | |
| Change Period (Y+R _c), s | 6.0 | 6.6 | | * 6.8 | | 6.6 | 6.0 | * 6.8 | | | | |
| Max Green Setting (Gmax), s | 9.0 | 45.4 | | * 46 | | 60.4 | 17.0 | * 23 | | | | |
| Max Q Clear Time (g_c+l1), s | 7.7 | 36.8 | | 34.0 | | 16.5 | 17.1 | 9.6 | | | | |
| Green Ext Time (p_c), s | 0.0 | 4.0 | | 8.2 | | 6.5 | 0.0 | 8.8 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 35.1 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings

1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2019 Future Background

A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | SWL | SWT | SWR |
|----------------------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 483 | 403 | 38 | 87 | 290 | 48 | 1307 | 99 | 1102 | 407 |
| Future Volume (vph) | 483 | 403 | 38 | 87 | 290 | 48 | 1307 | 99 | 1102 | 407 |
| Turn Type | Split | NA | Free | Split | NA | Perm | NA | pm+pt | NA | pm+ov |
| Protected Phases | 8 | 8 | | 7 | 7 | | 6 | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | | 7 | | 2 | |
| Detector Phase | 8 | 8 | | 7 | 7 | 7 | 6 | 5 | 2 | 8 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 39.0 | 39.0 | | 15.9 | 15.9 | 15.9 | 40.7 | 11.8 | 40.7 | 39.0 |
| Total Split (s) | 39.0 | 39.0 | | 39.0 | 39.0 | 39.0 | 98.0 | 14.0 | 112.0 | 39.0 |
| Total Split (%) | 20.5% | 20.5% | | 20.5% | 20.5% | 20.5% | 51.6% | 7.4% | 58.9% | 20.5% |
| Yellow Time (s) | 4.8 | 4.8 | | 4.0 | 4.0 | 4.0 | 4.8 | 4.8 | 4.8 | 4.8 |
| All-Red Time (s) | 2.9 | 2.9 | | 4.1 | 4.1 | 4.1 | 2.9 | 2.0 | 2.9 | 2.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | 7.7 | 6.8 | 7.7 | 7.7 |
| Lead/Lag | Lag | Lag | | Lead | Lead | Lead | Lag | Lead | | Lag |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | | Yes |
| Recall Mode | None | None | | None | None | None | C-Min | None | C-Min | None |

Intersection Summary

Cycle Length: 190

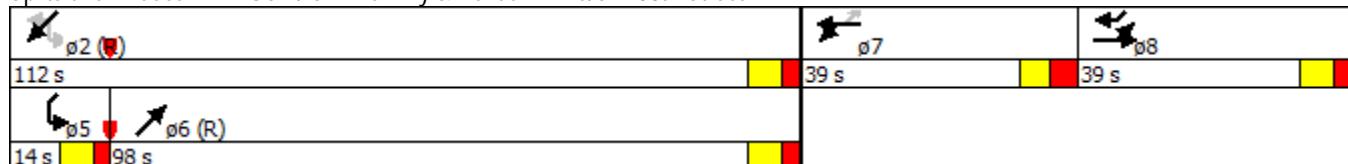
Actuated Cycle Length: 190

Offset: 61 (32%), Referenced to phase 2:SWTL and 6:NET, Start of Green

Natural Cycle: 110

Control Type: Actuated-Coordinated

Splits and Phases: 1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street



HCM Signalized Intersection Capacity Analysis
1: US 1 / S Dixie Hwy & Kendall Drive/SW 88th Street

2019 Future Background
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|------------------------|-------|------|-------|-------|-------|------|------|------|-------|------|-------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 483 | 403 | 38 | 87 | 290 | 48 | 0 | 1307 | 86 | 99 | 1102 | 407 |
| Future Volume (vph) | 483 | 403 | 38 | 87 | 290 | 48 | 0 | 1307 | 86 | 99 | 1102 | 407 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.7 | 7.7 | 4.0 | 8.1 | 8.1 | 8.1 | | 7.7 | | 6.8 | 7.7 | 7.7 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | | 1.00 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1610 | 3336 | 1564 | 1770 | 3539 | 1557 | | 5034 | | 1770 | 5085 | 1572 |
| Flt Permitted | 0.95 | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.06 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1610 | 3336 | 1564 | 1770 | 3539 | 1557 | | 5034 | | 112 | 5085 | 1572 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 508 | 424 | 40 | 92 | 305 | 51 | 0 | 1376 | 91 | 104 | 1160 | 428 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 4 | 0 | 0 | 0 | 21 |
| Lane Group Flow (vph) | 305 | 627 | 40 | 92 | 305 | 6 | 0 | 1463 | 0 | 104 | 1160 | 407 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | | | 1 | 1 | | 1 |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Turn Type | Split | NA | Free | Split | NA | Perm | | NA | pm+pt | NA | pm+ov | |
| Protected Phases | 8 | 8 | | 7 | 7 | | | 6 | | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | 7 | | | | 2 | | 2 |
| Actuated Green, G (s) | 57.3 | 57.3 | 190.0 | 23.3 | 23.3 | 23.3 | | 70.7 | 85.9 | 85.9 | 143.2 | |
| Effective Green, g (s) | 57.3 | 57.3 | 190.0 | 23.3 | 23.3 | 23.3 | | 70.7 | 85.9 | 85.9 | 143.2 | |
| Actuated g/C Ratio | 0.30 | 0.30 | 1.00 | 0.12 | 0.12 | 0.12 | | 0.37 | 0.45 | 0.45 | 0.75 | |
| Clearance Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | | 7.7 | 6.8 | 7.7 | 7.7 | |
| Vehicle Extension (s) | 3.5 | 3.5 | | 4.0 | 4.0 | 4.0 | | 1.0 | 2.0 | 1.0 | 3.5 | |
| Lane Grp Cap (vph) | 485 | 1006 | 1564 | 217 | 433 | 190 | | 1873 | | 123 | 2298 | 1248 |
| v/s Ratio Prot | c0.19 | 0.19 | | 0.05 | c0.09 | | | 0.29 | c0.04 | 0.23 | 0.10 | |
| v/s Ratio Perm | | | 0.03 | | | 0.00 | | | c0.34 | | 0.16 | |
| v/c Ratio | 0.63 | 0.62 | 0.03 | 0.42 | 0.70 | 0.03 | | 0.78 | 0.85 | 0.50 | 0.33 | |
| Uniform Delay, d1 | 57.2 | 57.1 | 0.0 | 77.1 | 80.0 | 73.4 | | 52.8 | 40.1 | 37.0 | 7.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.7 | 1.3 | 0.0 | 1.8 | 5.5 | 0.1 | | 3.3 | 37.2 | 0.8 | 0.2 | |
| Delay (s) | 59.9 | 58.3 | 0.0 | 79.0 | 85.6 | 73.5 | | 56.1 | 77.3 | 37.7 | 7.8 | |
| Level of Service | E | E | A | E | F | E | | E | | E | D | A |
| Approach Delay (s) | | 56.4 | | | 82.8 | | | 56.1 | | | 32.6 | |
| Approach LOS | | E | | | F | | | E | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 50.1 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.76 | | |
| Actuated Cycle Length (s) | 190.0 | Sum of lost time (s) | 30.3 |
| Intersection Capacity Utilization | 83.3% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

Timings

2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2019 Future Background

A.M. Peak Hour

| Lane Group | EBT | EBR | WBT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↑ | ↑↓ | ↑ | ↑↑↓ | ↑ | ↑↑↓ |
| Traffic Volume (vph) | 580 | 24 | 269 | 98 | 3486 | 59 | 1835 |
| Future Volume (vph) | 580 | 24 | 269 | 98 | 3486 | 59 | 1835 |
| Turn Type | NA | Perm | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 8 | | 4 | 1 | 6 | 5 | 2 |
| Permitted Phases | | | | 6 | | 2 | |
| Detector Phase | 8 | 8 | 4 | 1 | 6 | 5 | 2 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 12.0 | 12.0 | 12.0 | 5.0 | 7.0 | 5.0 | 7.0 |
| Minimum Split (s) | 34.9 | 34.9 | 34.9 | 11.4 | 37.0 | 11.4 | 37.0 |
| Total Split (s) | 44.0 | 44.0 | 44.0 | 18.0 | 135.0 | 11.0 | 128.0 |
| Total Split (%) | 23.2% | 23.2% | 23.2% | 9.5% | 71.1% | 5.8% | 67.4% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.4 | 4.0 | 4.4 |
| All-Red Time (s) | 4.9 | 4.9 | 4.9 | 2.0 | 3.6 | 2.0 | 3.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.9 | 8.9 | 8.9 | 6.0 | 8.0 | 6.0 | 8.0 |
| Lead/Lag | | | | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | C-Min | None | C-Min |

Intersection Summary

Cycle Length: 190

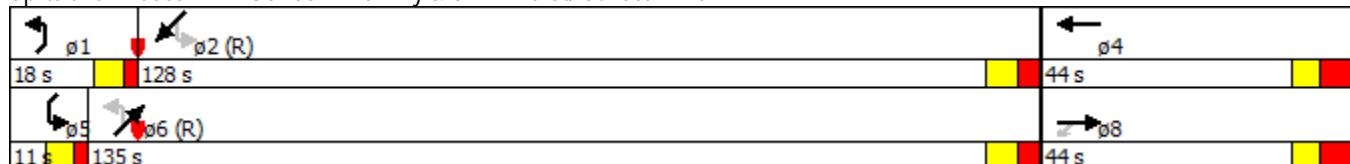
Actuated Cycle Length: 190

Offset: 160 (84%), Referenced to phase 2:SWTL and 6:NETL, Start of Green

Natural Cycle: 145

Control Type: Actuated-Coordinated

Splits and Phases: 2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive



HCM 2010 Signalized Intersection Summary
2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2019 Future Background
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|---------------------------------------|------|-------|------|-------|------|-------|------|-------|-------|------|------|------|
| Lane Configurations | | ↑↑ | ↑ | | ↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | |
| Traffic Volume (veh/h) | 0 | 580 | 24 | 0 | 269 | 3 | 98 | 3486 | 90 | 59 | 1835 | 215 |
| Future Volume (veh/h) | 0 | 580 | 24 | 0 | 269 | 3 | 98 | 3486 | 90 | 59 | 1835 | 215 |
| Number | 3 | 8 | 18 | 7 | 4 | 14 | 1 | 6 | 16 | 5 | 2 | 12 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.98 | 1.00 | | 0.96 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1863 | 1863 | 0 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 0 | 604 | 0 | 0 | 280 | 3 | 102 | 3631 | 94 | 61 | 1911 | 224 |
| Adj No. of Lanes | 0 | 2 | 1 | 0 | 2 | 0 | 1 | 3 | 0 | 1 | 3 | 0 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, % | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 0 | 645 | 288 | 0 | 654 | 7 | 170 | 3424 | 88 | 83 | 3074 | 357 |
| Arrive On Green | 0.00 | 0.18 | 0.00 | 0.00 | 0.18 | 0.18 | 0.03 | 0.67 | 0.67 | 0.03 | 0.67 | 0.67 |
| Sat Flow, veh/h | 0 | 3632 | 1583 | 0 | 3680 | 38 | 1774 | 5095 | 131 | 1774 | 4601 | 534 |
| Grp Volume(v), veh/h | 0 | 604 | 0 | 0 | 138 | 145 | 102 | 2404 | 1321 | 61 | 1403 | 732 |
| Grp Sat Flow(s),veh/h/ln | 0 | 1770 | 1583 | 0 | 1770 | 1856 | 1774 | 1695 | 1836 | 1774 | 1695 | 1744 |
| Q Serve(g_s), s | 0.0 | 32.0 | 0.0 | 0.0 | 13.1 | 13.2 | 3.5 | 127.7 | 127.7 | 2.4 | 44.5 | 45.6 |
| Cycle Q Clear(g_c), s | 0.0 | 32.0 | 0.0 | 0.0 | 13.1 | 13.2 | 3.5 | 127.7 | 127.7 | 2.4 | 44.5 | 45.6 |
| Prop In Lane | 0.00 | | 1.00 | 0.00 | | 0.02 | 1.00 | | 0.07 | 1.00 | | 0.31 |
| Lane Grp Cap(c), veh/h | 0 | 645 | 288 | 0 | 322 | 338 | 170 | 2278 | 1234 | 83 | 2265 | 1165 |
| V/C Ratio(X) | 0.00 | 0.94 | 0.00 | 0.00 | 0.43 | 0.43 | 0.60 | 1.06 | 1.07 | 0.74 | 0.62 | 0.63 |
| Avail Cap(c_a), veh/h | 0 | 654 | 292 | 0 | 327 | 343 | 230 | 2278 | 1234 | 85 | 2265 | 1165 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 76.6 | 0.0 | 0.0 | 68.9 | 68.9 | 21.2 | 31.2 | 31.2 | 54.5 | 17.9 | 18.0 |
| Incr Delay (d2), s/veh | 0.0 | 21.0 | 0.0 | 0.0 | 0.9 | 0.9 | 1.3 | 35.4 | 46.8 | 24.6 | 1.3 | 2.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.0 | 17.6 | 0.0 | 0.0 | 6.5 | 6.8 | 2.8 | 70.7 | 80.5 | 3.7 | 21.1 | 22.6 |
| LnGrp Delay(d),s/veh | 0.0 | 97.6 | 0.0 | 0.0 | 69.8 | 69.8 | 22.5 | 66.6 | 78.0 | 79.1 | 19.1 | 20.6 |
| LnGrp LOS | F | | | | E | E | C | F | F | E | B | C |
| Approach Vol, veh/h | | 604 | | | 283 | | | 3827 | | | 2196 | |
| Approach Delay, s/veh | | 97.6 | | | 69.8 | | | 69.3 | | | 21.3 | |
| Approach LOS | | F | | | E | | | E | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 11.5 | 134.9 | | 43.5 | 10.8 | 135.7 | | 43.5 | | | | |
| Change Period (Y+R _c), s | 6.0 | 8.0 | | * 8.9 | 6.0 | 8.0 | | * 8.9 | | | | |
| Max Green Setting (Gmax), s | 12.0 | 120.0 | | * 35 | 5.0 | 127.0 | | * 35 | | | | |
| Max Q Clear Time (g_c+l1), s | 5.5 | 47.6 | | 15.2 | 4.4 | 129.7 | | 34.0 | | | | |
| Green Ext Time (p_c), s | 0.1 | 60.6 | | 5.8 | 0.0 | 0.0 | | 0.6 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 56.6 | | | | | | | | |
| HCM 2010 LOS | | | | E | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings

3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2019 Future Background

A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | NET | NER | SWT | SWR | ø1 | ø2 |
|----------------------|-------|-------|-------|-------|-------|-------|-------|------|--------|------|-------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ | | |
| Traffic Volume (vph) | 486 | 196 | 4 | 218 | 274 | 2774 | 142 | 2208 | 496 | | |
| Future Volume (vph) | 486 | 196 | 4 | 218 | 274 | 2774 | 142 | 2208 | 496 | | |
| Turn Type | Split | NA | Perm | Split | NA | NA | Prot | NA | custom | | |
| Protected Phases | 3 | 3 | | 4 | 4 | 6 | 6 | 12 | 23 | 1 | 2 |
| Permitted Phases | | | | 3 | | | | | | | |
| Detector Phase | 3 | 3 | 3 | 4 | 4 | 6 | 6 | 12 | 23 | | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 15.0 | 15.0 | | | 1.0 | 15.0 |
| Minimum Split (s) | 26.1 | 26.1 | 26.1 | 26.1 | 26.1 | 25.5 | 25.5 | | | 25.0 | 32.5 |
| Total Split (s) | 33.0 | 33.0 | 33.0 | 28.0 | 28.0 | 129.0 | 129.0 | | | 25.0 | 104.0 |
| Total Split (%) | 17.4% | 17.4% | 17.4% | 14.7% | 14.7% | 67.9% | 67.9% | | | 13% | 55% |
| Yellow Time (s) | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.8 | 4.8 | | | 2.0 | 4.8 |
| All-Red Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 2.7 | 2.7 | | | 0.0 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | 7.5 | 7.5 | | | | |
| Lead/Lag | Lead | Lead | Lead | Lag | Lag | | | | | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | | | | Yes | Yes |
| Recall Mode | None | None | None | None | None | C-Min | C-Min | | | Max | C-Min |

Intersection Summary

Cycle Length: 190

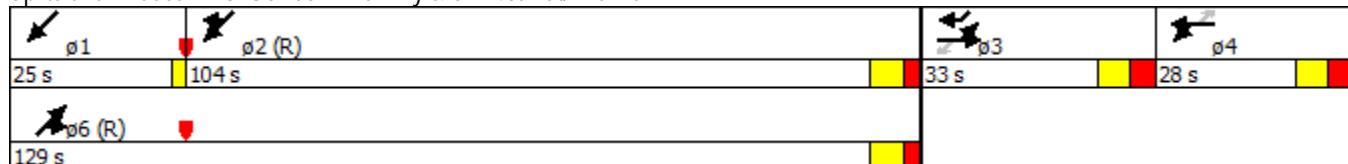
Actuated Cycle Length: 190

Offset: 99 (52%), Referenced to phase 2:SWT and 6:NET, Start of Green

Natural Cycle: 150

Control Type: Actuated-Coordinated

Splits and Phases: 3: US 1/S Dixie Hwy & SW 40th St/Bird Rd



HCM Signalized Intersection Capacity Analysis
3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2019 Future Background
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|-----------------------------------|-------|-------|-------|-------|-------|------|---------------------------|-------|-------|------|-------|--------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | ↑ | | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 486 | 196 | 4 | 218 | 274 | 0 | 0 | 2774 | 142 | 0 | 2208 | 496 |
| Future Volume (vph) | 486 | 196 | 4 | 218 | 274 | 0 | 0 | 2774 | 142 | 0 | 2208 | 496 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | | | 7.5 | 7.5 | | 2.0 | 7.5 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | | | 0.91 | 1.00 | | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (prot) | 3221 | 1678 | 1532 | 1770 | 3539 | | | 5085 | 1583 | | 5085 | 1583 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (perm) | 3221 | 1678 | 1532 | 1770 | 3539 | | | 5085 | 1583 | | 5085 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 517 | 209 | 4 | 232 | 291 | 0 | 0 | 2951 | 151 | 0 | 2349 | 528 |
| RTOR Reduction (vph) | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 465 | 261 | 1 | 232 | 291 | 0 | 0 | 2951 | 151 | 0 | 2349 | 528 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | | | | | | |
| Confl. Bikes (#/hr) | | | | 4 | | | | | | | | |
| Turn Type | Split | NA | Perm | Split | NA | Perm | | NA | Prot | | NA | custom |
| Protected Phases | 3 | 3 | | 4 | 4 | | | 6 | 6 | | 12 | 23 |
| Permitted Phases | | | 3 | | | 4 | | | | | | |
| Actuated Green, G (s) | 24.9 | 24.9 | 24.9 | 19.9 | 19.9 | | | 121.5 | 121.5 | | 121.5 | 128.9 |
| Effective Green, g (s) | 24.9 | 24.9 | 24.9 | 19.9 | 19.9 | | | 121.5 | 121.5 | | 121.5 | 128.9 |
| Actuated g/C Ratio | 0.13 | 0.13 | 0.13 | 0.10 | 0.10 | | | 0.64 | 0.64 | | 0.64 | 0.68 |
| Clearance Time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | | | 7.5 | 7.5 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | | | 1.0 | 1.0 | | | |
| Lane Grp Cap (vph) | 422 | 219 | 200 | 185 | 370 | | | 3251 | 1012 | | 3251 | 1073 |
| v/s Ratio Prot | 0.14 | c0.16 | | c0.13 | 0.08 | | | c0.58 | 0.10 | | 0.46 | 0.33 |
| v/s Ratio Perm | | | 0.00 | | | | | | | | | |
| v/c Ratio | 1.10 | 1.19 | 0.00 | 1.25 | 0.79 | | | 0.91 | 0.15 | | 0.72 | 0.49 |
| Uniform Delay, d1 | 82.5 | 82.5 | 71.8 | 85.0 | 83.0 | | | 29.4 | 13.7 | | 23.0 | 14.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 74.3 | 122.3 | 0.0 | 150.7 | 10.2 | | | 4.9 | 0.3 | | 1.4 | 0.4 |
| Delay (s) | 156.9 | 204.9 | 71.8 | 235.8 | 93.2 | | | 34.3 | 14.0 | | 24.4 | 15.1 |
| Level of Service | F | F | E | F | F | | | C | B | | C | B |
| Approach Delay (s) | | 173.6 | | | 156.4 | | | 33.3 | | | 22.7 | |
| Approach LOS | | F | | | F | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 52.1 | | | | HCM 2000 Level of Service | | D | | | |
| HCM 2000 Volume to Capacity ratio | | | 1.00 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 190.0 | | | | Sum of lost time (s) | | | 25.7 | | |
| Intersection Capacity Utilization | | | 97.8% | | | | ICU Level of Service | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Timings

4: SW 27th Ave & US 1/S Dixie Hwy

2019 Future Background

A.M. Peak Hour

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↓ | ↑ | ↑↑↓ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 171 | 2932 | 44 | 2709 | 31 | 335 | 210 | 80 | 486 | 363 |
| Future Volume (vph) | 171 | 2932 | 44 | 2709 | 31 | 335 | 210 | 80 | 486 | 363 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Perm | Perm | NA | pm+ov |
| Protected Phases | 1 | 6 | | 2 | | 4 | | 4 | 8 | 1 |
| Permitted Phases | 6 | | 2 | | 4 | | 4 | 8 | | 8 |
| Detector Phase | 1 | 6 | 2 | 2 | 4 | 4 | 4 | 8 | 8 | 1 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 |
| Minimum Split (s) | 9.5 | 39.9 | 39.9 | 39.9 | 29.6 | 29.6 | 29.6 | 29.6 | 29.6 | 9.5 |
| Total Split (s) | 31.0 | 158.0 | 127.0 | 127.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 | 31.0 |
| Total Split (%) | 16.3% | 83.2% | 66.8% | 66.8% | 16.8% | 16.8% | 16.8% | 16.8% | 16.8% | 16.3% |
| Yellow Time (s) | 3.5 | 4.8 | 4.8 | 4.8 | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 3.5 |
| All-Red Time (s) | 1.0 | 2.1 | 2.1 | 2.1 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 6.9 | 6.9 | 6.9 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 | 4.5 |
| Lead/Lag | Lead | | Lag | Lag | | | | | | Lead |
| Lead-Lag Optimize? | Yes | | Yes | Yes | | | | | | Yes |
| Recall Mode | None | C-Min | C-Min | C-Min | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 190

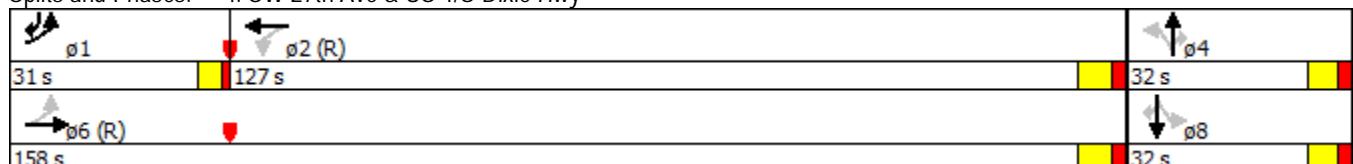
Actuated Cycle Length: 190

Offset: 39 (21%), Referenced to phase 2:WBTL and 6:EBTL, Start of Green

Natural Cycle: 120

Control Type: Actuated-Coordinated

Splits and Phases: 4: SW 27th Ave & US 1/S Dixie Hwy



HCM 2010 Signalized Intersection Summary
4: SW 27th Ave & US 1/S Dixie Hwy

2019 Future Background
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--|------|-------|------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 171 | 2932 | 18 | 44 | 2709 | 61 | 31 | 335 | 210 | 80 | 486 | 363 |
| Future Volume (veh/h) | 171 | 2932 | 18 | 44 | 2709 | 61 | 31 | 335 | 210 | 80 | 486 | 363 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pbT}) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.85 | 0.97 | | 0.85 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 176 | 3023 | 19 | 45 | 2793 | 0 | 32 | 345 | 216 | 82 | 501 | 374 |
| Adj No. of Lanes | 1 | 3 | 0 | 1 | 3 | 0 | 1 | 2 | 1 | 1 | 2 | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 196 | 4147 | 26 | 77 | 3565 | 0 | 38 | 473 | 179 | 71 | 473 | 291 |
| Arrive On Green | 0.07 | 0.80 | 0.80 | 0.70 | 0.70 | 0.00 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| Sat Flow, veh/h | 1774 | 5214 | 33 | 76 | 5253 | 0 | 631 | 3539 | 1342 | 822 | 3539 | 1340 |
| Grp Volume(v), veh/h | 176 | 1963 | 1079 | 45 | 2793 | 0 | 32 | 345 | 216 | 82 | 501 | 374 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1857 | 76 | 1695 | 0 | 631 | 1770 | 1342 | 822 | 1770 | 1340 |
| Q Serve(g_s), s | 11.0 | 53.5 | 53.9 | 97.2 | 69.2 | 0.0 | 0.0 | 17.8 | 25.4 | 7.6 | 25.4 | 25.4 |
| Cycle Q Clear(g_c), s | 11.0 | 53.5 | 53.9 | 133.2 | 69.2 | 0.0 | 25.4 | 17.8 | 25.4 | 25.4 | 25.4 | 25.4 |
| Prop In Lane | 1.00 | | 0.02 | 1.00 | | 0.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 196 | 2696 | 1477 | 77 | 3565 | 0 | 38 | 473 | 179 | 71 | 473 | 291 |
| V/C Ratio(X) | 0.90 | 0.73 | 0.73 | 0.59 | 0.78 | 0.00 | 0.84 | 0.73 | 1.20 | 1.16 | 1.06 | 1.29 |
| Avail Cap(c_a), veh/h | 318 | 2696 | 1477 | 77 | 3565 | 0 | 38 | 473 | 179 | 71 | 473 | 291 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 62.4 | 9.5 | 9.5 | 53.2 | 18.8 | 0.0 | 95.0 | 79.0 | 82.3 | 93.2 | 82.3 | 76.3 |
| Incr Delay (d2), s/veh | 17.5 | 1.8 | 3.2 | 28.9 | 1.8 | 0.0 | 88.0 | 5.9 | 132.6 | 155.7 | 57.8 | 151.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 10.1 | 25.5 | 28.6 | 3.0 | 32.9 | 0.0 | 2.6 | 9.1 | 16.0 | 6.8 | 16.2 | 27.6 |
| LnGrp Delay(d),s/veh | 79.9 | 11.2 | 12.7 | 82.1 | 20.6 | 0.0 | 183.0 | 84.9 | 214.9 | 249.0 | 140.1 | 228.2 |
| LnGrp LOS | E | B | B | F | C | | F | F | F | F | F | F |
| Approach Vol, veh/h | | 3218 | | | 2838 | | | 593 | | | 957 | |
| Approach Delay, s/veh | | 15.5 | | | 21.6 | | | 137.5 | | | 183.9 | |
| Approach LOS | | B | | | C | | | F | | | F | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 17.9 | 140.1 | | 32.0 | | 158.0 | | 32.0 | | | | |
| Change Period (Y+R _c), s | 4.5 | 6.9 | | * 6.6 | | 6.9 | | * 6.6 | | | | |
| Max Green Setting (Gmax), s | 26.5 | 120.1 | | * 25 | | 151.1 | | * 25 | | | | |
| Max Q Clear Time (g _{c+l1}), s | 13.0 | 135.2 | | 27.4 | | 55.9 | | 27.4 | | | | |
| Green Ext Time (p _c), s | 0.4 | 0.0 | | 0.0 | | 81.0 | | 0.0 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 48.5 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings
5: SE 26th Rd & US 1/Brickell Ave

2019 Future Background

A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBT | WBR | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 238 | 1265 | 18 | 211 | 273 | 928 | 555 | 137 | 568 | 104 |
| Future Volume (vph) | 238 | 1265 | 18 | 211 | 273 | 928 | 555 | 137 | 568 | 104 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Free | Prot | NA | Perm |
| Protected Phases | 7 | 4 | | 8 | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | Free | | | 6 |
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 11.0 | 27.8 | 27.8 | 27.8 | 27.8 | 33.6 | | 11.0 | 33.6 | 33.6 |
| Total Split (s) | 23.0 | 53.0 | 53.0 | 30.0 | 30.0 | 52.0 | | 15.0 | 67.0 | 67.0 |
| Total Split (%) | 19.2% | 44.2% | 44.2% | 25.0% | 25.0% | 43.3% | | 12.5% | 55.8% | 55.8% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.8 | 2.8 | 2.8 | 2.8 | 2.6 | | 2.0 | 2.6 | 2.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.8 | 6.8 | 6.8 | 6.8 | 6.6 | | 6.0 | 6.6 | 6.6 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | | Yes | | |
| Recall Mode | None | Max | Max | None | None | C-Min | | None | C-Min | C-Min |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 74 (62%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Natural Cycle: 85

Control Type: Actuated-Coordinated

Splits and Phases: 5: SE 26th Rd & US 1/Brickell Ave



HCM 2010 Signalized Intersection Summary
5: SE 26th Rd & US 1/Brickell Ave

2019 Future Background
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|-------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | | ↑↑ | ↑ | | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 238 | 1265 | 18 | 0 | 211 | 273 | 0 | 928 | 555 | 137 | 568 | 104 |
| Future Volume (veh/h) | 238 | 1265 | 18 | 0 | 211 | 273 | 0 | 928 | 555 | 137 | 568 | 104 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 0 | 1863 | 1863 | 0 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 294 | 1562 | 0 | 0 | 260 | 0 | 0 | 1146 | 0 | 169 | 701 | 0 |
| Adj No. of Lanes | 1 | 3 | 1 | 0 | 2 | 1 | 0 | 2 | 1 | 2 | 2 | 1 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 224 | 1781 | 797 |
| Arrive On Green | 0.14 | 0.38 | 0.00 | 0.00 | 0.19 | 0.00 | 0.00 | 0.39 | 0.00 | 0.07 | 0.50 | 0.00 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 0 | 3632 | 1583 | 0 | 3632 | 1583 | 3442 | 3539 | 1583 |
| Grp Volume(v), veh/h | 294 | 1562 | 0 | 0 | 260 | 0 | 0 | 1146 | 0 | 169 | 701 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 0 | 1770 | 1583 | 0 | 1770 | 1583 | 1721 | 1770 | 1583 |
| Q Serve(g_s), s | 15.5 | 32.7 | 0.0 | 0.0 | 7.7 | 0.0 | 0.0 | 35.1 | 0.0 | 5.8 | 14.7 | 0.0 |
| Cycle Q Clear(g_c), s | 15.5 | 32.7 | 0.0 | 0.0 | 7.7 | 0.0 | 0.0 | 35.1 | 0.0 | 5.8 | 14.7 | 0.0 |
| Prop In Lane | 1.00 | | | 1.00 | 0.00 | | 1.00 | 0.00 | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 224 | 1781 | 797 |
| V/C Ratio(X) | 0.65 | 0.80 | 0.00 | 0.00 | 0.38 | 0.00 | 0.00 | 0.83 | 0.00 | 0.76 | 0.39 | 0.00 |
| Avail Cap(c_a), veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 258 | 1781 | 797 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 30.8 | 32.8 | 0.0 | 0.0 | 42.1 | 0.0 | 0.0 | 33.2 | 0.0 | 55.2 | 18.5 | 0.0 |
| Incr Delay (d2), s/veh | 2.5 | 3.5 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 6.1 | 0.0 | 8.4 | 0.7 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 7.8 | 16.0 | 0.0 | 0.0 | 3.8 | 0.0 | 0.0 | 18.4 | 0.0 | 3.0 | 7.4 | 0.0 |
| LnGrp Delay(d),s/veh | 33.2 | 36.2 | 0.0 | 0.0 | 42.4 | 0.0 | 0.0 | 39.3 | 0.0 | 63.6 | 19.1 | 0.0 |
| LnGrp LOS | C | D | | | D | | | D | | E | B | |
| Approach Vol, veh/h | | 1856 | | | 260 | | | 1146 | | | 870 | |
| Approach Delay, s/veh | | 35.8 | | | 42.4 | | | 39.3 | | | 27.7 | |
| Approach LOS | | D | | | D | | | D | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 13.8 | 53.2 | | 53.0 | | 67.0 | 23.0 | 30.0 | | | | |
| Change Period (Y+R _c), s | 6.0 | 6.6 | | * 6.8 | | 6.6 | 6.0 | * 6.8 | | | | |
| Max Green Setting (Gmax), s | 9.0 | 45.4 | | * 46 | | 60.4 | 17.0 | * 23 | | | | |
| Max Q Clear Time (g_c+l1), s | 7.8 | 37.1 | | 34.7 | | 16.7 | 17.5 | 9.7 | | | | |
| Green Ext Time (p_c), s | 0.0 | 3.9 | | 7.9 | | 6.6 | 0.0 | 8.9 | | | | |

Intersection Summary

| | |
|---------------------|------|
| HCM 2010 Ctrl Delay | 35.5 |
| HCM 2010 LOS | D |

Notes

Timings
1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2019 Future Total
A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | SWL | SWT | SWR |
|----------------------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 483 | 403 | 38 | 87 | 290 | 48 | 1288 | 99 | 1086 | 407 |
| Future Volume (vph) | 483 | 403 | 38 | 87 | 290 | 48 | 1288 | 99 | 1086 | 407 |
| Turn Type | Split | NA | Free | Split | NA | Perm | NA | pm+pt | NA | pm+ov |
| Protected Phases | 8 | 8 | | 7 | 7 | | 6 | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | | 7 | | 2 | |
| Detector Phase | 8 | 8 | | 7 | 7 | 7 | 6 | 5 | 2 | 8 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 39.0 | 39.0 | | 15.9 | 15.9 | 15.9 | 40.7 | 11.8 | 40.7 | 39.0 |
| Total Split (s) | 39.0 | 39.0 | | 39.0 | 39.0 | 39.0 | 98.0 | 14.0 | 112.0 | 39.0 |
| Total Split (%) | 20.5% | 20.5% | | 20.5% | 20.5% | 20.5% | 51.6% | 7.4% | 58.9% | 20.5% |
| Yellow Time (s) | 4.8 | 4.8 | | 4.0 | 4.0 | 4.0 | 4.8 | 4.8 | 4.8 | 4.8 |
| All-Red Time (s) | 2.9 | 2.9 | | 4.1 | 4.1 | 4.1 | 2.9 | 2.0 | 2.9 | 2.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | 7.7 | 6.8 | 7.7 | 7.7 |
| Lead/Lag | Lag | Lag | | Lead | Lead | Lead | Lag | Lead | | Lag |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | | Yes |
| Recall Mode | None | None | | None | None | None | C-Min | None | C-Min | None |

Intersection Summary

Cycle Length: 190

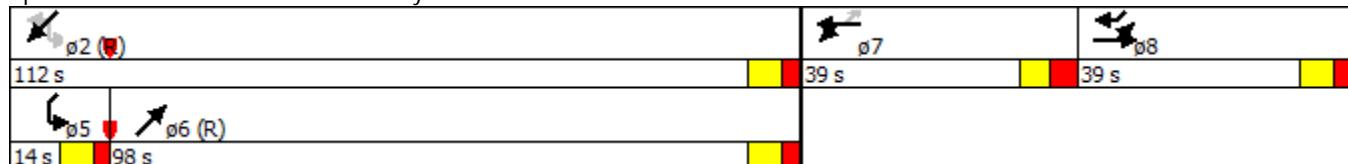
Actuated Cycle Length: 190

Offset: 61 (32%), Referenced to phase 2:SWTL and 6:NET, Start of Green

Natural Cycle: 110

Control Type: Actuated-Coordinated

Splits and Phases: 1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street



HCM Signalized Intersection Capacity Analysis
1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2019 Future Total
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|------------------------|-------|------|-------|-------|-------|------|------|------|-------|-------|-------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 483 | 403 | 38 | 87 | 290 | 48 | 0 | 1288 | 86 | 99 | 1086 | 407 |
| Future Volume (vph) | 483 | 403 | 38 | 87 | 290 | 48 | 0 | 1288 | 86 | 99 | 1086 | 407 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.7 | 7.7 | 4.0 | 8.1 | 8.1 | 8.1 | | 7.7 | | 6.8 | 7.7 | 7.7 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | | 1.00 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1610 | 3336 | 1564 | 1770 | 3539 | 1557 | | 5033 | | 1770 | 5085 | 1572 |
| Flt Permitted | 0.95 | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.06 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1610 | 3336 | 1564 | 1770 | 3539 | 1557 | | 5033 | | 116 | 5085 | 1572 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 508 | 424 | 40 | 92 | 305 | 51 | 0 | 1356 | 91 | 104 | 1143 | 428 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 4 | 0 | 0 | 0 | 21 |
| Lane Group Flow (vph) | 305 | 627 | 40 | 92 | 305 | 6 | 0 | 1443 | 0 | 104 | 1143 | 407 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | | | 1 | 1 | | 1 |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Turn Type | Split | NA | Free | Split | NA | Perm | | NA | pm+pt | NA | pm+ov | |
| Protected Phases | 8 | 8 | | 7 | 7 | | | 6 | | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | 7 | | | | 2 | | 2 |
| Actuated Green, G (s) | 57.8 | 57.8 | 190.0 | 23.3 | 23.3 | 23.3 | | 70.2 | 85.4 | 85.4 | 143.2 | |
| Effective Green, g (s) | 57.8 | 57.8 | 190.0 | 23.3 | 23.3 | 23.3 | | 70.2 | 85.4 | 85.4 | 143.2 | |
| Actuated g/C Ratio | 0.30 | 0.30 | 1.00 | 0.12 | 0.12 | 0.12 | | 0.37 | 0.45 | 0.45 | 0.75 | |
| Clearance Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | | 7.7 | 6.8 | 7.7 | 7.7 | |
| Vehicle Extension (s) | 3.5 | 3.5 | | 4.0 | 4.0 | 4.0 | | 1.0 | 2.0 | 1.0 | 3.5 | |
| Lane Grp Cap (vph) | 489 | 1014 | 1564 | 217 | 433 | 190 | | 1859 | | 125 | 2285 | 1248 |
| v/s Ratio Prot | c0.19 | 0.19 | | 0.05 | c0.09 | | | 0.29 | | c0.04 | 0.22 | 0.10 |
| v/s Ratio Perm | | | 0.03 | | | 0.00 | | | | c0.34 | | 0.16 |
| v/c Ratio | 0.62 | 0.62 | 0.03 | 0.42 | 0.70 | 0.03 | | 0.78 | 0.83 | 0.50 | 0.33 | |
| Uniform Delay, d1 | 56.8 | 56.6 | 0.0 | 77.1 | 80.0 | 73.4 | | 52.9 | 40.0 | 37.1 | 7.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.6 | 1.2 | 0.0 | 1.8 | 5.5 | 0.1 | | 3.2 | 34.1 | 0.8 | 0.2 | |
| Delay (s) | 59.4 | 57.8 | 0.0 | 79.0 | 85.6 | 73.5 | | 56.2 | 74.1 | 37.9 | 7.8 | |
| Level of Service | E | E | A | E | F | E | | E | | E | D | A |
| Approach Delay (s) | | 55.9 | | | 82.8 | | | 56.2 | | | 32.5 | |
| Approach LOS | | E | | | F | | | E | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 50.0 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.75 | | |
| Actuated Cycle Length (s) | 190.0 | Sum of lost time (s) | 30.3 |
| Intersection Capacity Utilization | 83.3% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

Timings
2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2019 Future Total
A.M. Peak Hour

| Lane Group | EBT | EBR | WBT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ |
| Traffic Volume (vph) | 580 | 24 | 268 | 98 | 3446 | 59 | 1814 |
| Future Volume (vph) | 580 | 24 | 268 | 98 | 3446 | 59 | 1814 |
| Turn Type | NA | Perm | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 8 | | 4 | 1 | 6 | 5 | 2 |
| Permitted Phases | | | | 6 | | 2 | |
| Detector Phase | 8 | 8 | 4 | 1 | 6 | 5 | 2 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 12.0 | 12.0 | 12.0 | 5.0 | 7.0 | 5.0 | 7.0 |
| Minimum Split (s) | 34.9 | 34.9 | 34.9 | 11.4 | 37.0 | 11.4 | 37.0 |
| Total Split (s) | 44.0 | 44.0 | 44.0 | 18.0 | 135.0 | 11.0 | 128.0 |
| Total Split (%) | 23.2% | 23.2% | 23.2% | 9.5% | 71.1% | 5.8% | 67.4% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.4 | 4.0 | 4.4 |
| All-Red Time (s) | 4.9 | 4.9 | 4.9 | 2.0 | 3.6 | 2.0 | 3.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.9 | 8.9 | 8.9 | 6.0 | 8.0 | 6.0 | 8.0 |
| Lead/Lag | | | | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | C-Min | None | C-Min |

Intersection Summary

Cycle Length: 190

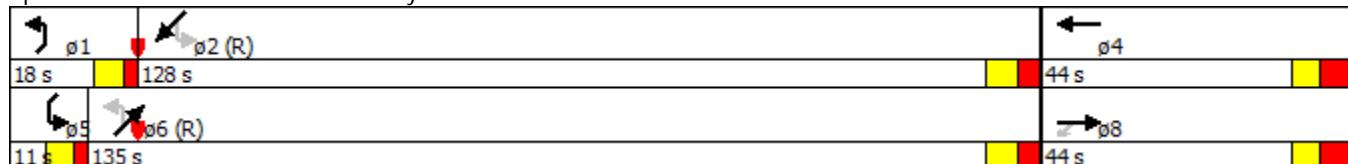
Actuated Cycle Length: 190

Offset: 160 (84%), Referenced to phase 2:SWTL and 6:NETL, Start of Green

Natural Cycle: 145

Control Type: Actuated-Coordinated

Splits and Phases: 2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive



HCM 2010 Signalized Intersection Summary
2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2019 Future Total
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|---------------------------------------|------|-------|------|-------|------|-------|------|-------|-------|------|------|------|
| Lane Configurations | | ↑↑ | ↑ | | ↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | |
| Traffic Volume (veh/h) | 0 | 580 | 24 | 0 | 268 | 3 | 98 | 3446 | 90 | 59 | 1814 | 215 |
| Future Volume (veh/h) | 0 | 580 | 24 | 0 | 268 | 3 | 98 | 3446 | 90 | 59 | 1814 | 215 |
| Number | 3 | 8 | 18 | 7 | 4 | 14 | 1 | 6 | 16 | 5 | 2 | 12 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.98 | 1.00 | | 0.96 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1863 | 1863 | 0 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 0 | 604 | 0 | 0 | 279 | 3 | 102 | 3590 | 94 | 61 | 1890 | 224 |
| Adj No. of Lanes | 0 | 2 | 1 | 0 | 2 | 0 | 1 | 3 | 0 | 1 | 3 | 0 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, % | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 0 | 645 | 288 | 0 | 654 | 7 | 172 | 3423 | 89 | 83 | 3069 | 360 |
| Arrive On Green | 0.00 | 0.18 | 0.00 | 0.00 | 0.18 | 0.18 | 0.03 | 0.67 | 0.67 | 0.03 | 0.67 | 0.67 |
| Sat Flow, veh/h | 0 | 3632 | 1583 | 0 | 3680 | 39 | 1774 | 5094 | 132 | 1774 | 4594 | 539 |
| Grp Volume(v), veh/h | 0 | 604 | 0 | 0 | 138 | 144 | 102 | 2378 | 1306 | 61 | 1390 | 724 |
| Grp Sat Flow(s),veh/h/ln | 0 | 1770 | 1583 | 0 | 1770 | 1856 | 1774 | 1695 | 1836 | 1774 | 1695 | 1743 |
| Q Serve(g_s), s | 0.0 | 32.0 | 0.0 | 0.0 | 13.1 | 13.1 | 3.5 | 127.7 | 127.7 | 2.4 | 43.8 | 44.8 |
| Cycle Q Clear(g_c), s | 0.0 | 32.0 | 0.0 | 0.0 | 13.1 | 13.1 | 3.5 | 127.7 | 127.7 | 2.4 | 43.8 | 44.8 |
| Prop In Lane | 0.00 | | 1.00 | 0.00 | | 0.02 | 1.00 | | 0.07 | 1.00 | | 0.31 |
| Lane Grp Cap(c), veh/h | 0 | 645 | 288 | 0 | 322 | 338 | 172 | 2278 | 1234 | 83 | 2265 | 1165 |
| V/C Ratio(X) | 0.00 | 0.94 | 0.00 | 0.00 | 0.43 | 0.43 | 0.59 | 1.04 | 1.06 | 0.74 | 0.61 | 0.62 |
| Avail Cap(c_a), veh/h | 0 | 654 | 292 | 0 | 327 | 343 | 233 | 2278 | 1234 | 85 | 2265 | 1165 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 76.6 | 0.0 | 0.0 | 68.9 | 68.9 | 20.5 | 31.2 | 31.2 | 54.5 | 17.7 | 17.9 |
| Incr Delay (d2), s/veh | 0.0 | 21.0 | 0.0 | 0.0 | 0.9 | 0.9 | 1.2 | 31.4 | 42.8 | 24.6 | 1.3 | 2.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.0 | 17.6 | 0.0 | 0.0 | 6.5 | 6.8 | 2.7 | 69.4 | 79.1 | 3.7 | 20.9 | 22.3 |
| LnGrp Delay(d),s/veh | 0.0 | 97.6 | 0.0 | 0.0 | 69.8 | 69.8 | 21.7 | 62.6 | 74.0 | 79.1 | 19.0 | 20.4 |
| LnGrp LOS | F | | | | E | E | C | F | F | E | B | C |
| Approach Vol, veh/h | | 604 | | | 282 | | | 3786 | | | 2175 | |
| Approach Delay, s/veh | | 97.6 | | | 69.8 | | | 65.4 | | | 21.1 | |
| Approach LOS | | F | | | E | | | E | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 11.5 | 134.9 | | 43.5 | 10.8 | 135.7 | | 43.5 | | | | |
| Change Period (Y+R _c), s | 6.0 | 8.0 | | * 8.9 | 6.0 | 8.0 | | * 8.9 | | | | |
| Max Green Setting (Gmax), s | 12.0 | 120.0 | | * 35 | 5.0 | 127.0 | | * 35 | | | | |
| Max Q Clear Time (g_c+l1), s | 5.5 | 46.8 | | 15.1 | 4.4 | 129.7 | | 34.0 | | | | |
| Green Ext Time (p_c), s | 0.1 | 60.3 | | 5.8 | 0.0 | 0.0 | | 0.6 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 54.4 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings
3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2019 Future Total
A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | NET | NER | SWT | SWR | ø1 | ø2 |
|----------------------|-------|-------|-------|-------|-------|-------|-------|------|--------|------|-------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ | | |
| Traffic Volume (vph) | 486 | 196 | 4 | 218 | 274 | 2741 | 142 | 2173 | 496 | | |
| Future Volume (vph) | 486 | 196 | 4 | 218 | 274 | 2741 | 142 | 2173 | 496 | | |
| Turn Type | Split | NA | Perm | Split | NA | NA | Prot | NA | custom | | |
| Protected Phases | 3 | 3 | | 4 | 4 | 6 | 6 | 12 | 23 | 1 | 2 |
| Permitted Phases | | | | 3 | | | | | | | |
| Detector Phase | 3 | 3 | 3 | 4 | 4 | 6 | 6 | 12 | 23 | | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 15.0 | 15.0 | | | 1.0 | 15.0 |
| Minimum Split (s) | 26.1 | 26.1 | 26.1 | 26.1 | 26.1 | 25.5 | 25.5 | | | 25.0 | 32.5 |
| Total Split (s) | 33.0 | 33.0 | 33.0 | 28.0 | 28.0 | 129.0 | 129.0 | | | 25.0 | 104.0 |
| Total Split (%) | 17.4% | 17.4% | 17.4% | 14.7% | 14.7% | 67.9% | 67.9% | | | 13% | 55% |
| Yellow Time (s) | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.8 | 4.8 | | | 2.0 | 4.8 |
| All-Red Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 2.7 | 2.7 | | | 0.0 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | 7.5 | 7.5 | | | | |
| Lead/Lag | Lead | Lead | Lead | Lag | Lag | | | | | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | | | | Yes | Yes |
| Recall Mode | None | None | None | None | None | C-Min | C-Min | | | Max | C-Min |

Intersection Summary

Cycle Length: 190

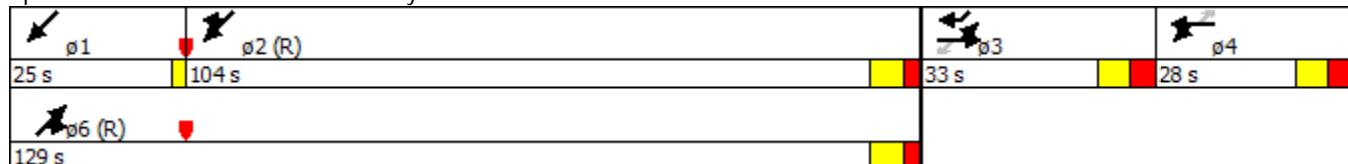
Actuated Cycle Length: 190

Offset: 99 (52%), Referenced to phase 2:SWT and 6:NET, Start of Green

Natural Cycle: 140

Control Type: Actuated-Coordinated

Splits and Phases: 3: US 1/S Dixie Hwy & SW 40th St/Bird Rd



HCM Signalized Intersection Capacity Analysis
3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2019 Future Total
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|-----------------------------------|-------|-------|-------|-------|-------|------|---------------------------|-------|-------|------|-------|--------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | ↑ | | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 486 | 196 | 4 | 218 | 274 | 0 | 0 | 2741 | 142 | 0 | 2173 | 496 |
| Future Volume (vph) | 486 | 196 | 4 | 218 | 274 | 0 | 0 | 2741 | 142 | 0 | 2173 | 496 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | | | 7.5 | 7.5 | | 2.0 | 7.5 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | | | 0.91 | 1.00 | | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (prot) | 3221 | 1678 | 1532 | 1770 | 3539 | | | 5085 | 1583 | | 5085 | 1583 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (perm) | 3221 | 1678 | 1532 | 1770 | 3539 | | | 5085 | 1583 | | 5085 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 517 | 209 | 4 | 232 | 291 | 0 | 0 | 2916 | 151 | 0 | 2312 | 528 |
| RTOR Reduction (vph) | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 465 | 261 | 1 | 232 | 291 | 0 | 0 | 2916 | 151 | 0 | 2312 | 528 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | | | | | | |
| Confl. Bikes (#/hr) | | | | 4 | | | | | | | | |
| Turn Type | Split | NA | Perm | Split | NA | Perm | | NA | Prot | | NA | custom |
| Protected Phases | 3 | 3 | | 4 | 4 | | | 6 | 6 | | 12 | 23 |
| Permitted Phases | | | 3 | | | 4 | | | | | | |
| Actuated Green, G (s) | 24.9 | 24.9 | 24.9 | 19.9 | 19.9 | | | 121.5 | 121.5 | | 121.5 | 128.9 |
| Effective Green, g (s) | 24.9 | 24.9 | 24.9 | 19.9 | 19.9 | | | 121.5 | 121.5 | | 121.5 | 128.9 |
| Actuated g/C Ratio | 0.13 | 0.13 | 0.13 | 0.10 | 0.10 | | | 0.64 | 0.64 | | 0.64 | 0.68 |
| Clearance Time (s) | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | | | 7.5 | 7.5 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | | | 1.0 | 1.0 | | | |
| Lane Grp Cap (vph) | 422 | 219 | 200 | 185 | 370 | | | 3251 | 1012 | | 3251 | 1073 |
| v/s Ratio Prot | 0.14 | c0.16 | | c0.13 | 0.08 | | | c0.57 | 0.10 | | 0.45 | 0.33 |
| v/s Ratio Perm | | | | 0.00 | | | | | | | | |
| v/c Ratio | 1.10 | 1.19 | 0.00 | 1.25 | 0.79 | | | 0.90 | 0.15 | | 0.71 | 0.49 |
| Uniform Delay, d1 | 82.5 | 82.5 | 71.8 | 85.0 | 83.0 | | | 29.0 | 13.7 | | 22.6 | 14.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 74.3 | 122.3 | 0.0 | 150.7 | 10.2 | | | 4.4 | 0.3 | | 1.3 | 0.4 |
| Delay (s) | 156.9 | 204.9 | 71.8 | 235.8 | 93.2 | | | 33.4 | 14.0 | | 24.0 | 15.1 |
| Level of Service | F | F | E | F | F | | | C | B | | C | B |
| Approach Delay (s) | | | 173.6 | | 156.4 | | | 32.4 | | | 22.3 | |
| Approach LOS | | | F | | F | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | | 51.9 | | | HCM 2000 Level of Service | | D | | | |
| HCM 2000 Volume to Capacity ratio | | | | 0.99 | | | | | | | | |
| Actuated Cycle Length (s) | | | | 190.0 | | | Sum of lost time (s) | | 25.7 | | | |
| Intersection Capacity Utilization | | | | 97.2% | | | ICU Level of Service | | F | | | |
| Analysis Period (min) | | | | 15 | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Timings
4: SW 27th Ave & US 1/S Dixie Hwy

2019 Future Total

A.M. Peak Hour

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↓ | ↑ | ↑↑↓ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 171 | 2900 | 44 | 2679 | 31 | 335 | 210 | 80 | 486 | 363 |
| Future Volume (vph) | 171 | 2900 | 44 | 2679 | 31 | 335 | 210 | 80 | 486 | 363 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Perm | Perm | NA | pm+ov |
| Protected Phases | 1 | 6 | | 2 | | 4 | | 4 | 8 | 1 |
| Permitted Phases | 6 | | 2 | | 4 | | 4 | 8 | | 8 |
| Detector Phase | 1 | 6 | 2 | 2 | 4 | 4 | 4 | 8 | 8 | 1 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 |
| Minimum Split (s) | 9.5 | 39.9 | 39.9 | 39.9 | 29.6 | 29.6 | 29.6 | 29.6 | 29.6 | 9.5 |
| Total Split (s) | 31.0 | 158.0 | 127.0 | 127.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 | 31.0 |
| Total Split (%) | 16.3% | 83.2% | 66.8% | 66.8% | 16.8% | 16.8% | 16.8% | 16.8% | 16.8% | 16.3% |
| Yellow Time (s) | 3.5 | 4.8 | 4.8 | 4.8 | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 3.5 |
| All-Red Time (s) | 1.0 | 2.1 | 2.1 | 2.1 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 6.9 | 6.9 | 6.9 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 | 4.5 |
| Lead/Lag | Lead | | Lag | Lag | | | | | | Lead |
| Lead-Lag Optimize? | Yes | | Yes | Yes | | | | | | Yes |
| Recall Mode | None | C-Min | C-Min | C-Min | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 190

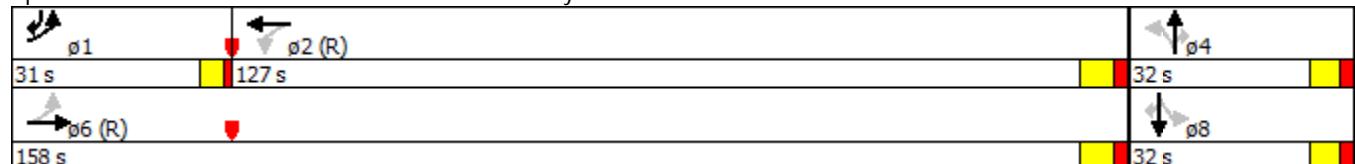
Actuated Cycle Length: 190

Offset: 39 (21%), Referenced to phase 2:WBTL and 6:EBTL, Start of Green

Natural Cycle: 120

Control Type: Actuated-Coordinated

Splits and Phases: 4: SW 27th Ave & US 1/S Dixie Hwy



HCM 2010 Signalized Intersection Summary
4: SW 27th Ave & US 1/S Dixie Hwy

2019 Future Total
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|-------|------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 171 | 2900 | 18 | 44 | 2679 | 61 | 31 | 335 | 210 | 80 | 486 | 363 |
| Future Volume (veh/h) | 171 | 2900 | 18 | 44 | 2679 | 61 | 31 | 335 | 210 | 80 | 486 | 363 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.85 | 0.97 | | 0.85 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 176 | 2990 | 19 | 45 | 2762 | 0 | 32 | 345 | 216 | 82 | 501 | 374 |
| Adj No. of Lanes | 1 | 3 | 0 | 1 | 3 | 0 | 1 | 2 | 1 | 1 | 2 | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 196 | 4146 | 26 | 78 | 3571 | 0 | 38 | 473 | 179 | 71 | 473 | 289 |
| Arrive On Green | 0.07 | 0.80 | 0.80 | 0.70 | 0.70 | 0.00 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| Sat Flow, veh/h | 1774 | 5214 | 33 | 78 | 5253 | 0 | 631 | 3539 | 1342 | 822 | 3539 | 1340 |
| Grp Volume(v), veh/h | 176 | 1942 | 1067 | 45 | 2762 | 0 | 32 | 345 | 216 | 82 | 501 | 374 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1857 | 78 | 1695 | 0 | 631 | 1770 | 1342 | 822 | 1770 | 1340 |
| Q Serve(g_s), s | 10.8 | 52.2 | 52.6 | 98.5 | 67.3 | 0.0 | 0.0 | 17.8 | 25.4 | 7.6 | 25.4 | 25.4 |
| Cycle Q Clear(g_c), s | 10.8 | 52.2 | 52.6 | 133.4 | 67.3 | 0.0 | 25.4 | 17.8 | 25.4 | 25.4 | 25.4 | 25.4 |
| Prop In Lane | 1.00 | | 0.02 | 1.00 | | 0.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 196 | 2696 | 1477 | 78 | 3571 | 0 | 38 | 473 | 179 | 71 | 473 | 289 |
| V/C Ratio(X) | 0.90 | 0.72 | 0.72 | 0.57 | 0.77 | 0.00 | 0.84 | 0.73 | 1.20 | 1.16 | 1.06 | 1.29 |
| Avail Cap(c_a), veh/h | 320 | 2696 | 1477 | 78 | 3571 | 0 | 38 | 473 | 179 | 71 | 473 | 289 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 61.3 | 9.3 | 9.4 | 50.5 | 18.4 | 0.0 | 95.0 | 79.0 | 82.3 | 93.2 | 82.3 | 76.4 |
| Incr Delay (d2), s/veh | 17.2 | 1.7 | 3.1 | 27.0 | 1.7 | 0.0 | 88.0 | 5.9 | 132.6 | 155.7 | 57.8 | 155.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 10.1 | 24.6 | 27.9 | 3.0 | 31.8 | 0.0 | 2.6 | 9.1 | 16.0 | 6.8 | 16.2 | 27.7 |
| LnGrp Delay(d),s/veh | 78.6 | 11.0 | 12.5 | 77.5 | 20.1 | 0.0 | 183.0 | 84.9 | 214.9 | 249.0 | 140.1 | 231.9 |
| LnGrp LOS | E | B | B | E | C | | F | F | F | F | F | F |
| Approach Vol, veh/h | | 3185 | | | 2807 | | | 593 | | | 957 | |
| Approach Delay, s/veh | | 15.2 | | | 21.1 | | | 137.5 | | | 185.3 | |
| Approach LOS | | B | | | C | | | F | | | F | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 17.7 | 140.3 | | 32.0 | | 158.0 | | 32.0 | | | | |
| Change Period (Y+R _c), s | 4.5 | 6.9 | | * 6.6 | | 6.9 | | * 6.6 | | | | |
| Max Green Setting (Gmax), s | 26.5 | 120.1 | | * 25 | | 151.1 | | * 25 | | | | |
| Max Q Clear Time (g_c+l1), s | 12.8 | 135.4 | | 27.4 | | 54.6 | | 27.4 | | | | |
| Green Ext Time (p_c), s | 0.4 | 0.0 | | 0.0 | | 81.1 | | 0.0 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 48.6 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings
5: SE 26th Rd & US 1/Brickell Ave

2019 Future Total
A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBT | WBR | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 238 | 1265 | 18 | 211 | 273 | 905 | 555 | 137 | 554 | 104 |
| Future Volume (vph) | 238 | 1265 | 18 | 211 | 273 | 905 | 555 | 137 | 554 | 104 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Free | Prot | NA | Perm |
| Protected Phases | 7 | 4 | | 8 | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | Free | | | 6 |
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 11.0 | 27.8 | 27.8 | 27.8 | 27.8 | 33.6 | | 11.0 | 33.6 | 33.6 |
| Total Split (s) | 23.0 | 53.0 | 53.0 | 30.0 | 30.0 | 52.0 | | 15.0 | 67.0 | 67.0 |
| Total Split (%) | 19.2% | 44.2% | 44.2% | 25.0% | 25.0% | 43.3% | | 12.5% | 55.8% | 55.8% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.8 | 2.8 | 2.8 | 2.8 | 2.6 | | 2.0 | 2.6 | 2.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.8 | 6.8 | 6.8 | 6.8 | 6.6 | | 6.0 | 6.6 | 6.6 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | | Yes | | |
| Recall Mode | None | Max | Max | None | None | C-Min | | None | C-Min | C-Min |

Intersection Summary

Cycle Length: 120

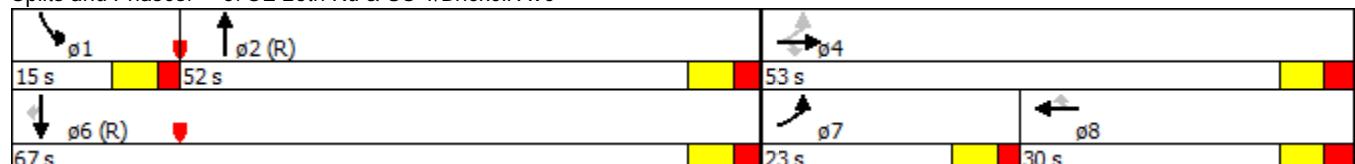
Actuated Cycle Length: 120

Offset: 74 (62%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Natural Cycle: 85

Control Type: Actuated-Coordinated

Splits and Phases: 5: SE 26th Rd & US 1/Brickell Ave



HCM 2010 Signalized Intersection Summary
5: SE 26th Rd & US 1/Brickell Ave

2019 Future Total
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|-------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | | ↑↑ | ↑ | | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 238 | 1265 | 18 | 0 | 211 | 273 | 0 | 905 | 555 | 137 | 554 | 104 |
| Future Volume (veh/h) | 238 | 1265 | 18 | 0 | 211 | 273 | 0 | 905 | 555 | 137 | 554 | 104 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 0 | 1863 | 1863 | 0 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 294 | 1562 | 0 | 0 | 260 | 0 | 0 | 1117 | 0 | 169 | 684 | 0 |
| Adj No. of Lanes | 1 | 3 | 1 | 0 | 2 | 1 | 0 | 2 | 1 | 2 | 2 | 1 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 224 | 1781 | 797 |
| Arrive On Green | 0.14 | 0.38 | 0.00 | 0.00 | 0.19 | 0.00 | 0.00 | 0.39 | 0.00 | 0.07 | 0.50 | 0.00 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 0 | 3632 | 1583 | 0 | 3632 | 1583 | 3442 | 3539 | 1583 |
| Grp Volume(v), veh/h | 294 | 1562 | 0 | 0 | 260 | 0 | 0 | 1117 | 0 | 169 | 684 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 0 | 1770 | 1583 | 0 | 1770 | 1583 | 1721 | 1770 | 1583 |
| Q Serve(g_s), s | 15.5 | 32.7 | 0.0 | 0.0 | 7.7 | 0.0 | 0.0 | 33.8 | 0.0 | 5.8 | 14.3 | 0.0 |
| Cycle Q Clear(g_c), s | 15.5 | 32.7 | 0.0 | 0.0 | 7.7 | 0.0 | 0.0 | 33.8 | 0.0 | 5.8 | 14.3 | 0.0 |
| Prop In Lane | 1.00 | | | 1.00 | 0.00 | | 1.00 | 0.00 | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 224 | 1781 | 797 |
| V/C Ratio(X) | 0.65 | 0.80 | 0.00 | 0.00 | 0.38 | 0.00 | 0.00 | 0.81 | 0.00 | 0.76 | 0.38 | 0.00 |
| Avail Cap(c_a), veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 258 | 1781 | 797 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 30.8 | 32.8 | 0.0 | 0.0 | 42.1 | 0.0 | 0.0 | 32.8 | 0.0 | 55.2 | 18.3 | 0.0 |
| Incr Delay (d2), s/veh | 2.5 | 3.5 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 5.3 | 0.0 | 8.4 | 0.6 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 7.8 | 16.0 | 0.0 | 0.0 | 3.8 | 0.0 | 0.0 | 17.5 | 0.0 | 3.0 | 7.1 | 0.0 |
| LnGrp Delay(d),s/veh | 33.2 | 36.2 | 0.0 | 0.0 | 42.4 | 0.0 | 0.0 | 38.1 | 0.0 | 63.6 | 19.0 | 0.0 |
| LnGrp LOS | C | D | | | D | | | D | | E | B | |
| Approach Vol, veh/h | | 1856 | | | 260 | | | 1117 | | | 853 | |
| Approach Delay, s/veh | | 35.8 | | | 42.4 | | | 38.1 | | | 27.8 | |
| Approach LOS | | D | | | D | | | D | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 13.8 | 53.2 | | 53.0 | | 67.0 | 23.0 | 30.0 | | | | |
| Change Period (Y+R _c), s | 6.0 | 6.6 | | * 6.8 | | 6.6 | 6.0 | * 6.8 | | | | |
| Max Green Setting (Gmax), s | 9.0 | 45.4 | | * 46 | | 60.4 | 17.0 | * 23 | | | | |
| Max Q Clear Time (g_c+l1), s | 7.8 | 35.8 | | 34.7 | | 16.3 | 17.5 | 9.7 | | | | |
| Green Ext Time (p_c), s | 0.0 | 4.2 | | 7.9 | | 6.3 | 0.0 | 8.9 | | | | |

Intersection Summary

| | |
|---------------------|------|
| HCM 2010 Ctrl Delay | 35.2 |
| HCM 2010 LOS | D |

Notes

Timings

1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2016 Existing Conditions

P.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | SWL | SWT | SWR |
|----------------------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 450 | 458 | 491 | 142 | 494 | 39 | 1350 | 112 | 1839 | 645 |
| Future Volume (vph) | 450 | 458 | 491 | 142 | 494 | 39 | 1350 | 112 | 1839 | 645 |
| Turn Type | Split | NA | Free | Split | NA | Perm | NA | pm+pt | NA | pm+ov |
| Protected Phases | 8 | 8 | | 7 | 7 | | 6 | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | 7 | | 2 | | 2 |
| Detector Phase | 8 | 8 | | 7 | 7 | 7 | 6 | 5 | 2 | 8 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 44.7 | 44.7 | | 15.9 | 15.9 | 15.9 | 40.7 | 11.8 | 40.7 | 44.7 |
| Total Split (s) | 48.0 | 48.0 | | 45.0 | 45.0 | 45.0 | 83.0 | 14.0 | 97.0 | 48.0 |
| Total Split (%) | 25.3% | 25.3% | | 23.7% | 23.7% | 23.7% | 43.7% | 7.4% | 51.1% | 25.3% |
| Yellow Time (s) | 4.8 | 4.8 | | 4.0 | 4.0 | 4.0 | 4.8 | 4.8 | 4.8 | 4.8 |
| All-Red Time (s) | 2.9 | 2.9 | | 4.1 | 4.1 | 4.1 | 2.9 | 2.0 | 2.9 | 2.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | 7.7 | 6.8 | 7.7 | 7.7 |
| Lead/Lag | Lag | Lag | | Lead | Lead | Lead | Lag | Lead | | Lag |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | | Yes |
| Recall Mode | None | None | | None | None | None | C-Min | None | C-Min | None |

Intersection Summary

Cycle Length: 190

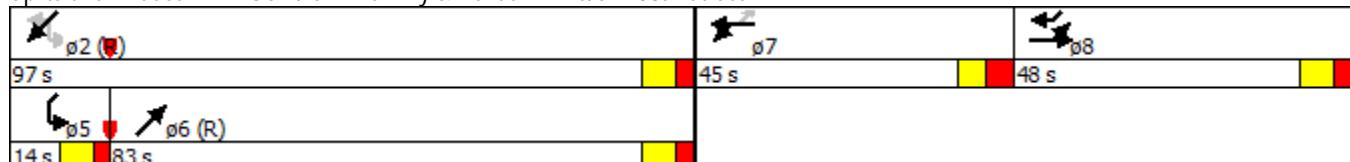
Actuated Cycle Length: 190

Offset: 116 (61%), Referenced to phase 2:SWTL and 6:NET, Start of Green

Natural Cycle: 135

Control Type: Actuated-Coordinated

Splits and Phases: 1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street



HCM Signalized Intersection Capacity Analysis
1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2016 Existing Conditions

P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|------------------------|-------|------|-------|-------|-------|------|------|------|------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 450 | 458 | 491 | 142 | 494 | 39 | 0 | 1350 | 125 | 112 | 1839 | 645 |
| Future Volume (vph) | 450 | 458 | 491 | 142 | 494 | 39 | 0 | 1350 | 125 | 112 | 1839 | 645 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.7 | 7.7 | 4.0 | 8.1 | 8.1 | 8.1 | | 7.7 | | 6.8 | 7.7 | 7.7 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | | 1.00 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1610 | 3348 | 1563 | 1770 | 3539 | 1583 | | 5014 | | 1770 | 5085 | 1568 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.05 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1610 | 3348 | 1563 | 1770 | 3539 | 1583 | | 5014 | | 99 | 5085 | 1568 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 459 | 467 | 501 | 145 | 504 | 40 | 0 | 1378 | 128 | 114 | 1877 | 658 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 33 | 0 | 6 | 0 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 303 | 623 | 501 | 145 | 504 | 7 | 0 | 1500 | 0 | 114 | 1877 | 648 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | 1 | | 2 | 2 | | 1 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | 4 |
| Turn Type | Split | NA | Free | Split | NA | Perm | | NA | | pm+pt | NA | pm+ov |
| Protected Phases | 8 | 8 | | 7 | 7 | | | 6 | | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | 7 | | | | 2 | | 2 |
| Actuated Green, G (s) | 45.1 | 45.1 | 190.0 | 34.4 | 34.4 | 34.4 | | 70.6 | | 87.0 | 87.0 | 132.1 |
| Effective Green, g (s) | 45.1 | 45.1 | 190.0 | 34.4 | 34.4 | 34.4 | | 70.6 | | 87.0 | 87.0 | 132.1 |
| Actuated g/C Ratio | 0.24 | 0.24 | 1.00 | 0.18 | 0.18 | 0.18 | | 0.37 | | 0.46 | 0.46 | 0.70 |
| Clearance Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | | 7.7 | | 6.8 | 7.7 | 7.7 |
| Vehicle Extension (s) | 3.5 | 3.5 | | 4.0 | 4.0 | 4.0 | | 1.0 | | 2.0 | 1.0 | 3.5 |
| Lane Grp Cap (vph) | 382 | 794 | 1563 | 320 | 640 | 286 | | 1863 | | 129 | 2328 | 1153 |
| v/s Ratio Prot | c0.19 | 0.19 | | 0.08 | c0.14 | | | 0.30 | | 0.04 | c0.37 | 0.13 |
| v/s Ratio Perm | | | 0.32 | | | 0.00 | | | | c0.36 | | 0.28 |
| v/c Ratio | 0.79 | 0.78 | 0.32 | 0.45 | 0.79 | 0.03 | | 0.81 | | 0.88 | 0.81 | 0.56 |
| Uniform Delay, d1 | 68.1 | 67.9 | 0.0 | 69.4 | 74.3 | 64.0 | | 53.5 | | 47.0 | 44.3 | 14.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 11.1 | 5.3 | 0.5 | 1.4 | 6.7 | 0.0 | | 3.8 | | 44.8 | 3.1 | 0.7 |
| Delay (s) | 79.1 | 73.2 | 0.5 | 70.8 | 81.0 | 64.1 | | 57.4 | | 91.8 | 47.4 | 15.2 |
| Level of Service | E | E | A | E | F | E | | E | | F | D | B |
| Approach Delay (s) | | 48.9 | | | 77.9 | | | 57.4 | | | 41.3 | |
| Approach LOS | | D | | | E | | | E | | | D | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|---|
| HCM 2000 Control Delay | 50.9 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.87 | | |
| Actuated Cycle Length (s) | 190.0 | Sum of lost time (s) | |
| Intersection Capacity Utilization | 91.7% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

Timings

2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2016 Existing Conditions

P.M. Peak Hour

| Lane Group | EBT | EBR | WBT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ |
| Traffic Volume (vph) | 518 | 84 | 468 | 128 | 2010 | 49 | 2633 |
| Future Volume (vph) | 518 | 84 | 468 | 128 | 2010 | 49 | 2633 |
| Turn Type | NA | Perm | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 8 | | 4 | 1 | 6 | 5 | 2 |
| Permitted Phases | | | | 6 | | 2 | |
| Detector Phase | 8 | 8 | 4 | 1 | 6 | 5 | 2 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 12.0 | 12.0 | 12.0 | 5.0 | 7.0 | 5.0 | 7.0 |
| Minimum Split (s) | 34.9 | 34.9 | 34.9 | 11.0 | 37.0 | 11.4 | 37.0 |
| Total Split (s) | 44.0 | 44.0 | 44.0 | 11.0 | 133.0 | 13.0 | 135.0 |
| Total Split (%) | 23.2% | 23.2% | 23.2% | 5.8% | 70.0% | 6.8% | 71.1% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.4 | 4.0 | 4.4 |
| All-Red Time (s) | 4.9 | 4.9 | 4.9 | 2.0 | 3.6 | 2.0 | 3.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.9 | 8.9 | 8.9 | 6.0 | 8.0 | 6.0 | 8.0 |
| Lead/Lag | | | | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | C-Min | None | C-Min |

Intersection Summary

Cycle Length: 190

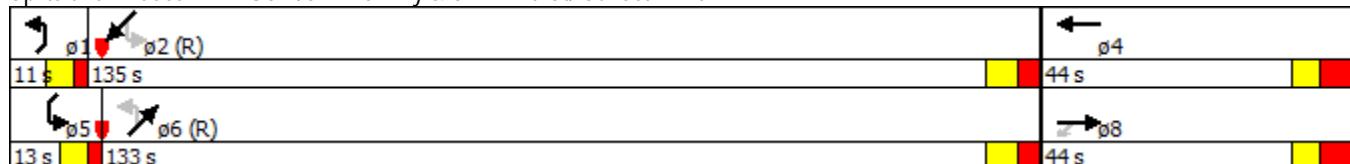
Actuated Cycle Length: 190

Offset: 161 (85%), Referenced to phase 2:SWTL and 6:NETL, Start of Green

Natural Cycle: 125

Control Type: Actuated-Coordinated

Splits and Phases: 2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive



HCM 2010 Signalized Intersection Summary
2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2016 Existing Conditions
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|---------------------------------------|------|-------|------|-------|------|-------|-------|-------|------|------|------|------|
| Lane Configurations | | ↑↑ | ↑ | | ↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | |
| Traffic Volume (veh/h) | 0 | 518 | 84 | 0 | 468 | 9 | 128 | 2010 | 89 | 49 | 2633 | 251 |
| Future Volume (veh/h) | 0 | 518 | 84 | 0 | 468 | 9 | 128 | 2010 | 89 | 49 | 2633 | 251 |
| Number | 3 | 8 | 18 | 7 | 4 | 14 | 1 | 6 | 16 | 5 | 2 | 12 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 0.90 | 1.00 | | 0.98 | 1.00 | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1863 | 1863 | 0 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 0 | 534 | 0 | 0 | 482 | 9 | 132 | 2072 | 92 | 51 | 2714 | 259 |
| Adj No. of Lanes | 0 | 2 | 1 | 0 | 2 | 0 | 1 | 3 | 0 | 1 | 3 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 0 | 610 | 273 | 0 | 611 | 11 | 102 | 3405 | 151 | 165 | 3220 | 297 |
| Arrive On Green | 0.00 | 0.17 | 0.00 | 0.00 | 0.17 | 0.17 | 0.03 | 0.68 | 0.68 | 0.02 | 0.68 | 0.68 |
| Sat Flow, veh/h | 0 | 3632 | 1583 | 0 | 3639 | 66 | 1774 | 4989 | 221 | 1774 | 4730 | 436 |
| Grp Volume(v), veh/h | 0 | 534 | 0 | 0 | 240 | 251 | 132 | 1406 | 758 | 51 | 1919 | 1054 |
| Grp Sat Flow(s),veh/h/ln | 0 | 1770 | 1583 | 0 | 1770 | 1843 | 1774 | 1695 | 1819 | 1774 | 1695 | 1776 |
| Q Serve(g_s), s | 0.0 | 27.9 | 0.0 | 0.0 | 24.7 | 24.8 | 5.0 | 42.7 | 43.1 | 1.7 | 79.1 | 88.5 |
| Cycle Q Clear(g_c), s | 0.0 | 27.9 | 0.0 | 0.0 | 24.7 | 24.8 | 5.0 | 42.7 | 43.1 | 1.7 | 79.1 | 88.5 |
| Prop In Lane | 0.00 | | 1.00 | 0.00 | | 0.04 | 1.00 | | 0.12 | 1.00 | | 0.25 |
| Lane Grp Cap(c), veh/h | 0 | 610 | 273 | 0 | 305 | 318 | 102 | 2314 | 1242 | 165 | 2308 | 1209 |
| V/C Ratio(X) | 0.00 | 0.88 | 0.00 | 0.00 | 0.79 | 0.79 | 1.29 | 0.61 | 0.61 | 0.31 | 0.83 | 0.87 |
| Avail Cap(c_a), veh/h | 0 | 654 | 292 | 0 | 327 | 340 | 102 | 2314 | 1242 | 186 | 2308 | 1209 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 76.6 | 0.0 | 0.0 | 75.3 | 75.3 | 57.5 | 16.4 | 16.4 | 15.2 | 22.3 | 23.8 |
| Incr Delay (d2), s/veh | 0.0 | 12.1 | 0.0 | 0.0 | 11.4 | 11.2 | 187.1 | 1.2 | 2.2 | 0.4 | 3.7 | 8.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.0 | 14.7 | 0.0 | 0.0 | 13.0 | 13.6 | 10.7 | 20.3 | 22.3 | 0.9 | 38.0 | 46.0 |
| LnGrp Delay(d),s/veh | 0.0 | 88.8 | 0.0 | 0.0 | 86.7 | 86.5 | 244.6 | 17.5 | 18.7 | 15.6 | 26.0 | 32.6 |
| LnGrp LOS | | F | | | F | F | B | B | B | C | C | |
| Approach Vol, veh/h | | 534 | | | 491 | | | 2296 | | | 3024 | |
| Approach Delay, s/veh | | 88.8 | | | 86.6 | | | 31.0 | | | 28.1 | |
| Approach LOS | | F | | | F | | | C | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 11.0 | 137.4 | | 41.6 | 10.7 | 137.7 | | 41.6 | | | | |
| Change Period (Y+R _c), s | 6.0 | 8.0 | | * 8.9 | 6.0 | 8.0 | | * 8.9 | | | | |
| Max Green Setting (Gmax), s | 5.0 | 127.0 | | * 35 | 7.0 | 125.0 | | * 35 | | | | |
| Max Q Clear Time (g_c+l1), s | 7.0 | 90.5 | | 26.8 | 3.7 | 45.1 | | 29.9 | | | | |
| Green Ext Time (p_c), s | 0.0 | 29.4 | | 4.0 | 0.0 | 51.6 | | 2.8 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 38.8 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings

3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2016 Existing Conditions

P.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | NER | SWT | SWR | ø1 | ø2 |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|------|--------|------|-------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ | | |
| Traffic Volume (vph) | 367 | 136 | 20 | 172 | 314 | 3 | 2310 | 200 | 2095 | 621 | | |
| Future Volume (vph) | 367 | 136 | 20 | 172 | 314 | 3 | 2310 | 200 | 2095 | 621 | | |
| Turn Type | Split | NA | Perm | Split | NA | Perm | NA | Prot | NA | custom | | |
| Protected Phases | 3 | 3 | | 4 | 4 | | 6 | 6 | 12 | 23 | 1 | 2 |
| Permitted Phases | | | | 3 | | 4 | | | | | | |
| Detector Phase | 3 | 3 | 3 | 4 | 4 | 4 | 6 | 6 | 12 | 23 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 15.0 | 15.0 | | | 1.0 | 15.0 |
| Minimum Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 25.5 | 25.5 | | | 25.0 | 32.5 |
| Total Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 138.0 | 138.0 | | | 25.0 | 113.0 |
| Total Split (%) | 13.7% | 13.7% | 13.7% | 13.7% | 13.7% | 13.7% | 72.6% | 72.6% | | | 13% | 59% |
| Yellow Time (s) | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.8 | 4.8 | | | 2.0 | 4.8 |
| All-Red Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.7 | 2.7 | | | 0.0 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 7.5 | 7.5 | | | | |
| Lead/Lag | Lead | Lead | Lead | Lag | Lag | Lag | | | | | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | | | | | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C-Min | C-Min | | | Max | C-Min |

Intersection Summary

Cycle Length: 190

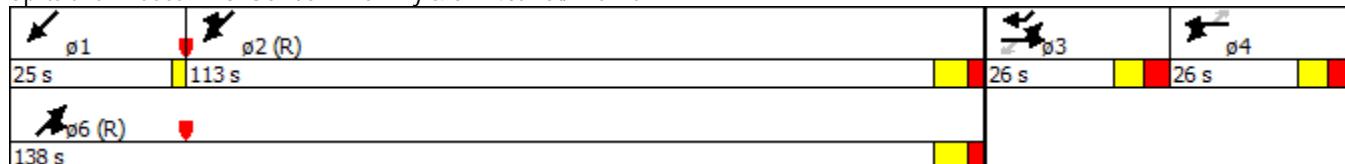
Actuated Cycle Length: 190

Offset: 136 (72%), Referenced to phase 2:SWT and 6:NET, Start of Green

Natural Cycle: 110

Control Type: Actuated-Coordinated

Splits and Phases: 3: US 1/S Dixie Hwy & SW 40th St/Bird Rd



HCM Signalized Intersection Capacity Analysis
3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2016 Existing Conditions

P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|-----------------------------------|-------|-------|-------|-------|---------------------------|------|------|-------|-------|------|-------|--------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | ↑ | | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 367 | 136 | 20 | 172 | 314 | 3 | 0 | 2310 | 200 | 0 | 2095 | 621 |
| Future Volume (vph) | 367 | 136 | 20 | 172 | 314 | 3 | 0 | 2310 | 200 | 0 | 2095 | 621 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | 7.5 | 7.5 | | 2.0 | 7.5 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | 1.00 | | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (prot) | 3221 | 1677 | 1523 | 1770 | 3539 | 1583 | | 5085 | 1583 | | 5085 | 1583 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (perm) | 3221 | 1677 | 1523 | 1770 | 3539 | 1583 | | 5085 | 1583 | | 5085 | 1583 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 386 | 143 | 21 | 181 | 331 | 3 | 0 | 2432 | 211 | 0 | 2205 | 654 |
| RTOR Reduction (vph) | 0 | 0 | 18 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 347 | 182 | 3 | 181 | 331 | 0 | 0 | 2432 | 211 | 0 | 2205 | 654 |
| Confl. Peds. (#/hr) | | | 5 | 5 | | | 7 | | | | | 7 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | | | | 6 |
| Turn Type | Split | NA | Perm | Split | NA | Perm | | NA | Prot | | NA | custom |
| Protected Phases | 3 | 3 | | 4 | 4 | | | 6 | 6 | | 12 | 23 |
| Permitted Phases | | | 3 | | | 4 | | | | | | |
| Actuated Green, G (s) | 26.1 | 26.1 | 26.1 | 22.6 | 22.6 | 22.6 | | 117.8 | 117.8 | | 117.8 | 123.6 |
| Effective Green, g (s) | 26.1 | 26.1 | 26.1 | 22.6 | 22.6 | 22.6 | | 117.8 | 117.8 | | 117.8 | 123.6 |
| Actuated g/C Ratio | 0.14 | 0.14 | 0.14 | 0.12 | 0.12 | 0.12 | | 0.62 | 0.62 | | 0.62 | 0.65 |
| Clearance Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | 7.5 | 7.5 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | | 1.0 | 1.0 | | | |
| Lane Grp Cap (vph) | 442 | 230 | 209 | 210 | 420 | 188 | | 3152 | 981 | | 3152 | 1029 |
| v/s Ratio Prot | 0.11 | c0.11 | | c0.10 | 0.09 | | | c0.48 | 0.13 | | 0.43 | 0.41 |
| v/s Ratio Perm | | | 0.00 | | | 0.00 | | | | | | |
| v/c Ratio | 0.79 | 0.79 | 0.01 | 0.86 | 0.79 | 0.00 | | 0.77 | 0.22 | | 0.70 | 0.64 |
| Uniform Delay, d1 | 79.2 | 79.3 | 70.8 | 82.2 | 81.4 | 73.8 | | 26.3 | 15.8 | | 24.2 | 19.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 8.9 | 16.8 | 0.0 | 28.2 | 9.1 | 0.0 | | 1.9 | 0.5 | | 1.3 | 1.3 |
| Delay (s) | 88.1 | 96.1 | 70.9 | 110.4 | 90.5 | 73.8 | | 28.2 | 16.3 | | 25.5 | 21.1 |
| Level of Service | F | F | E | F | F | E | | C | B | | C | C |
| Approach Delay (s) | | 90.1 | | | 97.4 | | | 27.2 | | | 24.5 | |
| Approach LOS | | F | | | F | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 36.8 | | HCM 2000 Level of Service | | | | D | | | |
| HCM 2000 Volume to Capacity ratio | | | 0.80 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 190.0 | | Sum of lost time (s) | | | | 25.5 | | | |
| Intersection Capacity Utilization | | | 83.0% | | ICU Level of Service | | | | E | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Timings

4: SW 27th Ave & US 1/S Dixie Hwy

2016 Existing Conditions

P.M. Peak Hour

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↓ | ↑ | ↑↑↓ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 156 | 2475 | 127 | 2877 | 26 | 509 | 129 | 39 | 501 | 226 |
| Future Volume (vph) | 156 | 2475 | 127 | 2877 | 26 | 509 | 129 | 39 | 501 | 226 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | NA | pm+ov | Perm | NA | pm+ov |
| Protected Phases | 1 | 6 | 5 | 2 | | 4 | 5 | | 8 | 1 |
| Permitted Phases | 6 | | 2 | | 4 | | 4 | 8 | | 8 |
| Detector Phase | 1 | 6 | 5 | 2 | 4 | 4 | 5 | 8 | 8 | 1 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 5.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 | 5.0 |
| Minimum Split (s) | 11.8 | 39.9 | 11.8 | 39.9 | 29.6 | 29.6 | 11.8 | 29.6 | 29.6 | 11.8 |
| Total Split (s) | 16.0 | 132.0 | 20.0 | 136.0 | 38.0 | 38.0 | 20.0 | 38.0 | 38.0 | 16.0 |
| Total Split (%) | 8.4% | 69.5% | 10.5% | 71.6% | 20.0% | 20.0% | 10.5% | 20.0% | 20.0% | 8.4% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 4.8 | 4.4 | 4.4 | 4.8 | 4.4 | 4.4 | 4.8 |
| All-Red Time (s) | 2.0 | 2.1 | 2.0 | 2.1 | 2.2 | 2.2 | 2.0 | 2.2 | 2.2 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.8 | 6.9 | 6.8 | 6.9 | 6.6 | 6.6 | 6.8 | 6.6 | 6.6 | 6.8 |
| Lead/Lag | Lead | Lag | Lead | Lag | | | Lead | | Lead | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | Yes | | Yes | |
| Recall Mode | None | C-Min | None | C-Min | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 190

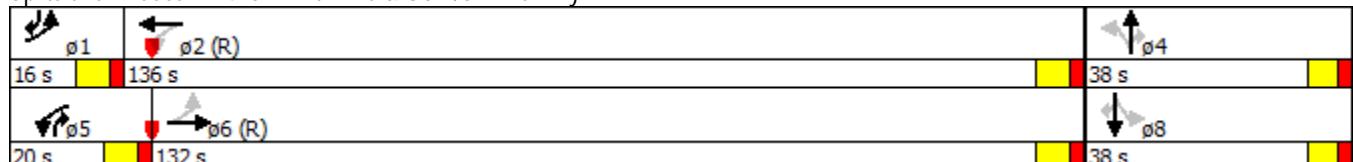
Actuated Cycle Length: 190

Offset: 71 (37%), Referenced to phase 2:WBTL and 6:EBTL, Start of Green

Natural Cycle: 125

Control Type: Actuated-Coordinated

Splits and Phases: 4: SW 27th Ave & US 1/S Dixie Hwy



HCM 2010 Signalized Intersection Summary
4: SW 27th Ave & US 1/S Dixie Hwy

2016 Existing Conditions
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|-------|-------|------|-------|------|-------|------|-------|------|-------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 156 | 2475 | 33 | 127 | 2877 | 97 | 26 | 509 | 129 | 39 | 501 | 226 |
| Future Volume (veh/h) | 156 | 2475 | 33 | 127 | 2877 | 97 | 26 | 509 | 129 | 39 | 501 | 226 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pb} T) | 1.00 | | 0.98 | 1.00 | | 1.00 | 1.00 | | 0.78 | 1.00 | | 0.77 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 156 | 2475 | 33 | 127 | 2877 | 0 | 26 | 509 | 129 | 39 | 501 | 226 |
| Adj No. of Lanes | 1 | 3 | 0 | 1 | 3 | 0 | 1 | 2 | 1 | 1 | 2 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 147 | 3591 | 48 | 151 | 3455 | 0 | 58 | 585 | 258 | 58 | 585 | 279 |
| Arrive On Green | 0.05 | 0.69 | 0.69 | 0.03 | 0.68 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 1774 | 5171 | 69 | 1774 | 5253 | 0 | 725 | 3539 | 1238 | 787 | 3539 | 1225 |
| Grp Volume(v), veh/h | 156 | 1621 | 887 | 127 | 2877 | 0 | 26 | 509 | 129 | 39 | 501 | 226 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1849 | 1774 | 1695 | 0 | 725 | 1770 | 1238 | 787 | 1770 | 1225 |
| Q Serve(g_s), s | 9.2 | 53.2 | 53.6 | 4.2 | 79.3 | 0.0 | 5.2 | 26.6 | 17.7 | 4.8 | 26.2 | 31.4 |
| Cycle Q Clear(g_c), s | 9.2 | 53.2 | 53.6 | 4.2 | 79.3 | 0.0 | 31.4 | 26.6 | 17.7 | 31.4 | 26.2 | 31.4 |
| Prop In Lane | 1.00 | | 0.04 | 1.00 | | 0.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 147 | 2354 | 1284 | 151 | 3455 | 0 | 58 | 585 | 258 | 58 | 585 | 279 |
| V/C Ratio(X) | 1.06 | 0.69 | 0.69 | 0.84 | 0.83 | 0.00 | 0.45 | 0.87 | 0.50 | 0.68 | 0.86 | 0.81 |
| Avail Cap(c_a), veh/h | 147 | 2354 | 1284 | 215 | 3455 | 0 | 58 | 585 | 258 | 58 | 585 | 279 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 63.0 | 17.0 | 17.1 | 35.8 | 22.5 | 0.0 | 93.0 | 77.3 | 68.1 | 93.8 | 77.1 | 72.0 |
| Incr Delay (d2), s/veh | 90.9 | 1.7 | 3.1 | 18.3 | 2.5 | 0.0 | 6.4 | 13.5 | 1.8 | 28.6 | 12.2 | 16.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 11.3 | 25.3 | 28.2 | 5.3 | 37.6 | 0.0 | 1.5 | 14.2 | 6.2 | 2.5 | 13.8 | 12.7 |
| LnGrp Delay(d),s/veh | 153.9 | 18.7 | 20.1 | 54.1 | 25.0 | 0.0 | 99.4 | 90.9 | 69.9 | 122.4 | 89.3 | 88.5 |
| LnGrp LOS | F | B | C | D | C | | F | F | E | F | F | F |
| Approach Vol, veh/h | | 2664 | | | 3004 | | | 664 | | | 766 | |
| Approach Delay, s/veh | | 27.1 | | | 26.2 | | | 87.1 | | | 90.8 | |
| Approach LOS | | C | | | C | | | F | | | F | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 16.0 | 136.0 | | 38.0 | 13.2 | 138.8 | | 38.0 | | | | |
| Change Period (Y+R _c), s | 6.8 | 6.9 | | * 6.6 | 6.8 | 6.9 | | * 6.6 | | | | |
| Max Green Setting (Gmax), s | 9.2 | 129.1 | | * 31 | 13.2 | 125.1 | | * 31 | | | | |
| Max Q Clear Time (g_c+l1), s | 11.2 | 81.3 | | 33.4 | 6.2 | 55.6 | | 33.4 | | | | |
| Green Ext Time (p_c), s | 0.0 | 39.7 | | 0.0 | 0.2 | 53.5 | | 0.0 | | | | |

Intersection Summary

| | |
|---------------------|------|
| HCM 2010 Ctrl Delay | 39.2 |
| HCM 2010 LOS | D |

Notes

Timings
5: SE 26th Rd & US 1/Brickell Ave

2016 Existing Conditions
P.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBT | WBR | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 309 | 774 | 14 | 428 | 205 | 713 | 457 | 224 | 815 | 38 |
| Future Volume (vph) | 309 | 774 | 14 | 428 | 205 | 713 | 457 | 224 | 815 | 38 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Free | Prot | NA | Perm |
| Protected Phases | 7 | 4 | | 8 | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | Free | | | 6 |
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 11.0 | 27.8 | 27.8 | 27.8 | 27.8 | 33.6 | | 11.0 | 33.6 | 33.6 |
| Total Split (s) | 20.0 | 63.0 | 63.0 | 43.0 | 43.0 | 45.0 | | 22.0 | 67.0 | 67.0 |
| Total Split (%) | 15.4% | 48.5% | 48.5% | 33.1% | 33.1% | 34.6% | | 16.9% | 51.5% | 51.5% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.8 | 2.8 | 2.8 | 2.8 | 2.6 | | 2.0 | 2.6 | 2.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.8 | 6.8 | 6.8 | 6.8 | 6.6 | | 6.0 | 6.6 | 6.6 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | | Yes | | |
| Recall Mode | None | Max | Max | None | None | C-Min | | None | C-Min | C-Min |

Intersection Summary

Cycle Length: 130

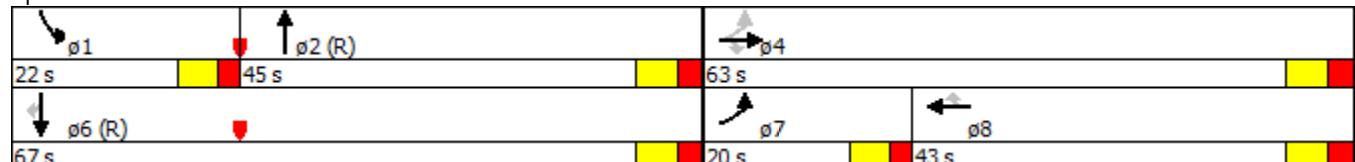
Actuated Cycle Length: 130

Offset: 96 (74%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Natural Cycle: 85

Control Type: Actuated-Coordinated

Splits and Phases: 5: SE 26th Rd & US 1/Brickell Ave



HCM 2010 Signalized Intersection Summary
5: SE 26th Rd & US 1/Brickell Ave

2016 Existing Conditions
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|-------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | | ↑↑ | ↑ | | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 309 | 774 | 14 | 0 | 428 | 205 | 0 | 713 | 457 | 224 | 815 | 38 |
| Future Volume (veh/h) | 309 | 774 | 14 | 0 | 428 | 205 | 0 | 713 | 457 | 224 | 815 | 38 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 0 | 1863 | 1863 | 0 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 322 | 806 | 0 | 0 | 446 | 0 | 0 | 743 | 0 | 233 | 849 | 0 |
| Adj No. of Lanes | 1 | 3 | 1 | 0 | 2 | 1 | 0 | 2 | 1 | 2 | 2 | 1 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 410 | 2198 | 684 | 0 | 986 | 441 | 0 | 1185 | 530 | 287 | 1644 | 736 |
| Arrive On Green | 0.11 | 0.43 | 0.00 | 0.00 | 0.28 | 0.00 | 0.00 | 0.33 | 0.00 | 0.08 | 0.46 | 0.00 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 0 | 3632 | 1583 | 0 | 3632 | 1583 | 3442 | 3539 | 1583 |
| Grp Volume(v), veh/h | 322 | 806 | 0 | 0 | 446 | 0 | 0 | 743 | 0 | 233 | 849 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 0 | 1770 | 1583 | 0 | 1770 | 1583 | 1721 | 1770 | 1583 |
| Q Serve(g_s), s | 14.0 | 13.9 | 0.0 | 0.0 | 13.5 | 0.0 | 0.0 | 23.0 | 0.0 | 8.7 | 22.0 | 0.0 |
| Cycle Q Clear(g_c), s | 14.0 | 13.9 | 0.0 | 0.0 | 13.5 | 0.0 | 0.0 | 23.0 | 0.0 | 8.7 | 22.0 | 0.0 |
| Prop In Lane | 1.00 | | | 1.00 | 0.00 | | 1.00 | 0.00 | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 410 | 2198 | 684 | 0 | 986 | 441 | 0 | 1185 | 530 | 287 | 1644 | 736 |
| V/C Ratio(X) | 0.78 | 0.37 | 0.00 | 0.00 | 0.45 | 0.00 | 0.00 | 0.63 | 0.00 | 0.81 | 0.52 | 0.00 |
| Avail Cap(c_a), veh/h | 410 | 2198 | 684 | 0 | 986 | 441 | 0 | 1185 | 530 | 424 | 1644 | 736 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 32.8 | 24.9 | 0.0 | 0.0 | 38.7 | 0.0 | 0.0 | 36.4 | 0.0 | 58.6 | 24.5 | 0.0 |
| Incr Delay (d2), s/veh | 8.9 | 0.5 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 2.5 | 0.0 | 4.4 | 1.2 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 5.0 | 6.6 | 0.0 | 0.0 | 6.7 | 0.0 | 0.0 | 11.7 | 0.0 | 4.3 | 11.0 | 0.0 |
| LnGrp Delay(d),s/veh | 41.6 | 25.4 | 0.0 | 0.0 | 39.0 | 0.0 | 0.0 | 38.9 | 0.0 | 63.0 | 25.7 | 0.0 |
| LnGrp LOS | D | C | | | D | | | D | | E | C | |
| Approach Vol, veh/h | 1128 | | | | 446 | | | 743 | | | 1082 | |
| Approach Delay, s/veh | 30.0 | | | | 39.0 | | | 38.9 | | | 33.7 | |
| Approach LOS | C | | | | D | | | D | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 16.9 | 50.1 | | 63.0 | | 67.0 | 20.0 | 43.0 | | | | |
| Change Period (Y+R _c), s | 6.0 | 6.6 | | * 6.8 | | 6.6 | 6.0 | * 6.8 | | | | |
| Max Green Setting (Gmax), s | 16.0 | 38.4 | | * 56 | | 60.4 | 14.0 | * 36 | | | | |
| Max Q Clear Time (g_c+l1), s | 10.7 | 25.0 | | 15.9 | | 24.0 | 16.0 | 15.5 | | | | |
| Green Ext Time (p_c), s | 0.2 | 4.2 | | 9.2 | | 5.2 | 0.0 | 7.6 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 34.3 | | | | | | | | |
| HCM 2010 LOS | | | | C | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings

1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2019 Future Background Conditions

P.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | SWL | SWT | SWR |
|----------------------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 457 | 465 | 498 | 144 | 501 | 40 | 1370 | 114 | 1867 | 655 |
| Future Volume (vph) | 457 | 465 | 498 | 144 | 501 | 40 | 1370 | 114 | 1867 | 655 |
| Turn Type | Split | NA | Free | Split | NA | Perm | NA | pm+pt | NA | pm+ov |
| Protected Phases | 8 | 8 | | 7 | 7 | | 6 | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | | 7 | | 2 | |
| Detector Phase | 8 | 8 | | 7 | 7 | 7 | 6 | 5 | 2 | 8 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 44.7 | 44.7 | | 15.9 | 15.9 | 15.9 | 40.7 | 11.8 | 40.7 | 44.7 |
| Total Split (s) | 48.0 | 48.0 | | 45.0 | 45.0 | 45.0 | 83.0 | 14.0 | 97.0 | 48.0 |
| Total Split (%) | 25.3% | 25.3% | | 23.7% | 23.7% | 23.7% | 43.7% | 7.4% | 51.1% | 25.3% |
| Yellow Time (s) | 4.8 | 4.8 | | 4.0 | 4.0 | 4.0 | 4.8 | 4.8 | 4.8 | 4.8 |
| All-Red Time (s) | 2.9 | 2.9 | | 4.1 | 4.1 | 4.1 | 2.9 | 2.0 | 2.9 | 2.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | 7.7 | 6.8 | 7.7 | 7.7 |
| Lead/Lag | Lag | Lag | | Lead | Lead | Lead | Lag | Lead | | Lag |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | | Yes |
| Recall Mode | None | None | | None | None | None | C-Min | None | C-Min | None |

Intersection Summary

Cycle Length: 190

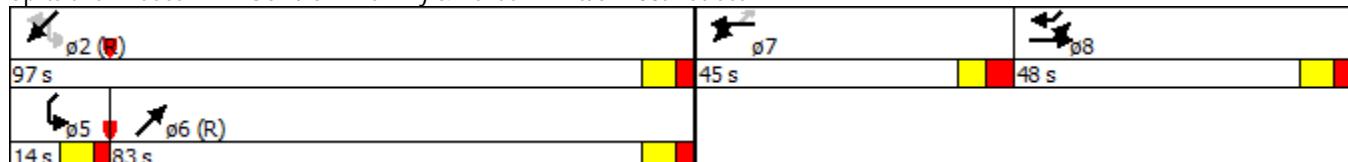
Actuated Cycle Length: 190

Offset: 116 (61%), Referenced to phase 2:SWTL and 6:NET, Start of Green

Natural Cycle: 135

Control Type: Actuated-Coordinated

Splits and Phases: 1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street



HCM Signalized Intersection Capacity Analysis
1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2019 Future Background Conditions

P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|------------------------|-------|------|-------|-------|-------|------|------|------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 457 | 465 | 498 | 144 | 501 | 40 | 0 | 1370 | 127 | 114 | 1867 | 655 |
| Future Volume (vph) | 457 | 465 | 498 | 144 | 501 | 40 | 0 | 1370 | 127 | 114 | 1867 | 655 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.7 | 7.7 | 4.0 | 8.1 | 8.1 | 8.1 | | 7.7 | | 6.8 | 7.7 | 7.7 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | | 1.00 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1610 | 3348 | 1563 | 1770 | 3539 | 1583 | | 5014 | | 1770 | 5085 | 1568 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.05 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1610 | 3348 | 1563 | 1770 | 3539 | 1583 | | 5014 | | 97 | 5085 | 1568 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 466 | 474 | 508 | 147 | 511 | 41 | 0 | 1398 | 130 | 116 | 1905 | 668 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 6 | 0 | 0 | 0 | 9 |
| Lane Group Flow (vph) | 308 | 632 | 508 | 147 | 511 | 7 | 0 | 1522 | 0 | 116 | 1905 | 659 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | 1 | | 2 | 2 | | 1 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | 4 |
| Turn Type | Split | NA | Free | Split | NA | Perm | | NA | pm+pt | NA | pm+ov | |
| Protected Phases | 8 | 8 | | 7 | 7 | | 6 | | 5 | 2 | | 8 |
| Permitted Phases | | | Free | | | 7 | | | 2 | | | 2 |
| Actuated Green, G (s) | 44.9 | 44.9 | 190.0 | 34.6 | 34.6 | 34.6 | | 70.1 | 87.0 | 87.0 | | 131.9 |
| Effective Green, g (s) | 44.9 | 44.9 | 190.0 | 34.6 | 34.6 | 34.6 | | 70.1 | 87.0 | 87.0 | | 131.9 |
| Actuated g/C Ratio | 0.24 | 0.24 | 1.00 | 0.18 | 0.18 | 0.18 | | 0.37 | 0.46 | 0.46 | | 0.69 |
| Clearance Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | | 7.7 | 6.8 | 7.7 | | 7.7 |
| Vehicle Extension (s) | 3.5 | 3.5 | | 4.0 | 4.0 | 4.0 | | 1.0 | 2.0 | 1.0 | | 3.5 |
| Lane Grp Cap (vph) | 380 | 791 | 1563 | 322 | 644 | 288 | | 1849 | | 133 | 2328 | 1152 |
| v/s Ratio Prot | c0.19 | 0.19 | | 0.08 | c0.14 | | 0.30 | | 0.05 | c0.37 | | 0.14 |
| v/s Ratio Perm | | | 0.33 | | | 0.00 | | | c0.35 | | | 0.28 |
| v/c Ratio | 0.81 | 0.80 | 0.33 | 0.46 | 0.79 | 0.03 | | 0.82 | 0.87 | 0.82 | | 0.57 |
| Uniform Delay, d1 | 68.5 | 68.3 | 0.0 | 69.3 | 74.3 | 63.9 | | 54.3 | 48.8 | 44.6 | | 14.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 |
| Incremental Delay, d2 | 12.6 | 5.8 | 0.6 | 1.4 | 7.0 | 0.0 | | 4.3 | 41.2 | 3.3 | | 0.7 |
| Delay (s) | 81.2 | 74.1 | 0.6 | 70.7 | 81.3 | 63.9 | | 58.6 | 90.0 | 48.0 | | 15.5 |
| Level of Service | F | E | A | E | F | E | | E | | F | D | B |
| Approach Delay (s) | | 49.8 | | | 78.1 | | | 58.6 | | | 41.7 | |
| Approach LOS | | D | | | E | | | E | | | D | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 51.6 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.87 | | |
| Actuated Cycle Length (s) | 190.0 | Sum of lost time (s) | |
| Intersection Capacity Utilization | 92.7% | ICU Level of Service | 30.3 |
| Analysis Period (min) | 15 | | F |
| c Critical Lane Group | | | |

Timings

2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2019 Future Background Conditions

P.M. Peak Hour

| Lane Group | EBT | EBR | WBT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ |
| Traffic Volume (vph) | 526 | 85 | 475 | 130 | 2040 | 50 | 2673 |
| Future Volume (vph) | 526 | 85 | 475 | 130 | 2040 | 50 | 2673 |
| Turn Type | NA | Perm | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 8 | | 4 | 1 | 6 | 5 | 2 |
| Permitted Phases | | | | 6 | | 2 | |
| Detector Phase | 8 | 8 | 4 | 1 | 6 | 5 | 2 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 12.0 | 12.0 | 12.0 | 5.0 | 7.0 | 5.0 | 7.0 |
| Minimum Split (s) | 34.9 | 34.9 | 34.9 | 11.4 | 37.0 | 11.4 | 37.0 |
| Total Split (s) | 43.6 | 43.6 | 43.6 | 11.4 | 133.0 | 13.4 | 135.0 |
| Total Split (%) | 22.9% | 22.9% | 22.9% | 6.0% | 70.0% | 7.1% | 71.1% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.4 | 4.4 | 4.4 | 4.4 |
| All-Red Time (s) | 4.9 | 4.9 | 4.9 | 2.0 | 3.6 | 2.0 | 3.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.9 | 8.9 | 8.9 | 6.4 | 8.0 | 6.4 | 8.0 |
| Lead/Lag | | | | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | C-Min | None | C-Min |

Intersection Summary

Cycle Length: 190

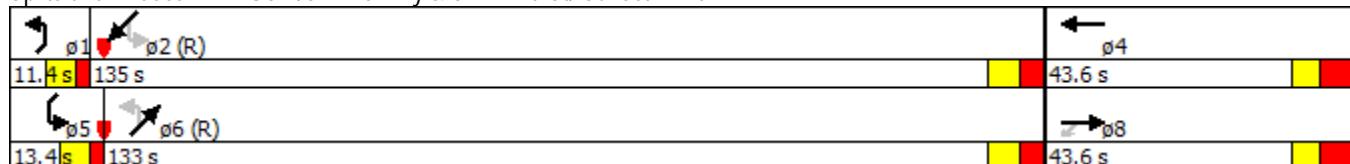
Actuated Cycle Length: 190

Offset: 161 (85%), Referenced to phase 2:SWTL and 6:NETL, Start of Green

Natural Cycle: 145

Control Type: Actuated-Coordinated

Splits and Phases: 2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive



HCM 2010 Signalized Intersection Summary
2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2019 Future Background Conditions
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|---------------------------------------|------|-------|------|-------|------|-------|-------|-------|------|------|------|------|
| Lane Configurations | | ↑↑ | ↑ | | ↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | |
| Traffic Volume (veh/h) | 0 | 526 | 85 | 0 | 475 | 9 | 130 | 2040 | 90 | 50 | 2673 | 255 |
| Future Volume (veh/h) | 0 | 526 | 85 | 0 | 475 | 9 | 130 | 2040 | 90 | 50 | 2673 | 255 |
| Number | 3 | 8 | 18 | 7 | 4 | 14 | 1 | 6 | 16 | 5 | 2 | 12 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 0.90 | 1.00 | | 0.98 | 1.00 | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1863 | 1863 | 0 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 0 | 542 | 0 | 0 | 490 | 9 | 134 | 2103 | 93 | 52 | 2756 | 263 |
| Adj No. of Lanes | 0 | 2 | 1 | 0 | 2 | 0 | 1 | 3 | 0 | 1 | 3 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 0 | 612 | 274 | 0 | 613 | 11 | 99 | 3392 | 149 | 160 | 3208 | 296 |
| Arrive On Green | 0.00 | 0.17 | 0.00 | 0.00 | 0.17 | 0.17 | 0.03 | 0.68 | 0.68 | 0.02 | 0.68 | 0.68 |
| Sat Flow, veh/h | 0 | 3632 | 1583 | 0 | 3641 | 65 | 1774 | 4990 | 220 | 1774 | 4730 | 436 |
| Grp Volume(v), veh/h | 0 | 542 | 0 | 0 | 244 | 255 | 134 | 1426 | 770 | 52 | 1948 | 1071 |
| Grp Sat Flow(s),veh/h/ln | 0 | 1770 | 1583 | 0 | 1770 | 1843 | 1774 | 1695 | 1819 | 1774 | 1695 | 1776 |
| Q Serve(g_s), s | 0.0 | 28.4 | 0.0 | 0.0 | 25.1 | 25.2 | 5.0 | 44.2 | 44.6 | 1.7 | 82.6 | 92.8 |
| Cycle Q Clear(g_c), s | 0.0 | 28.4 | 0.0 | 0.0 | 25.1 | 25.2 | 5.0 | 44.2 | 44.6 | 1.7 | 82.6 | 92.8 |
| Prop In Lane | 0.00 | | 1.00 | 0.00 | | 0.04 | 1.00 | | 0.12 | 1.00 | | 0.25 |
| Lane Grp Cap(c), veh/h | 0 | 612 | 274 | 0 | 306 | 319 | 99 | 2305 | 1237 | 160 | 2299 | 1205 |
| V/C Ratio(X) | 0.00 | 0.89 | 0.00 | 0.00 | 0.80 | 0.80 | 1.35 | 0.62 | 0.62 | 0.32 | 0.85 | 0.89 |
| Avail Cap(c_a), veh/h | 0 | 646 | 289 | 0 | 323 | 337 | 99 | 2305 | 1237 | 182 | 2299 | 1205 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 76.7 | 0.0 | 0.0 | 75.4 | 75.4 | 58.7 | 16.8 | 16.9 | 16.0 | 23.1 | 24.8 |
| Incr Delay (d2), s/veh | 0.0 | 13.5 | 0.0 | 0.0 | 12.6 | 12.3 | 209.7 | 1.3 | 2.4 | 0.4 | 4.1 | 10.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.0 | 15.1 | 0.0 | 0.0 | 13.4 | 14.0 | 11.0 | 21.0 | 23.1 | 0.9 | 39.7 | 48.5 |
| LnGrp Delay(d),s/veh | 0.0 | 90.2 | 0.0 | 0.0 | 88.0 | 87.7 | 268.5 | 18.1 | 19.2 | 16.4 | 27.2 | 34.7 |
| LnGrp LOS | | F | | | F | F | B | B | B | C | C | |
| Approach Vol, veh/h | | 542 | | | 499 | | | 2330 | | | 3071 | |
| Approach Delay, s/veh | | 90.2 | | | 87.8 | | | 32.9 | | | 29.7 | |
| Approach LOS | | F | | | F | | | C | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 11.4 | 136.8 | | 41.8 | 11.1 | 137.2 | | 41.8 | | | | |
| Change Period (Y+R _c), s | 6.4 | 8.0 | | * 8.9 | 6.4 | 8.0 | | * 8.9 | | | | |
| Max Green Setting (Gmax), s | 5.0 | 127.0 | | * 35 | 7.0 | 125.0 | | * 35 | | | | |
| Max Q Clear Time (g_c+l1), s | 7.0 | 94.8 | | 27.2 | 3.7 | 46.6 | | 30.4 | | | | |
| Green Ext Time (p_c), s | 0.0 | 27.0 | | 3.8 | 0.0 | 52.5 | | 2.4 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 40.4 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings

3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2019 Future Background Conditions

P.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | NER | SWT | SWR | ø1 | ø2 |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|------|--------|------|-------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | | |
| Traffic Volume (vph) | 373 | 138 | 20 | 175 | 319 | 3 | 2345 | 203 | 2127 | 630 | | |
| Future Volume (vph) | 373 | 138 | 20 | 175 | 319 | 3 | 2345 | 203 | 2127 | 630 | | |
| Turn Type | Split | NA | Perm | Split | NA | Perm | NA | Prot | NA | custom | | |
| Protected Phases | 3 | 3 | | 4 | 4 | | 6 | 6 | 12 | 23 | 1 | 2 |
| Permitted Phases | | | | 3 | | 4 | | | | | | |
| Detector Phase | 3 | 3 | 3 | 4 | 4 | 4 | 6 | 6 | 12 | 23 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 15.0 | 15.0 | | | 1.0 | 15.0 |
| Minimum Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 25.5 | 25.5 | | | 25.0 | 32.5 |
| Total Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 138.0 | 138.0 | | | 25.0 | 113.0 |
| Total Split (%) | 13.7% | 13.7% | 13.7% | 13.7% | 13.7% | 13.7% | 72.6% | 72.6% | | | 13% | 59% |
| Yellow Time (s) | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.8 | 4.8 | | | 2.0 | 4.8 |
| All-Red Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.7 | 2.7 | | | 0.0 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 7.5 | 7.5 | | | | |
| Lead/Lag | Lead | Lead | Lead | Lag | Lag | Lag | | | | | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | | | | | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C-Min | C-Min | | | Max | C-Min |

Intersection Summary

Cycle Length: 190

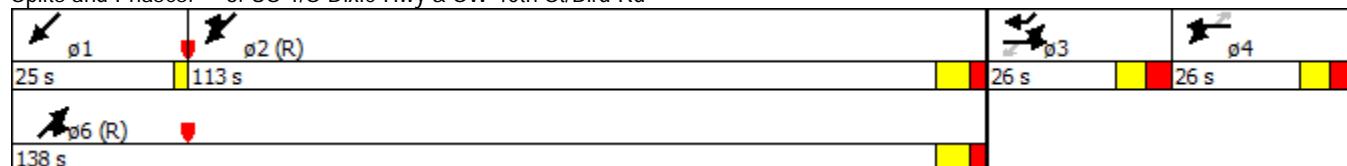
Actuated Cycle Length: 190

Offset: 136 (72%), Referenced to phase 2:SWT and 6:NET, Start of Green

Natural Cycle: 110

Control Type: Actuated-Coordinated

Splits and Phases: 3: US 1/S Dixie Hwy & SW 40th St/Bird Rd



HCM Signalized Intersection Capacity Analysis
3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2019 Future Background Conditions
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|-----------------------------------|-------|-------|-------|-------|-------|------|---------------------------|-------|-------|------|-------|--------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | ↑ | | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 373 | 138 | 20 | 175 | 319 | 3 | 0 | 2345 | 203 | 0 | 2127 | 630 |
| Future Volume (vph) | 373 | 138 | 20 | 175 | 319 | 3 | 0 | 2345 | 203 | 0 | 2127 | 630 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | 7.5 | 7.5 | | 2.0 | 7.5 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | 1.00 | | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (prot) | 3221 | 1677 | 1522 | 1770 | 3539 | 1583 | | 5085 | 1583 | | 5085 | 1583 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (perm) | 3221 | 1677 | 1522 | 1770 | 3539 | 1583 | | 5085 | 1583 | | 5085 | 1583 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 393 | 145 | 21 | 184 | 336 | 3 | 0 | 2468 | 214 | 0 | 2239 | 663 |
| RTOR Reduction (vph) | 0 | 0 | 19 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 354 | 184 | 2 | 184 | 336 | 0 | 0 | 2468 | 214 | 0 | 2239 | 663 |
| Confl. Peds. (#/hr) | | | 5 | 5 | | | 7 | | | | | 7 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | | | | 6 |
| Turn Type | Split | NA | Perm | Split | NA | Perm | | NA | Prot | | NA | custom |
| Protected Phases | 3 | 3 | | 4 | 4 | | | 6 | 6 | | 12 | 23 |
| Permitted Phases | | | 3 | | | 4 | | | | | | |
| Actuated Green, G (s) | 22.5 | 22.5 | 22.5 | 20.8 | 20.8 | 20.8 | | 123.2 | 123.2 | | 123.2 | 127.4 |
| Effective Green, g (s) | 22.5 | 22.5 | 22.5 | 20.8 | 20.8 | 20.8 | | 123.2 | 123.2 | | 123.2 | 127.4 |
| Actuated g/C Ratio | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 | 0.11 | | 0.65 | 0.65 | | 0.65 | 0.67 |
| Clearance Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | 7.5 | 7.5 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | | 1.0 | 1.0 | | | |
| Lane Grp Cap (vph) | 381 | 198 | 180 | 193 | 387 | 173 | | 3297 | 1026 | | 3297 | 1061 |
| v/s Ratio Prot | c0.11 | 0.11 | | c0.10 | 0.09 | | | c0.49 | 0.14 | | 0.44 | 0.42 |
| v/s Ratio Perm | | | 0.00 | | | 0.00 | | | | | | |
| v/c Ratio | 0.93 | 0.93 | 0.01 | 0.95 | 0.87 | 0.00 | | 0.75 | 0.21 | | 0.68 | 0.62 |
| Uniform Delay, d1 | 83.0 | 83.0 | 74.0 | 84.1 | 83.3 | 75.4 | | 22.8 | 13.6 | | 21.0 | 17.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 28.5 | 43.8 | 0.0 | 51.1 | 18.0 | 0.0 | | 1.6 | 0.5 | | 1.1 | 1.2 |
| Delay (s) | 111.5 | 126.8 | 74.0 | 135.2 | 101.3 | 75.4 | | 24.4 | 14.0 | | 22.1 | 18.9 |
| Level of Service | F | F | E | F | F | E | | C | B | | C | B |
| Approach Delay (s) | | 115.1 | | | 113.1 | | | 23.6 | | | 21.4 | |
| Approach LOS | | F | | | F | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 37.3 | | | | HCM 2000 Level of Service | | D | | | |
| HCM 2000 Volume to Capacity ratio | | | 0.81 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 190.0 | | | | Sum of lost time (s) | | 25.5 | | | |
| Intersection Capacity Utilization | | | 84.0% | | | | ICU Level of Service | | E | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Timings

4: SW 27th Ave & US 1/S Dixie Hwy

2019 Future Background Conditions

P.M. Peak Hour

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↓ | ↑ | ↑↑↓ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 158 | 2512 | 129 | 2920 | 26 | 517 | 131 | 40 | 509 | 229 |
| Future Volume (vph) | 158 | 2512 | 129 | 2920 | 26 | 517 | 131 | 40 | 509 | 229 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | NA | pm+ov | Perm | NA | pm+ov |
| Protected Phases | 1 | 6 | 5 | 2 | | 4 | 5 | | 8 | 1 |
| Permitted Phases | 6 | | 2 | | 4 | | 4 | 8 | | 8 |
| Detector Phase | 1 | 6 | 5 | 2 | 4 | 4 | 5 | 8 | 8 | 1 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 5.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 | 5.0 |
| Minimum Split (s) | 9.5 | 39.9 | 9.5 | 39.9 | 29.6 | 29.6 | 9.5 | 29.6 | 29.6 | 9.5 |
| Total Split (s) | 16.0 | 132.0 | 20.0 | 136.0 | 38.0 | 38.0 | 20.0 | 38.0 | 38.0 | 16.0 |
| Total Split (%) | 8.4% | 69.5% | 10.5% | 71.6% | 20.0% | 20.0% | 10.5% | 20.0% | 20.0% | 8.4% |
| Yellow Time (s) | 3.5 | 4.8 | 3.5 | 4.8 | 4.4 | 4.4 | 3.5 | 4.4 | 4.4 | 3.5 |
| All-Red Time (s) | 1.0 | 2.1 | 1.0 | 2.1 | 2.2 | 2.2 | 1.0 | 2.2 | 2.2 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 6.9 | 4.5 | 6.9 | 6.6 | 6.6 | 4.5 | 6.6 | 6.6 | 4.5 |
| Lead/Lag | Lead | Lag | Lead | Lag | | | | Lead | | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | Yes | | Yes |
| Recall Mode | None | C-Min | None | C-Min | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 190

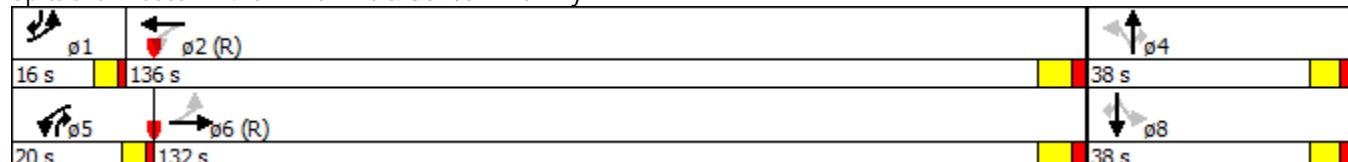
Actuated Cycle Length: 190

Offset: 75 (39%), Referenced to phase 2:WBTL and 6:EBTL, Start of Green

Natural Cycle: 120

Control Type: Actuated-Coordinated

Splits and Phases: 4: SW 27th Ave & US 1/S Dixie Hwy



HCM 2010 Signalized Intersection Summary
4: SW 27th Ave & US 1/S Dixie Hwy

2019 Future Background Conditions
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|-------|-------|------|-------|------|-------|-------|-------|------|-------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 158 | 2512 | 33 | 129 | 2920 | 98 | 26 | 517 | 131 | 40 | 509 | 229 |
| Future Volume (veh/h) | 158 | 2512 | 33 | 129 | 2920 | 98 | 26 | 517 | 131 | 40 | 509 | 229 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.98 | 1.00 | | 1.00 | 1.00 | | 0.78 | 1.00 | | 0.77 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 158 | 2512 | 33 | 129 | 2920 | 0 | 26 | 517 | 131 | 40 | 509 | 229 |
| Adj No. of Lanes | 1 | 3 | 0 | 1 | 3 | 0 | 1 | 2 | 1 | 1 | 2 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 166 | 3651 | 48 | 152 | 3455 | 0 | 56 | 585 | 258 | 55 | 585 | 298 |
| Arrive On Green | 0.06 | 0.71 | 0.71 | 0.03 | 0.68 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 1774 | 5172 | 68 | 1774 | 5253 | 0 | 717 | 3539 | 1238 | 780 | 3539 | 1225 |
| Grp Volume(v), veh/h | 158 | 1644 | 901 | 129 | 2920 | 0 | 26 | 517 | 131 | 40 | 509 | 229 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1849 | 1774 | 1695 | 0 | 717 | 1770 | 1238 | 780 | 1770 | 1225 |
| Q Serve(g_s), s | 10.5 | 52.6 | 53.0 | 4.3 | 82.1 | 0.0 | 4.8 | 27.1 | 18.0 | 4.3 | 26.6 | 31.4 |
| Cycle Q Clear(g_c), s | 10.5 | 52.6 | 53.0 | 4.3 | 82.1 | 0.0 | 31.4 | 27.1 | 18.0 | 31.4 | 26.6 | 31.4 |
| Prop In Lane | 1.00 | | 0.04 | 1.00 | | 0.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 166 | 2393 | 1306 | 152 | 3455 | 0 | 56 | 585 | 258 | 55 | 585 | 298 |
| V/C Ratio(X) | 0.95 | 0.69 | 0.69 | 0.85 | 0.85 | 0.00 | 0.47 | 0.88 | 0.51 | 0.72 | 0.87 | 0.77 |
| Avail Cap(c_a), veh/h | 166 | 2393 | 1306 | 236 | 3455 | 0 | 56 | 585 | 258 | 55 | 585 | 298 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 65.9 | 15.9 | 16.0 | 35.5 | 22.9 | 0.0 | 93.4 | 77.5 | 68.1 | 94.1 | 77.3 | 70.0 |
| Incr Delay (d2), s/veh | 54.8 | 1.6 | 3.0 | 15.9 | 2.7 | 0.0 | 7.1 | 15.1 | 1.9 | 38.0 | 13.5 | 11.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 10.6 | 25.0 | 28.1 | 5.3 | 39.0 | 0.0 | 1.5 | 14.5 | 6.3 | 2.7 | 14.2 | 12.4 |
| LnGrp Delay(d),s/veh | 120.7 | 17.6 | 19.0 | 51.4 | 25.7 | 0.0 | 100.5 | 92.6 | 70.0 | 132.1 | 90.9 | 81.8 |
| LnGrp LOS | F | B | B | D | C | | F | F | E | F | F | F |
| Approach Vol, veh/h | | 2703 | | | 3049 | | | 674 | | | 778 | |
| Approach Delay, s/veh | | 24.1 | | | 26.7 | | | 88.5 | | | 90.3 | |
| Approach LOS | | C | | | C | | | F | | | F | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 16.0 | 136.0 | | 38.0 | 11.0 | 141.0 | | 38.0 | | | | |
| Change Period (Y+R _c), s | 4.5 | 6.9 | | * 6.6 | 4.5 | 6.9 | | * 6.6 | | | | |
| Max Green Setting (Gmax), s | 11.5 | 129.1 | | * 31 | 15.5 | 125.1 | | * 31 | | | | |
| Max Q Clear Time (g_c+l1), s | 12.5 | 84.1 | | 33.4 | 6.3 | 55.0 | | 33.4 | | | | |
| Green Ext Time (p_c), s | 0.0 | 38.3 | | 0.0 | 0.2 | 54.9 | | 0.0 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 38.4 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings
5: SE 26th Rd & US 1/Brickell Ave

2019 Future Background Conditions

P.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBT | WBR | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 314 | 786 | 14 | 434 | 208 | 724 | 464 | 227 | 827 | 39 |
| Future Volume (vph) | 314 | 786 | 14 | 434 | 208 | 724 | 464 | 227 | 827 | 39 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Free | Prot | NA | Perm |
| Protected Phases | 7 | 4 | | 8 | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | Free | | | 6 |
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 11.0 | 27.8 | 27.8 | 27.8 | 27.8 | 33.6 | | 11.0 | 33.6 | 33.6 |
| Total Split (s) | 20.0 | 63.0 | 63.0 | 43.0 | 43.0 | 45.0 | | 22.0 | 67.0 | 67.0 |
| Total Split (%) | 15.4% | 48.5% | 48.5% | 33.1% | 33.1% | 34.6% | | 16.9% | 51.5% | 51.5% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.8 | 2.8 | 2.8 | 2.8 | 2.6 | | 2.0 | 2.6 | 2.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.8 | 6.8 | 6.8 | 6.8 | 6.6 | | 6.0 | 6.6 | 6.6 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | | Yes | | |
| Recall Mode | None | Max | Max | None | None | C-Min | | None | C-Min | C-Min |

Intersection Summary

Cycle Length: 130

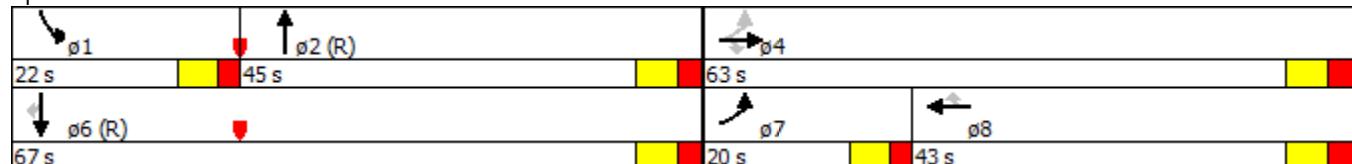
Actuated Cycle Length: 130

Offset: 96 (74%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Natural Cycle: 85

Control Type: Actuated-Coordinated

Splits and Phases: 5: SE 26th Rd & US 1/Brickell Ave



HCM 2010 Signalized Intersection Summary
5: SE 26th Rd & US 1/Brickell Ave

2019 Future Background Conditions
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|-------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | | ↑↑ | ↑ | | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 314 | 786 | 14 | 0 | 434 | 208 | 0 | 724 | 464 | 227 | 827 | 39 |
| Future Volume (veh/h) | 314 | 786 | 14 | 0 | 434 | 208 | 0 | 724 | 464 | 227 | 827 | 39 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 0 | 1863 | 1863 | 0 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 327 | 819 | 0 | 0 | 452 | 0 | 0 | 754 | 0 | 236 | 861 | 0 |
| Adj No. of Lanes | 1 | 3 | 1 | 0 | 2 | 1 | 0 | 2 | 1 | 2 | 2 | 1 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 408 | 2198 | 684 | 0 | 986 | 441 | 0 | 1182 | 529 | 290 | 1644 | 736 |
| Arrive On Green | 0.11 | 0.43 | 0.00 | 0.00 | 0.28 | 0.00 | 0.00 | 0.33 | 0.00 | 0.08 | 0.46 | 0.00 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 0 | 3632 | 1583 | 0 | 3632 | 1583 | 3442 | 3539 | 1583 |
| Grp Volume(v), veh/h | 327 | 819 | 0 | 0 | 452 | 0 | 0 | 754 | 0 | 236 | 861 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 0 | 1770 | 1583 | 0 | 1770 | 1583 | 1721 | 1770 | 1583 |
| Q Serve(g_s), s | 14.0 | 14.2 | 0.0 | 0.0 | 13.7 | 0.0 | 0.0 | 23.4 | 0.0 | 8.8 | 22.4 | 0.0 |
| Cycle Q Clear(g_c), s | 14.0 | 14.2 | 0.0 | 0.0 | 13.7 | 0.0 | 0.0 | 23.4 | 0.0 | 8.8 | 22.4 | 0.0 |
| Prop In Lane | 1.00 | | | 1.00 | 0.00 | | 1.00 | 0.00 | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 408 | 2198 | 684 | 0 | 986 | 441 | 0 | 1182 | 529 | 290 | 1644 | 736 |
| V/C Ratio(X) | 0.80 | 0.37 | 0.00 | 0.00 | 0.46 | 0.00 | 0.00 | 0.64 | 0.00 | 0.81 | 0.52 | 0.00 |
| Avail Cap(c_a), veh/h | 408 | 2198 | 684 | 0 | 986 | 441 | 0 | 1182 | 529 | 424 | 1644 | 736 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 33.3 | 25.0 | 0.0 | 0.0 | 38.8 | 0.0 | 0.0 | 36.6 | 0.0 | 58.5 | 24.6 | 0.0 |
| Incr Delay (d2), s/veh | 10.2 | 0.5 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 2.6 | 0.0 | 4.7 | 1.2 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 5.5 | 6.7 | 0.0 | 0.0 | 6.8 | 0.0 | 0.0 | 11.8 | 0.0 | 4.4 | 11.2 | 0.0 |
| LnGrp Delay(d),s/veh | 43.4 | 25.5 | 0.0 | 0.0 | 39.0 | 0.0 | 0.0 | 39.3 | 0.0 | 63.2 | 25.8 | 0.0 |
| LnGrp LOS | D | C | | | D | | | D | | E | C | |
| Approach Vol, veh/h | 1146 | | | | 452 | | | 754 | | | 1097 | |
| Approach Delay, s/veh | 30.6 | | | | 39.0 | | | 39.3 | | | 33.9 | |
| Approach LOS | C | | | | D | | | D | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 17.0 | 50.0 | | 63.0 | | 67.0 | 20.0 | 43.0 | | | | |
| Change Period (Y+R _c), s | 6.0 | 6.6 | | * 6.8 | | 6.6 | 6.0 | * 6.8 | | | | |
| Max Green Setting (Gmax), s | 16.0 | 38.4 | | * 56 | | 60.4 | 14.0 | * 36 | | | | |
| Max Q Clear Time (g_c+l1), s | 10.8 | 25.4 | | 16.2 | | 24.4 | 16.0 | 15.7 | | | | |
| Green Ext Time (p_c), s | 0.2 | 4.3 | | 9.4 | | 5.3 | 0.0 | 7.7 | | | | |

Intersection Summary

| | |
|---------------------|------|
| HCM 2010 Ctrl Delay | 34.6 |
| HCM 2010 LOS | C |

Notes

Timings
1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2019 Future Total
P.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | SWL | SWT | SWR |
|----------------------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 457 | 465 | 498 | 144 | 501 | 40 | 1350 | 114 | 1839 | 655 |
| Future Volume (vph) | 457 | 465 | 498 | 144 | 501 | 40 | 1350 | 114 | 1839 | 655 |
| Turn Type | Split | NA | Free | Split | NA | Perm | NA | pm+pt | NA | pm+ov |
| Protected Phases | 8 | 8 | | 7 | 7 | | 6 | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | | 7 | | 2 | |
| Detector Phase | 8 | 8 | | 7 | 7 | 7 | 6 | 5 | 2 | 8 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 44.7 | 44.7 | | 15.9 | 15.9 | 15.9 | 40.7 | 11.8 | 40.7 | 44.7 |
| Total Split (s) | 48.0 | 48.0 | | 45.0 | 45.0 | 45.0 | 83.0 | 14.0 | 97.0 | 48.0 |
| Total Split (%) | 25.3% | 25.3% | | 23.7% | 23.7% | 23.7% | 43.7% | 7.4% | 51.1% | 25.3% |
| Yellow Time (s) | 4.8 | 4.8 | | 4.0 | 4.0 | 4.0 | 4.8 | 4.8 | 4.8 | 4.8 |
| All-Red Time (s) | 2.9 | 2.9 | | 4.1 | 4.1 | 4.1 | 2.9 | 2.0 | 2.9 | 2.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | 7.7 | 6.8 | 7.7 | 7.7 |
| Lead/Lag | Lag | Lag | | Lead | Lead | Lead | Lag | Lead | | Lag |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | | Yes |
| Recall Mode | None | None | | None | None | None | C-Min | None | C-Min | None |

Intersection Summary

Cycle Length: 190

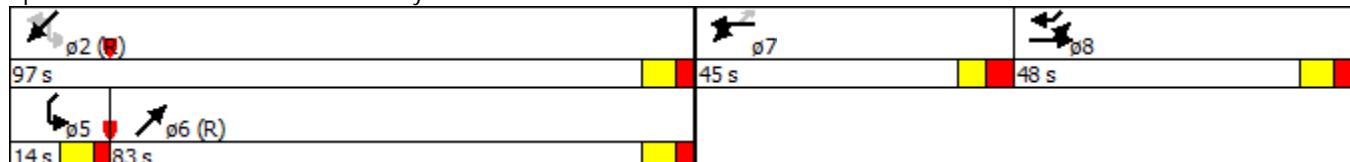
Actuated Cycle Length: 190

Offset: 116 (61%), Referenced to phase 2:SWTL and 6:NET, Start of Green

Natural Cycle: 135

Control Type: Actuated-Coordinated

Splits and Phases: 1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street



HCM Signalized Intersection Capacity Analysis
1: US 1/ S Dixie Hwy & Kendall Drive/SW 88th Street

2019 Future Total
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|------------------------|-------|------|-------|-------|-------|------|------|------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | | ↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 457 | 465 | 498 | 144 | 501 | 40 | 0 | 1350 | 127 | 114 | 1839 | 655 |
| Future Volume (vph) | 457 | 465 | 498 | 144 | 501 | 40 | 0 | 1350 | 127 | 114 | 1839 | 655 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.7 | 7.7 | 4.0 | 8.1 | 8.1 | 8.1 | | 7.7 | | 6.8 | 7.7 | 7.7 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | | 1.00 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1610 | 3348 | 1563 | 1770 | 3539 | 1583 | | 5013 | | 1770 | 5085 | 1568 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | | 0.05 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1610 | 3348 | 1563 | 1770 | 3539 | 1583 | | 5013 | | 97 | 5085 | 1568 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 466 | 474 | 508 | 147 | 511 | 41 | 0 | 1378 | 130 | 116 | 1877 | 668 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 6 | 0 | 0 | 0 | 9 |
| Lane Group Flow (vph) | 308 | 632 | 508 | 147 | 511 | 7 | 0 | 1502 | 0 | 116 | 1877 | 659 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | 1 | | 2 | 2 | | 1 |
| Confl. Bikes (#/hr) | | | | 1 | | | | | | | | 4 |
| Turn Type | Split | NA | Free | Split | NA | Perm | | NA | pm+pt | NA | pm+ov | |
| Protected Phases | 8 | 8 | | 7 | 7 | | | 6 | | 5 | 2 | 8 |
| Permitted Phases | | | Free | | | 7 | | | | 2 | | 2 |
| Actuated Green, G (s) | 45.3 | 45.3 | 190.0 | 34.7 | 34.7 | 34.7 | | 69.8 | | 86.5 | 86.5 | 131.8 |
| Effective Green, g (s) | 45.3 | 45.3 | 190.0 | 34.7 | 34.7 | 34.7 | | 69.8 | | 86.5 | 86.5 | 131.8 |
| Actuated g/C Ratio | 0.24 | 0.24 | 1.00 | 0.18 | 0.18 | 0.18 | | 0.37 | | 0.46 | 0.46 | 0.69 |
| Clearance Time (s) | 7.7 | 7.7 | | 8.1 | 8.1 | 8.1 | | 7.7 | | 6.8 | 7.7 | 7.7 |
| Vehicle Extension (s) | 3.5 | 3.5 | | 4.0 | 4.0 | 4.0 | | 1.0 | | 2.0 | 1.0 | 3.5 |
| Lane Grp Cap (vph) | 383 | 798 | 1563 | 323 | 646 | 289 | | 1841 | | 131 | 2315 | 1151 |
| v/s Ratio Prot | c0.19 | 0.19 | | 0.08 | c0.14 | | | 0.30 | | 0.05 | c0.37 | 0.14 |
| v/s Ratio Perm | | | 0.33 | | | 0.00 | | | | c0.36 | | 0.28 |
| v/c Ratio | 0.80 | 0.79 | 0.33 | 0.46 | 0.79 | 0.03 | | 0.82 | | 0.89 | 0.81 | 0.57 |
| Uniform Delay, d1 | 68.2 | 67.9 | 0.0 | 69.2 | 74.2 | 63.8 | | 54.3 | | 48.7 | 44.7 | 14.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 11.9 | 5.6 | 0.6 | 1.4 | 6.9 | 0.0 | | 4.1 | | 44.6 | 3.2 | 0.7 |
| Delay (s) | 80.1 | 73.5 | 0.6 | 70.6 | 81.1 | 63.8 | | 58.4 | | 93.4 | 47.9 | 15.5 |
| Level of Service | F | E | A | E | F | E | | E | | F | D | B |
| Approach Delay (s) | | 49.3 | | | 77.9 | | | 58.4 | | | 41.8 | |
| Approach LOS | | D | | | E | | | E | | | D | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 51.5 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.87 | | |
| Actuated Cycle Length (s) | 190.0 | Sum of lost time (s) | |
| Intersection Capacity Utilization | 92.3% | ICU Level of Service | 30.3 |
| Analysis Period (min) | 15 | | F |
| c Critical Lane Group | | | |

Timings
2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2019 Future Total
P.M. Peak Hour

| Lane Group | EBT | EBR | WBT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑↑ |
| Traffic Volume (vph) | 523 | 85 | 474 | 130 | 2017 | 50 | 2643 |
| Future Volume (vph) | 523 | 85 | 474 | 130 | 2017 | 50 | 2643 |
| Turn Type | NA | Perm | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 8 | | 4 | 1 | 6 | 5 | 2 |
| Permitted Phases | | | | 6 | | 2 | |
| Detector Phase | 8 | 8 | 4 | 1 | 6 | 5 | 2 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 12.0 | 12.0 | 12.0 | 5.0 | 7.0 | 5.0 | 7.0 |
| Minimum Split (s) | 34.9 | 34.9 | 34.9 | 11.4 | 37.0 | 11.4 | 37.0 |
| Total Split (s) | 43.6 | 43.6 | 43.6 | 11.4 | 133.0 | 13.4 | 135.0 |
| Total Split (%) | 22.9% | 22.9% | 22.9% | 6.0% | 70.0% | 7.1% | 71.1% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.4 | 4.4 | 4.4 | 4.4 |
| All-Red Time (s) | 4.9 | 4.9 | 4.9 | 2.0 | 3.6 | 2.0 | 3.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.9 | 8.9 | 8.9 | 6.4 | 8.0 | 6.4 | 8.0 |
| Lead/Lag | | | | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | C-Min | None | C-Min |

Intersection Summary

Cycle Length: 190

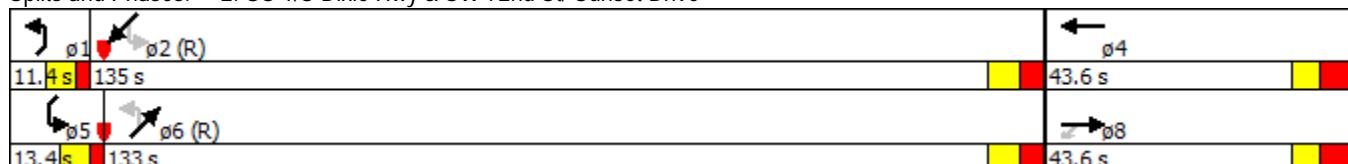
Actuated Cycle Length: 190

Offset: 161 (85%), Referenced to phase 2:SWTL and 6:NETL, Start of Green

Natural Cycle: 135

Control Type: Actuated-Coordinated

Splits and Phases: 2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive



HCM 2010 Signalized Intersection Summary
2: US 1/S Dixie Hwy & SW 72nd St/ Sunset Drive

2019 Future Total
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|---------------------------------------|------|-------|------|-------|------|-------|-------|-------|------|------|------|------|
| Lane Configurations | | ↑↑ | ↑ | | ↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | |
| Traffic Volume (veh/h) | 0 | 523 | 85 | 0 | 474 | 9 | 130 | 2017 | 90 | 50 | 2643 | 255 |
| Future Volume (veh/h) | 0 | 523 | 85 | 0 | 474 | 9 | 130 | 2017 | 90 | 50 | 2643 | 255 |
| Number | 3 | 8 | 18 | 7 | 4 | 14 | 1 | 6 | 16 | 5 | 2 | 12 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 0.90 | 1.00 | | 0.98 | 1.00 | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1863 | 1863 | 0 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 0 | 539 | 0 | 0 | 489 | 9 | 134 | 2079 | 93 | 52 | 2725 | 263 |
| Adj No. of Lanes | 0 | 2 | 1 | 0 | 2 | 0 | 1 | 3 | 0 | 1 | 3 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 0 | 610 | 273 | 0 | 612 | 11 | 101 | 3393 | 151 | 163 | 3207 | 299 |
| Arrive On Green | 0.00 | 0.17 | 0.00 | 0.00 | 0.17 | 0.17 | 0.03 | 0.68 | 0.68 | 0.02 | 0.68 | 0.68 |
| Sat Flow, veh/h | 0 | 3632 | 1583 | 0 | 3641 | 65 | 1774 | 4987 | 222 | 1774 | 4725 | 441 |
| Grp Volume(v), veh/h | 0 | 539 | 0 | 0 | 244 | 254 | 134 | 1411 | 761 | 52 | 1928 | 1060 |
| Grp Sat Flow(s),veh/h/ln | 0 | 1770 | 1583 | 0 | 1770 | 1843 | 1774 | 1695 | 1819 | 1774 | 1695 | 1775 |
| Q Serve(g_s), s | 0.0 | 28.2 | 0.0 | 0.0 | 25.1 | 25.2 | 5.0 | 43.3 | 43.7 | 1.7 | 80.5 | 90.4 |
| Cycle Q Clear(g_c), s | 0.0 | 28.2 | 0.0 | 0.0 | 25.1 | 25.2 | 5.0 | 43.3 | 43.7 | 1.7 | 80.5 | 90.4 |
| Prop In Lane | 0.00 | | 1.00 | 0.00 | | 0.04 | 1.00 | | 0.12 | 1.00 | | 0.25 |
| Lane Grp Cap(c), veh/h | 0 | 610 | 273 | 0 | 305 | 318 | 101 | 2306 | 1237 | 163 | 2301 | 1205 |
| V/C Ratio(X) | 0.00 | 0.88 | 0.00 | 0.00 | 0.80 | 0.80 | 1.33 | 0.61 | 0.62 | 0.32 | 0.84 | 0.88 |
| Avail Cap(c_a), veh/h | 0 | 646 | 289 | 0 | 323 | 337 | 101 | 2306 | 1237 | 185 | 2301 | 1205 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 76.8 | 0.0 | 0.0 | 75.5 | 75.5 | 58.0 | 16.6 | 16.7 | 15.6 | 22.8 | 24.3 |
| Incr Delay (d2), s/veh | 0.0 | 13.2 | 0.0 | 0.0 | 12.6 | 12.3 | 201.2 | 1.2 | 2.3 | 0.4 | 3.8 | 9.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.0 | 15.0 | 0.0 | 0.0 | 13.4 | 13.9 | 10.9 | 20.6 | 22.6 | 0.9 | 38.7 | 47.3 |
| LnGrp Delay(d),s/veh | 0.0 | 90.0 | 0.0 | 0.0 | 88.1 | 87.8 | 259.1 | 17.8 | 19.0 | 16.0 | 26.6 | 33.6 |
| LnGrp LOS | | F | | | F | F | B | B | B | C | C | |
| Approach Vol, veh/h | | 539 | | | 498 | | | 2306 | | | 3040 | |
| Approach Delay, s/veh | | 90.0 | | | 87.9 | | | 32.2 | | | 28.9 | |
| Approach LOS | | F | | | F | | | C | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 11.4 | 136.9 | | 41.7 | 11.1 | 137.3 | | 41.7 | | | | |
| Change Period (Y+R _c), s | 6.4 | 8.0 | | * 8.9 | 6.4 | 8.0 | | * 8.9 | | | | |
| Max Green Setting (Gmax), s | 5.0 | 127.0 | | * 35 | 7.0 | 125.0 | | * 35 | | | | |
| Max Q Clear Time (g_c+l1), s | 7.0 | 92.4 | | 27.2 | 3.7 | 45.7 | | 30.2 | | | | |
| Green Ext Time (p_c), s | 0.0 | 28.3 | | 3.8 | 0.0 | 51.8 | | 2.5 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 39.9 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings
3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2019 Future Total
P.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NET | NER | SWT | SWR | ø1 | ø2 |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|------|--------|------|-------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑ | ↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | | |
| Traffic Volume (vph) | 373 | 138 | 20 | 175 | 319 | 3 | 2316 | 203 | 2101 | 630 | | |
| Future Volume (vph) | 373 | 138 | 20 | 175 | 319 | 3 | 2316 | 203 | 2101 | 630 | | |
| Turn Type | Split | NA | Perm | Split | NA | Perm | NA | Prot | NA | custom | | |
| Protected Phases | 3 | 3 | | 4 | 4 | | 6 | 6 | 12 | 23 | 1 | 2 |
| Permitted Phases | | | | 3 | | 4 | | | | | | |
| Detector Phase | 3 | 3 | 3 | 4 | 4 | 4 | 6 | 6 | 12 | 23 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 15.0 | 15.0 | | | 1.0 | 15.0 |
| Minimum Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 25.5 | 25.5 | | | 25.0 | 32.5 |
| Total Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 138.0 | 138.0 | | | 25.0 | 113.0 |
| Total Split (%) | 13.7% | 13.7% | 13.7% | 13.7% | 13.7% | 13.7% | 72.6% | 72.6% | | | 13% | 59% |
| Yellow Time (s) | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.4 | 4.8 | 4.8 | | | 2.0 | 4.8 |
| All-Red Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.7 | 2.7 | | | 0.0 | 2.7 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 7.5 | 7.5 | | | | |
| Lead/Lag | Lead | Lead | Lead | Lag | Lag | Lag | | | | | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | | | | | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C-Min | C-Min | | | Max | C-Min |

Intersection Summary

Cycle Length: 190

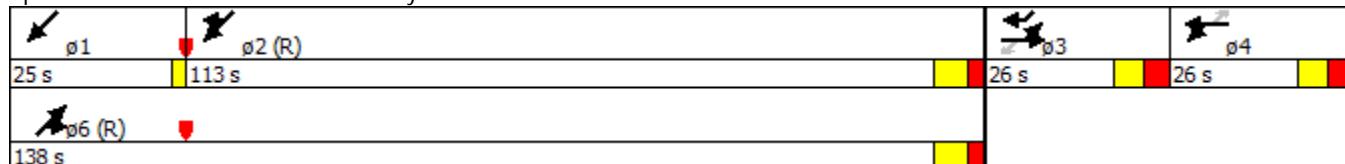
Actuated Cycle Length: 190

Offset: 136 (72%), Referenced to phase 2:SWT and 6:NET, Start of Green

Natural Cycle: 110

Control Type: Actuated-Coordinated

Splits and Phases: 3: US 1/S Dixie Hwy & SW 40th St/Bird Rd



HCM Signalized Intersection Capacity Analysis
3: US 1/S Dixie Hwy & SW 40th St/Bird Rd

2019 Future Total
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
|-----------------------------------|-------|-------|-------|-------|---------------------------|------|------|-------|-------|------|-------|--------|
| Lane Configurations | ↑↑ | ↓ | ↑ | ↑ | ↑↑ | ↑ | | ↑↑↑ | ↑ | ↑↑↑ | ↑↑↑ | ↑ |
| Traffic Volume (vph) | 373 | 138 | 20 | 175 | 319 | 3 | 0 | 2316 | 203 | 0 | 2101 | 630 |
| Future Volume (vph) | 373 | 138 | 20 | 175 | 319 | 3 | 0 | 2316 | 203 | 0 | 2101 | 630 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | 7.5 | 7.5 | | 2.0 | 7.5 |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.91 | 1.00 | | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (prot) | 3221 | 1677 | 1522 | 1770 | 3539 | 1583 | | 5085 | 1583 | | 5085 | 1583 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Satd. Flow (perm) | 3221 | 1677 | 1522 | 1770 | 3539 | 1583 | | 5085 | 1583 | | 5085 | 1583 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 393 | 145 | 21 | 184 | 336 | 3 | 0 | 2438 | 214 | 0 | 2212 | 663 |
| RTOR Reduction (vph) | 0 | 0 | 19 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 354 | 184 | 2 | 184 | 336 | 0 | 0 | 2438 | 214 | 0 | 2212 | 663 |
| Confl. Peds. (#/hr) | | | 5 | 5 | | | 7 | | | | | 7 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | | | | 6 |
| Turn Type | Split | NA | Perm | Split | NA | Perm | | NA | Prot | | NA | custom |
| Protected Phases | 3 | 3 | | 4 | 4 | | | 6 | 6 | | 12 | 23 |
| Permitted Phases | | | 3 | | | 4 | | | | | | |
| Actuated Green, G (s) | 22.5 | 22.5 | 22.5 | 20.8 | 20.8 | 20.8 | | 123.2 | 123.2 | | 123.2 | 126.8 |
| Effective Green, g (s) | 22.5 | 22.5 | 22.5 | 20.8 | 20.8 | 20.8 | | 123.2 | 123.2 | | 123.2 | 126.8 |
| Actuated g/C Ratio | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 | 0.11 | | 0.65 | 0.65 | | 0.65 | 0.67 |
| Clearance Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | 7.5 | 7.5 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | | 1.0 | 1.0 | | | |
| Lane Grp Cap (vph) | 381 | 198 | 180 | 193 | 387 | 173 | | 3297 | 1026 | | 3297 | 1056 |
| v/s Ratio Prot | c0.11 | 0.11 | | c0.10 | 0.09 | | | c0.48 | 0.14 | | 0.43 | 0.42 |
| v/s Ratio Perm | | | 0.00 | | | 0.00 | | | | | | |
| v/c Ratio | 0.93 | 0.93 | 0.01 | 0.95 | 0.87 | 0.00 | | 0.74 | 0.21 | | 0.67 | 0.63 |
| Uniform Delay, d1 | 83.0 | 83.0 | 74.0 | 84.1 | 83.3 | 75.4 | | 22.6 | 13.6 | | 20.8 | 18.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 28.5 | 43.8 | 0.0 | 51.1 | 18.0 | 0.0 | | 1.5 | 0.5 | | 1.1 | 1.2 |
| Delay (s) | 111.5 | 126.8 | 74.0 | 135.2 | 101.3 | 75.4 | | 24.1 | 14.0 | | 21.9 | 19.3 |
| Level of Service | F | F | E | F | F | E | | C | B | | C | B |
| Approach Delay (s) | | 115.1 | | | 113.1 | | | 23.3 | | | 21.3 | |
| Approach LOS | | F | | | F | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 37.3 | | HCM 2000 Level of Service | | | | D | | | |
| HCM 2000 Volume to Capacity ratio | | | 0.80 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 190.0 | | Sum of lost time (s) | | | | 25.5 | | | |
| Intersection Capacity Utilization | | | 83.4% | | ICU Level of Service | | | | E | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Timings
4: SW 27th Ave & US 1/S Dixie Hwy

2019 Future Total
P.M. Peak Hour

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↓ | ↑ | ↑↑↓ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 158 | 2484 | 129 | 2888 | 26 | 517 | 131 | 40 | 509 | 229 |
| Future Volume (vph) | 158 | 2484 | 129 | 2888 | 26 | 517 | 131 | 40 | 509 | 229 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | NA | pm+ov | Perm | NA | pm+ov |
| Protected Phases | 1 | 6 | 5 | 2 | | 4 | 5 | | 8 | 1 |
| Permitted Phases | 6 | | 2 | | 4 | | 4 | 8 | | 8 |
| Detector Phase | 1 | 6 | 5 | 2 | 4 | 4 | 5 | 8 | 8 | 1 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 5.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 | 5.0 |
| Minimum Split (s) | 9.5 | 39.9 | 9.5 | 39.9 | 29.6 | 29.6 | 9.5 | 29.6 | 29.6 | 9.5 |
| Total Split (s) | 16.0 | 132.0 | 20.0 | 136.0 | 38.0 | 38.0 | 20.0 | 38.0 | 38.0 | 16.0 |
| Total Split (%) | 8.4% | 69.5% | 10.5% | 71.6% | 20.0% | 20.0% | 10.5% | 20.0% | 20.0% | 8.4% |
| Yellow Time (s) | 3.5 | 4.8 | 3.5 | 4.8 | 4.4 | 4.4 | 3.5 | 4.4 | 4.4 | 3.5 |
| All-Red Time (s) | 1.0 | 2.1 | 1.0 | 2.1 | 2.2 | 2.2 | 1.0 | 2.2 | 2.2 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 6.9 | 4.5 | 6.9 | 6.6 | 6.6 | 4.5 | 6.6 | 6.6 | 4.5 |
| Lead/Lag | Lead | Lag | Lead | Lag | | | | Lead | | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | | | | Yes | | Yes |
| Recall Mode | None | C-Min | None | C-Min | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 190

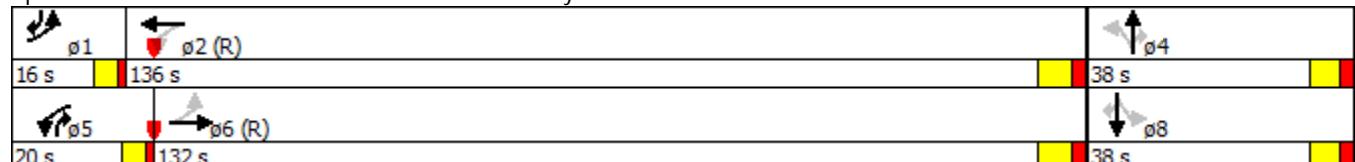
Actuated Cycle Length: 190

Offset: 75 (39%), Referenced to phase 2:WBTL and 6:EBTL, Start of Green

Natural Cycle: 120

Control Type: Actuated-Coordinated

Splits and Phases: 4: SW 27th Ave & US 1/S Dixie Hwy



HCM 2010 Signalized Intersection Summary
4: SW 27th Ave & US 1/S Dixie Hwy

2019 Future Total
P.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|-------|-------|------|-------|------|-------|-------|-------|------|-------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | | ↑ | ↑↑↑ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 158 | 2484 | 33 | 129 | 2888 | 98 | 26 | 517 | 131 | 40 | 509 | 229 |
| Future Volume (veh/h) | 158 | 2484 | 33 | 129 | 2888 | 98 | 26 | 517 | 131 | 40 | 509 | 229 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.98 | 1.00 | | 1.00 | 1.00 | | 0.78 | 1.00 | | 0.77 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 158 | 2484 | 33 | 129 | 2888 | 0 | 26 | 517 | 131 | 40 | 509 | 229 |
| Adj No. of Lanes | 1 | 3 | 0 | 1 | 3 | 0 | 1 | 2 | 1 | 1 | 2 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 168 | 3651 | 48 | 154 | 3455 | 0 | 56 | 585 | 258 | 55 | 585 | 298 |
| Arrive On Green | 0.06 | 0.71 | 0.71 | 0.03 | 0.68 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 1774 | 5171 | 69 | 1774 | 5253 | 0 | 717 | 3539 | 1238 | 780 | 3539 | 1225 |
| Grp Volume(v), veh/h | 158 | 1626 | 891 | 129 | 2888 | 0 | 26 | 517 | 131 | 40 | 509 | 229 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1849 | 1774 | 1695 | 0 | 717 | 1770 | 1238 | 780 | 1770 | 1225 |
| Q Serve(g_s), s | 10.3 | 51.5 | 51.9 | 4.3 | 80.0 | 0.0 | 4.8 | 27.1 | 18.0 | 4.3 | 26.6 | 31.4 |
| Cycle Q Clear(g_c), s | 10.3 | 51.5 | 51.9 | 4.3 | 80.0 | 0.0 | 31.4 | 27.1 | 18.0 | 31.4 | 26.6 | 31.4 |
| Prop In Lane | 1.00 | | 0.04 | 1.00 | | 0.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 168 | 2393 | 1306 | 154 | 3455 | 0 | 56 | 585 | 258 | 55 | 585 | 298 |
| V/C Ratio(X) | 0.94 | 0.68 | 0.68 | 0.84 | 0.84 | 0.00 | 0.47 | 0.88 | 0.51 | 0.72 | 0.87 | 0.77 |
| Avail Cap(c_a), veh/h | 168 | 2393 | 1306 | 238 | 3455 | 0 | 56 | 585 | 258 | 55 | 585 | 298 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 64.9 | 15.8 | 15.8 | 34.5 | 22.6 | 0.0 | 93.4 | 77.5 | 68.1 | 94.1 | 77.3 | 70.0 |
| Incr Delay (d2), s/veh | 51.9 | 1.6 | 2.9 | 14.3 | 2.6 | 0.0 | 7.1 | 15.1 | 1.9 | 38.0 | 13.5 | 11.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 10.5 | 24.5 | 27.3 | 5.2 | 38.0 | 0.0 | 1.5 | 14.5 | 6.3 | 2.7 | 14.2 | 12.4 |
| LnGrp Delay(d),s/veh | 116.8 | 17.4 | 18.7 | 48.8 | 25.2 | 0.0 | 100.5 | 92.6 | 70.0 | 132.1 | 90.9 | 81.8 |
| LnGrp LOS | F | B | B | D | C | | F | F | E | F | F | F |
| Approach Vol, veh/h | | 2675 | | | 3017 | | | 674 | | | 778 | |
| Approach Delay, s/veh | | 23.7 | | | 26.2 | | | 88.5 | | | 90.3 | |
| Approach LOS | | C | | | C | | | F | | | F | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 16.0 | 136.0 | | 38.0 | 11.0 | 141.0 | | 38.0 | | | | |
| Change Period (Y+R _c), s | 4.5 | 6.9 | | * 6.6 | 4.5 | 6.9 | | * 6.6 | | | | |
| Max Green Setting (Gmax), s | 11.5 | 129.1 | | * 31 | 15.5 | 125.1 | | * 31 | | | | |
| Max Q Clear Time (g_c+l1), s | 12.3 | 82.0 | | 33.4 | 6.3 | 53.9 | | 33.4 | | | | |
| Green Ext Time (p_c), s | 0.0 | 39.3 | | 0.0 | 0.2 | 54.7 | | 0.0 | | | | |
| <u>Intersection Summary</u> | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 38.1 | | | | | | | | | |
| HCM 2010 LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Timings
5: SE 26th Rd & US 1/Brickell Ave

2019 Future Total
A.M. Peak Hour

| Lane Group | EBL | EBT | EBR | WBT | WBR | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (vph) | 238 | 1265 | 18 | 211 | 273 | 905 | 555 | 137 | 554 | 104 |
| Future Volume (vph) | 238 | 1265 | 18 | 211 | 273 | 905 | 555 | 137 | 554 | 104 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | NA | Free | Prot | NA | Perm |
| Protected Phases | 7 | 4 | | 8 | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | Free | | | 6 |
| Detector Phase | 7 | 4 | 4 | 8 | 8 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Minimum Split (s) | 11.0 | 27.8 | 27.8 | 27.8 | 27.8 | 33.6 | | 11.0 | 33.6 | 33.6 |
| Total Split (s) | 23.0 | 53.0 | 53.0 | 30.0 | 30.0 | 52.0 | | 15.0 | 67.0 | 67.0 |
| Total Split (%) | 19.2% | 44.2% | 44.2% | 25.0% | 25.0% | 43.3% | | 12.5% | 55.8% | 55.8% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.8 | 2.8 | 2.8 | 2.8 | 2.6 | | 2.0 | 2.6 | 2.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.8 | 6.8 | 6.8 | 6.8 | 6.6 | | 6.0 | 6.6 | 6.6 |
| Lead/Lag | Lead | | | Lag | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | Yes | | | Yes | Yes | Yes | | Yes | | |
| Recall Mode | None | Max | Max | None | None | C-Min | | None | C-Min | C-Min |

Intersection Summary

Cycle Length: 120

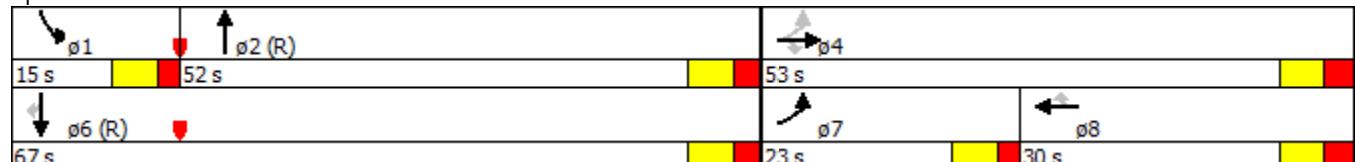
Actuated Cycle Length: 120

Offset: 74 (62%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Natural Cycle: 85

Control Type: Actuated-Coordinated

Splits and Phases: 5: SE 26th Rd & US 1/Brickell Ave



HCM 2010 Signalized Intersection Summary
5: SE 26th Rd & US 1/Brickell Ave

2019 Future Total
A.M. Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|-------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | | ↑↑ | ↑ | | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 238 | 1265 | 18 | 0 | 211 | 273 | 0 | 905 | 555 | 137 | 554 | 104 |
| Future Volume (veh/h) | 238 | 1265 | 18 | 0 | 211 | 273 | 0 | 905 | 555 | 137 | 554 | 104 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 0 | 1863 | 1863 | 0 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 294 | 1562 | 0 | 0 | 260 | 0 | 0 | 1117 | 0 | 169 | 684 | 0 |
| Adj No. of Lanes | 1 | 3 | 1 | 0 | 2 | 1 | 0 | 2 | 1 | 2 | 2 | 1 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 224 | 1781 | 797 |
| Arrive On Green | 0.14 | 0.38 | 0.00 | 0.00 | 0.19 | 0.00 | 0.00 | 0.39 | 0.00 | 0.07 | 0.50 | 0.00 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 0 | 3632 | 1583 | 0 | 3632 | 1583 | 3442 | 3539 | 1583 |
| Grp Volume(v), veh/h | 294 | 1562 | 0 | 0 | 260 | 0 | 0 | 1117 | 0 | 169 | 684 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 0 | 1770 | 1583 | 0 | 1770 | 1583 | 1721 | 1770 | 1583 |
| Q Serve(g_s), s | 15.5 | 32.7 | 0.0 | 0.0 | 7.7 | 0.0 | 0.0 | 33.8 | 0.0 | 5.8 | 14.3 | 0.0 |
| Cycle Q Clear(g_c), s | 15.5 | 32.7 | 0.0 | 0.0 | 7.7 | 0.0 | 0.0 | 33.8 | 0.0 | 5.8 | 14.3 | 0.0 |
| Prop In Lane | 1.00 | | | 1.00 | 0.00 | | 1.00 | 0.00 | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 224 | 1781 | 797 |
| V/C Ratio(X) | 0.65 | 0.80 | 0.00 | 0.00 | 0.38 | 0.00 | 0.00 | 0.81 | 0.00 | 0.76 | 0.38 | 0.00 |
| Avail Cap(c_a), veh/h | 456 | 1958 | 610 | 0 | 684 | 306 | 0 | 1374 | 615 | 258 | 1781 | 797 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 30.8 | 32.8 | 0.0 | 0.0 | 42.1 | 0.0 | 0.0 | 32.8 | 0.0 | 55.2 | 18.3 | 0.0 |
| Incr Delay (d2), s/veh | 2.5 | 3.5 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 5.3 | 0.0 | 8.4 | 0.6 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 7.8 | 16.0 | 0.0 | 0.0 | 3.8 | 0.0 | 0.0 | 17.5 | 0.0 | 3.0 | 7.1 | 0.0 |
| LnGrp Delay(d),s/veh | 33.2 | 36.2 | 0.0 | 0.0 | 42.4 | 0.0 | 0.0 | 38.1 | 0.0 | 63.6 | 19.0 | 0.0 |
| LnGrp LOS | C | D | | | D | | | D | | E | B | |
| Approach Vol, veh/h | | 1856 | | | 260 | | | 1117 | | | 853 | |
| Approach Delay, s/veh | | 35.8 | | | 42.4 | | | 38.1 | | | 27.8 | |
| Approach LOS | | D | | | D | | | D | | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 13.8 | 53.2 | | 53.0 | | 67.0 | 23.0 | 30.0 | | | | |
| Change Period (Y+R _c), s | 6.0 | 6.6 | | * 6.8 | | 6.6 | 6.0 | * 6.8 | | | | |
| Max Green Setting (Gmax), s | 9.0 | 45.4 | | * 46 | | 60.4 | 17.0 | * 23 | | | | |
| Max Q Clear Time (g_c+l1), s | 7.8 | 35.8 | | 34.7 | | 16.3 | 17.5 | 9.7 | | | | |
| Green Ext Time (p_c), s | 0.0 | 4.2 | | 7.9 | | 6.3 | 0.0 | 8.9 | | | | |

Intersection Summary

| | |
|---------------------|------|
| HCM 2010 Ctrl Delay | 35.2 |
| HCM 2010 LOS | D |

Notes